

Fig.1A

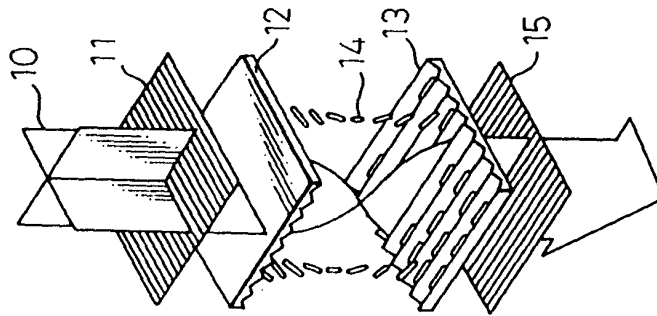


Fig.1B

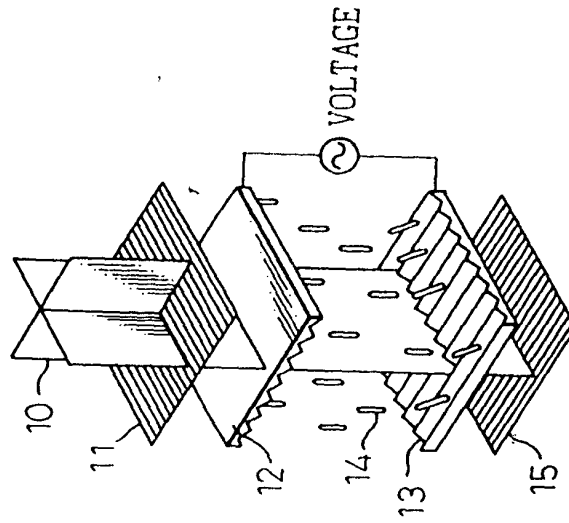


Fig.2A

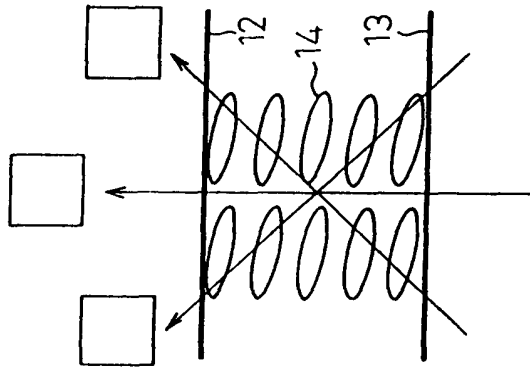


Fig.2B

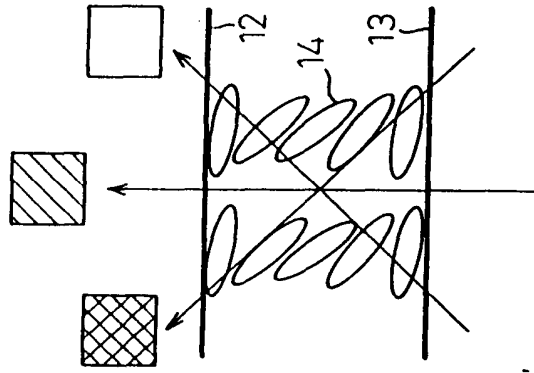


Fig.2C

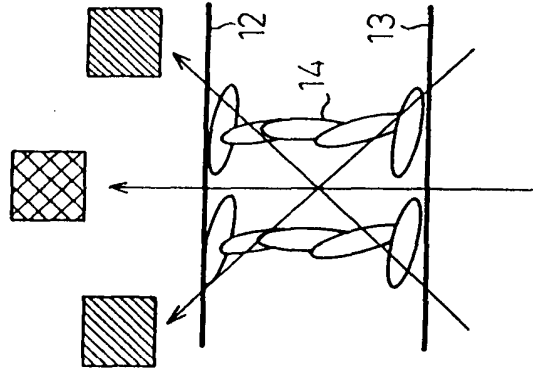


Fig.3A

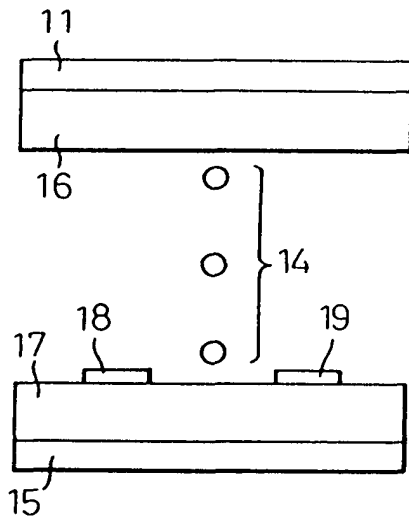


Fig.3C

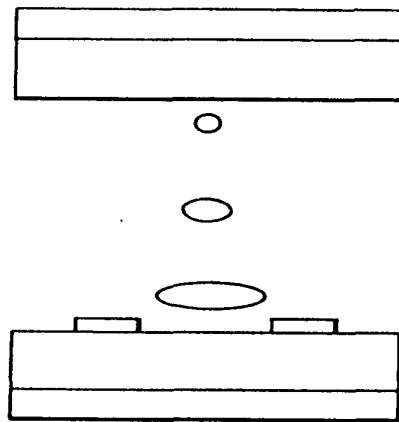


Fig.3B

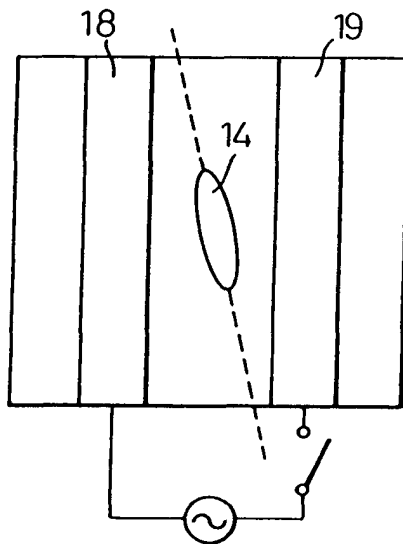


Fig.3D

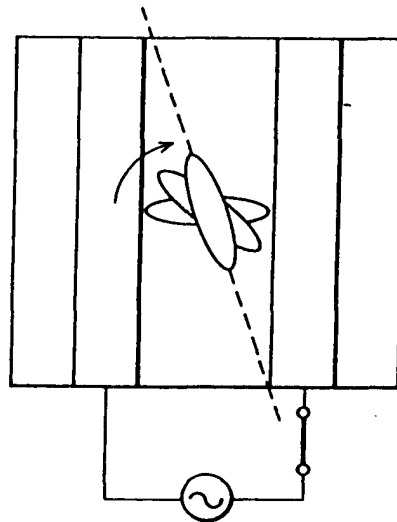
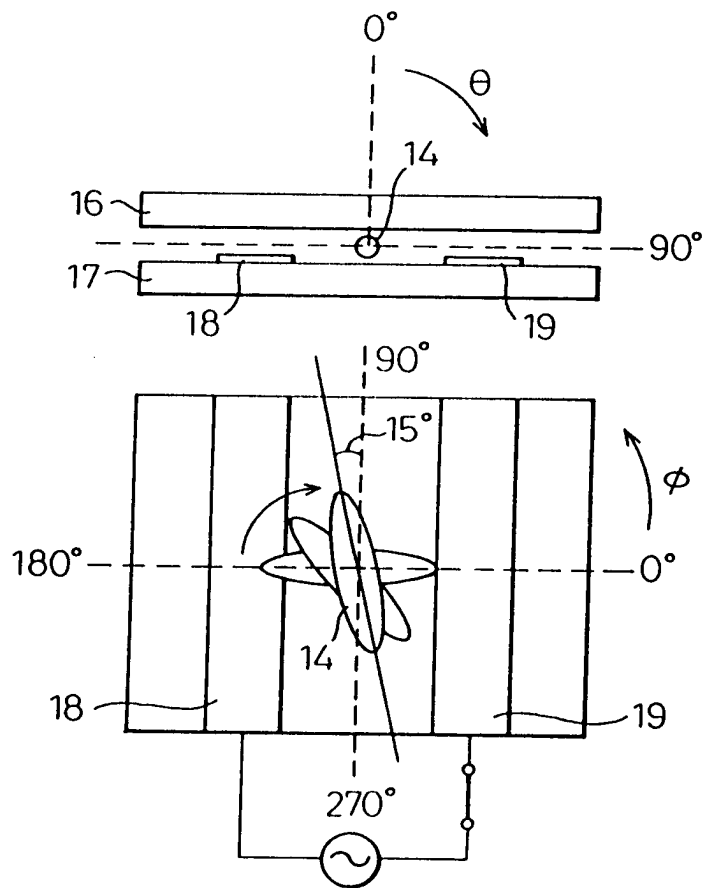
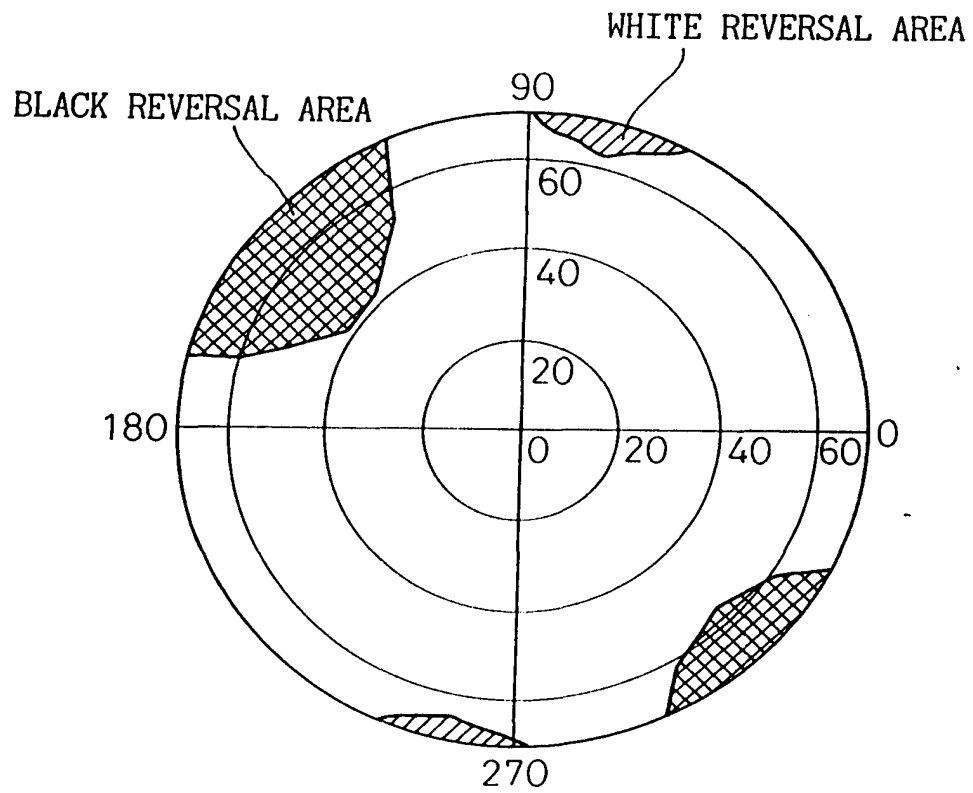


Fig. 4



5/246

Fig. 5



6/246

Fig. 6A

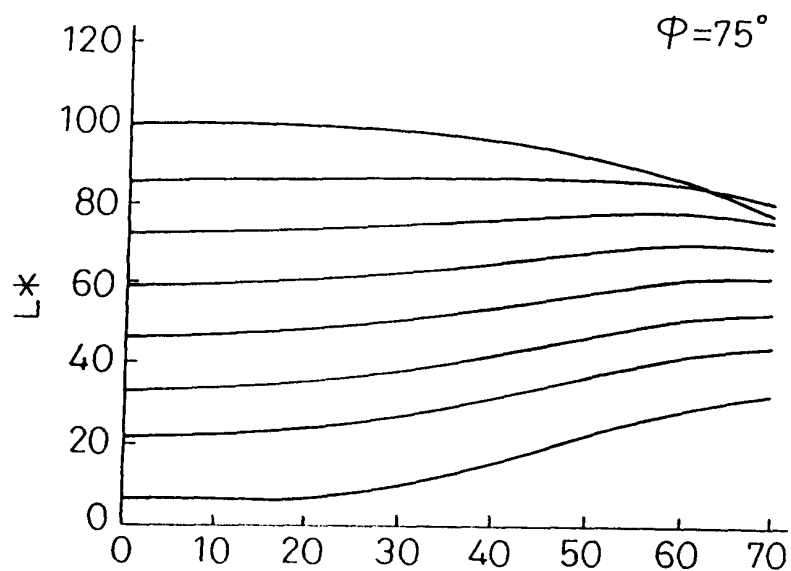


Fig. 6B

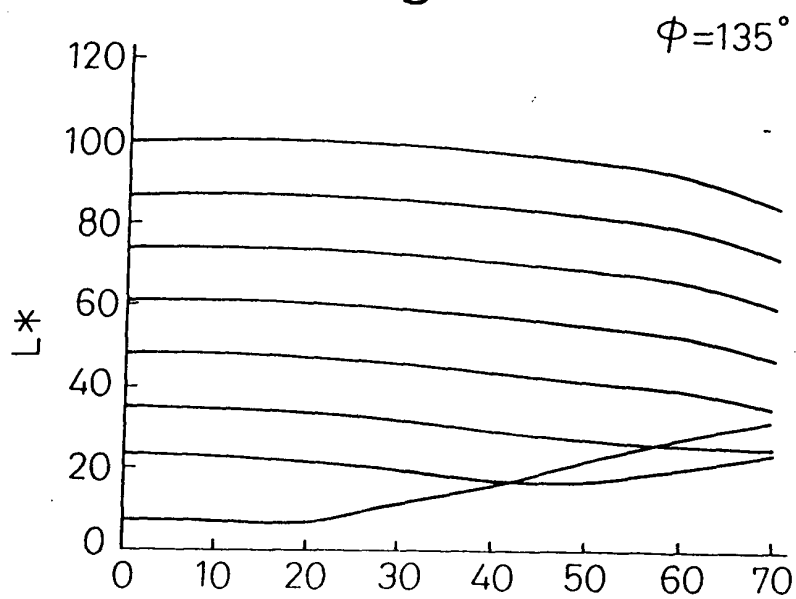


Fig.7A                      Fig.7B                      Fig.7C

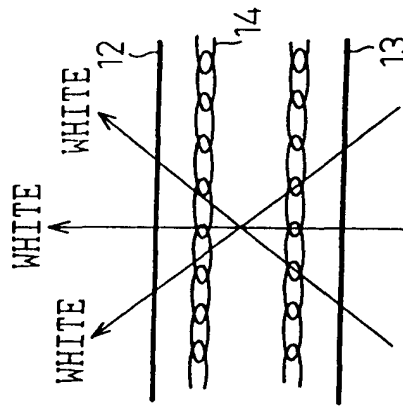
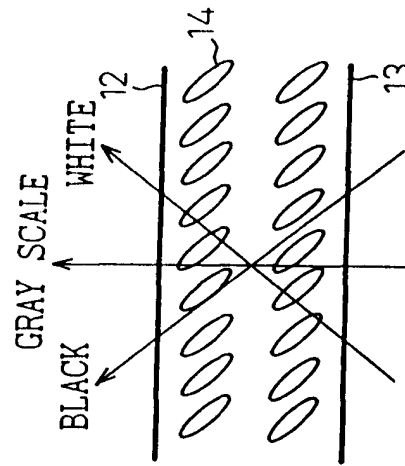
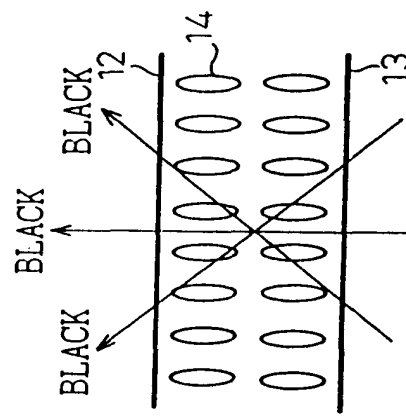


Fig.8A

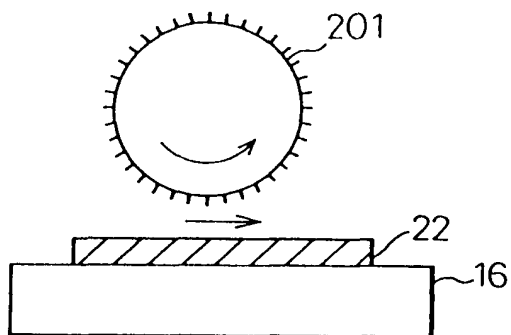


Fig.8B

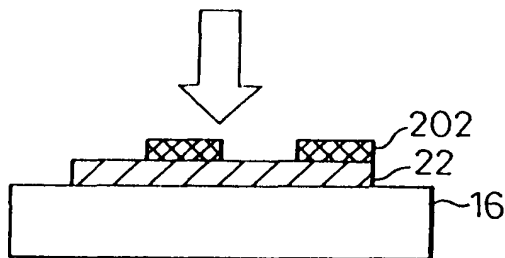


Fig.8C

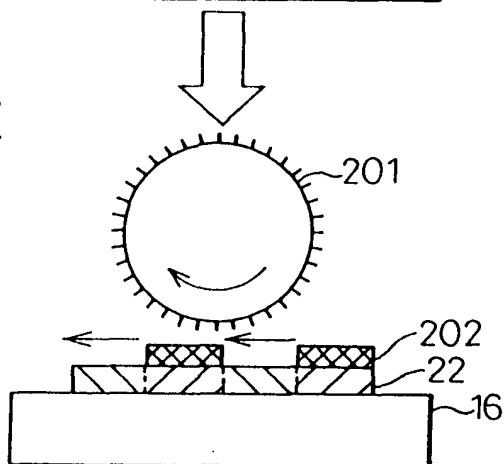




Fig.9A

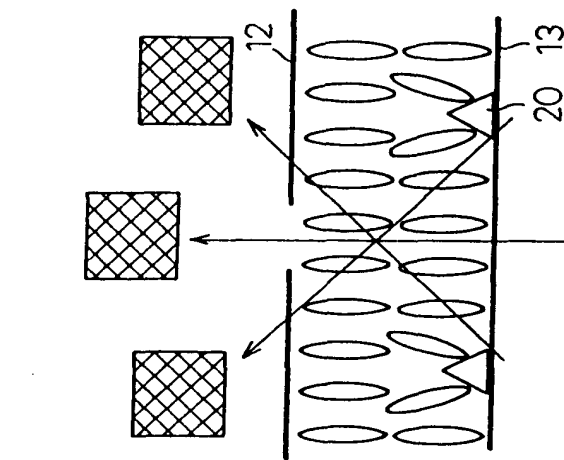


Fig.9B

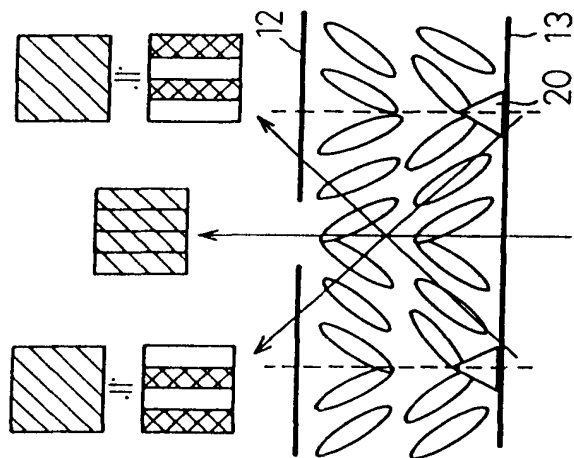


Fig.9C

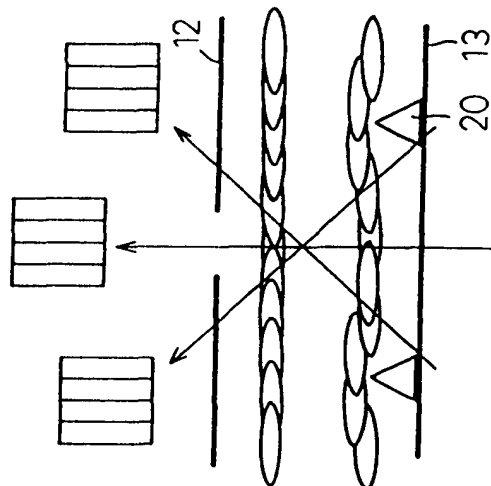


Fig.10A

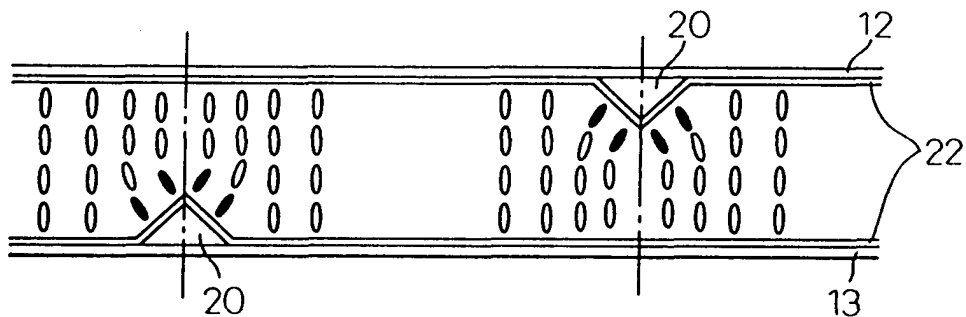


Fig.10B

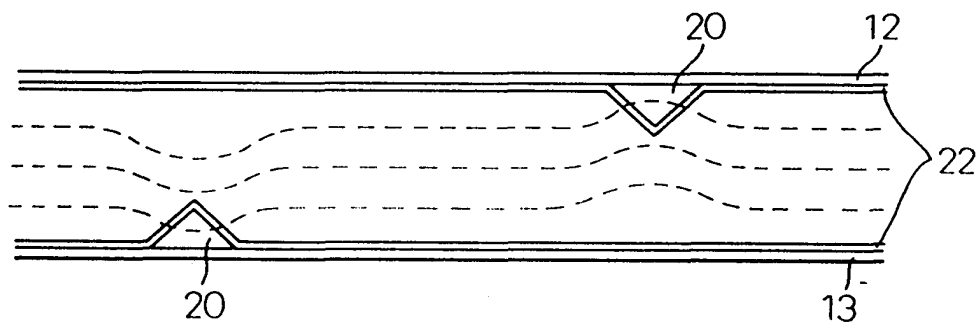


Fig.10C

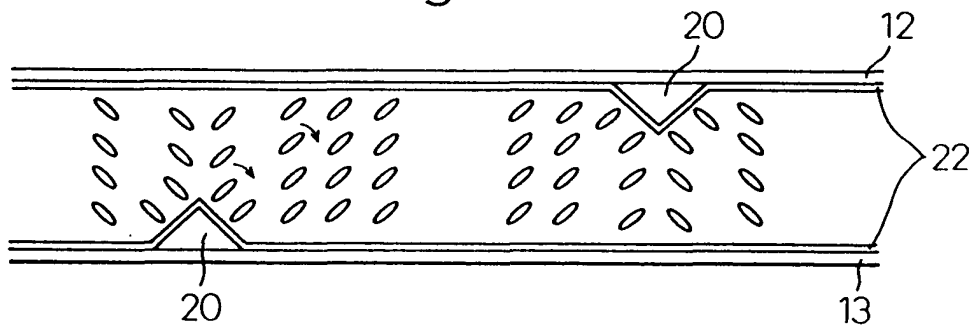


Fig.11A

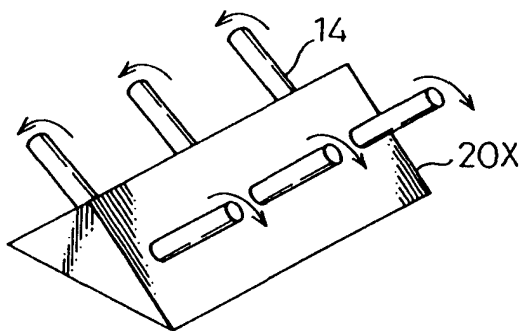


Fig.11B

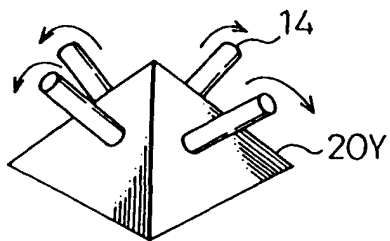


Fig.11C

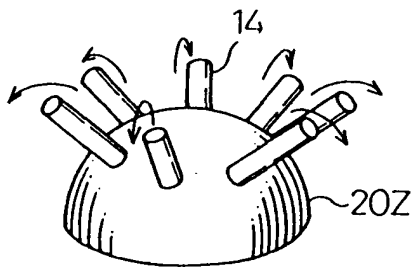


Fig.12A

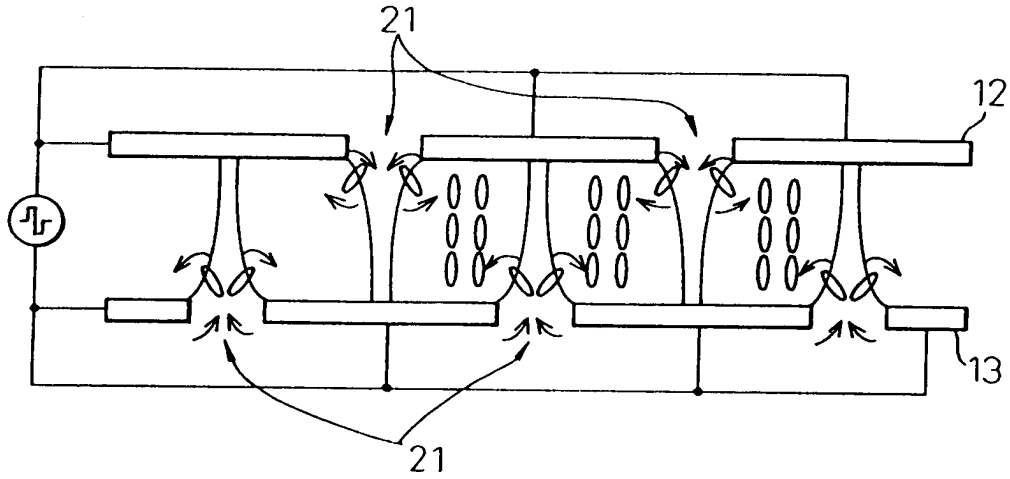


Fig.12B

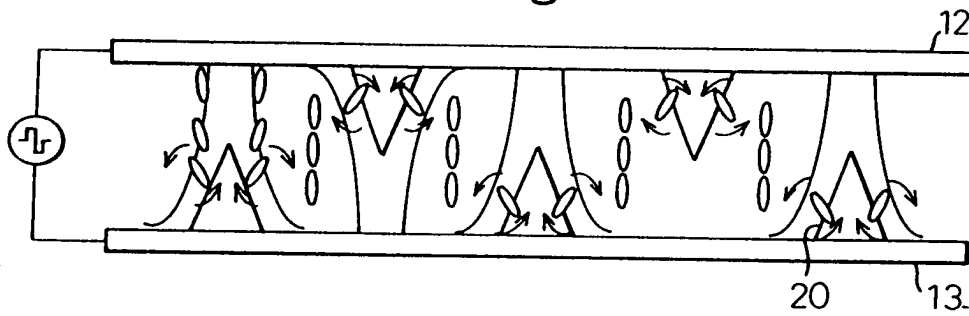
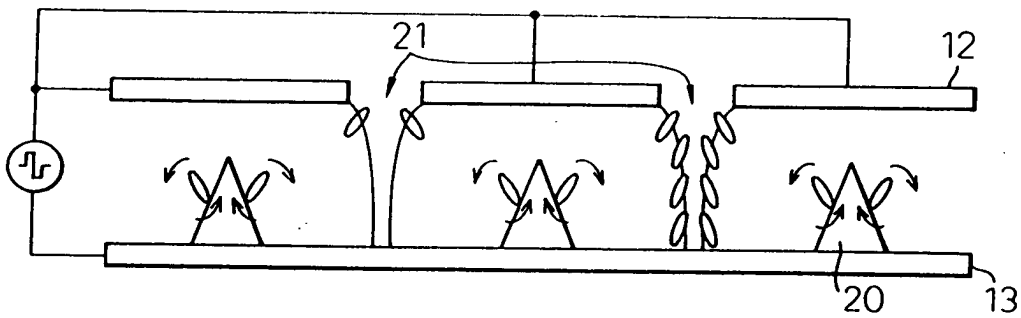
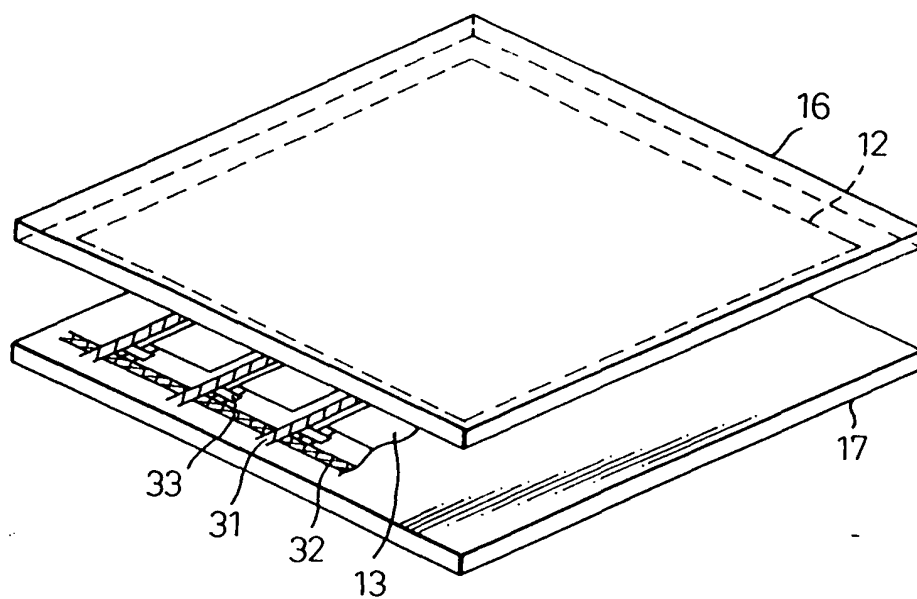


Fig.12C



13/246

Fig.13



14/246

Fig.14A

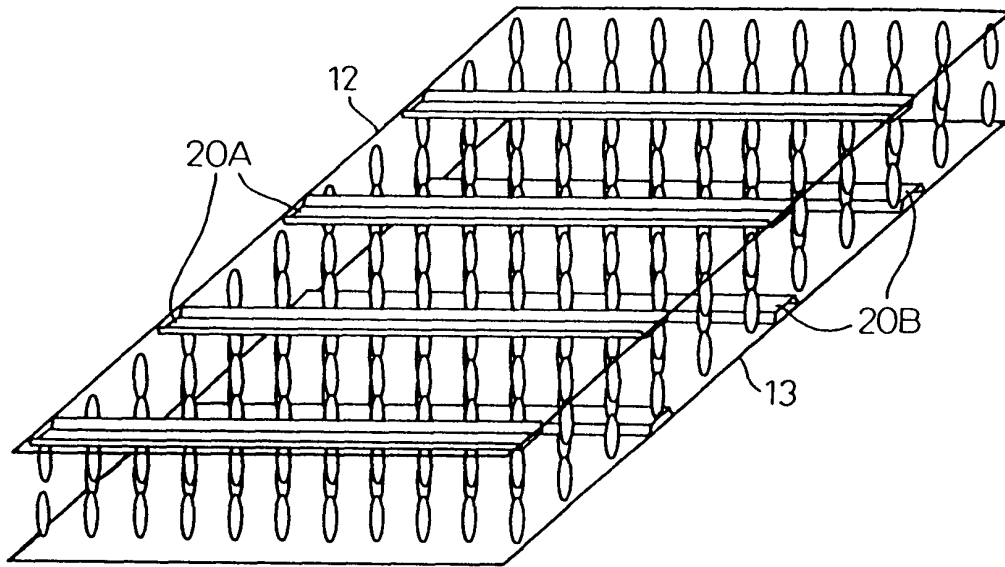


Fig.14B

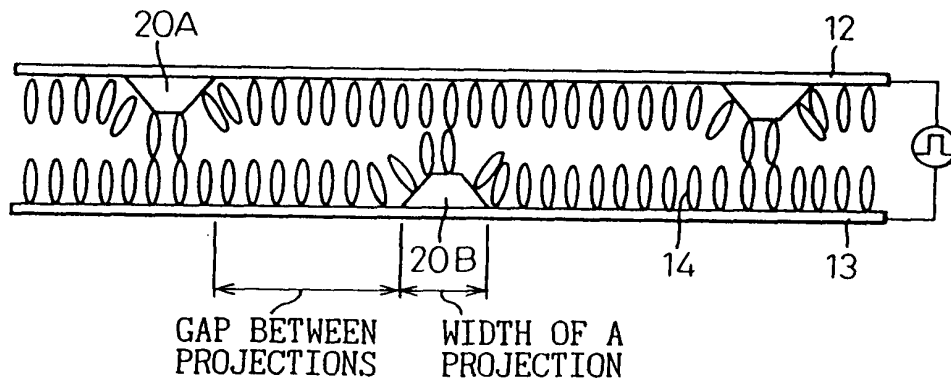


Fig.15

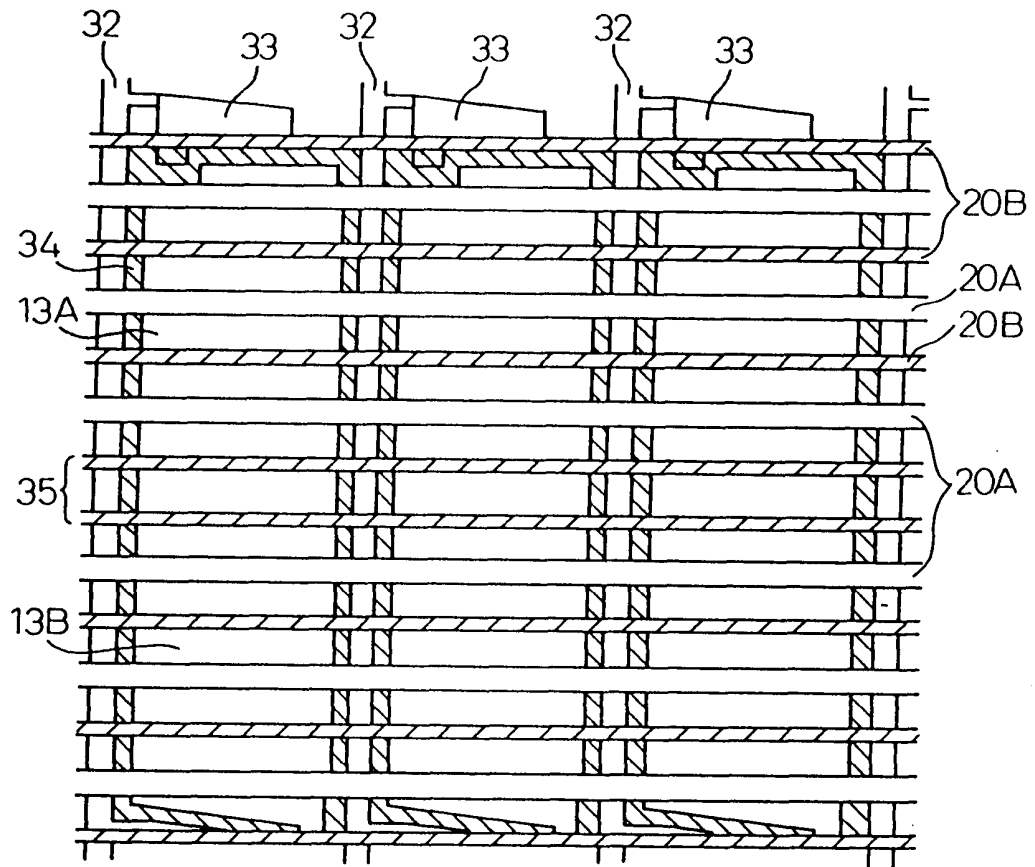


Fig.16

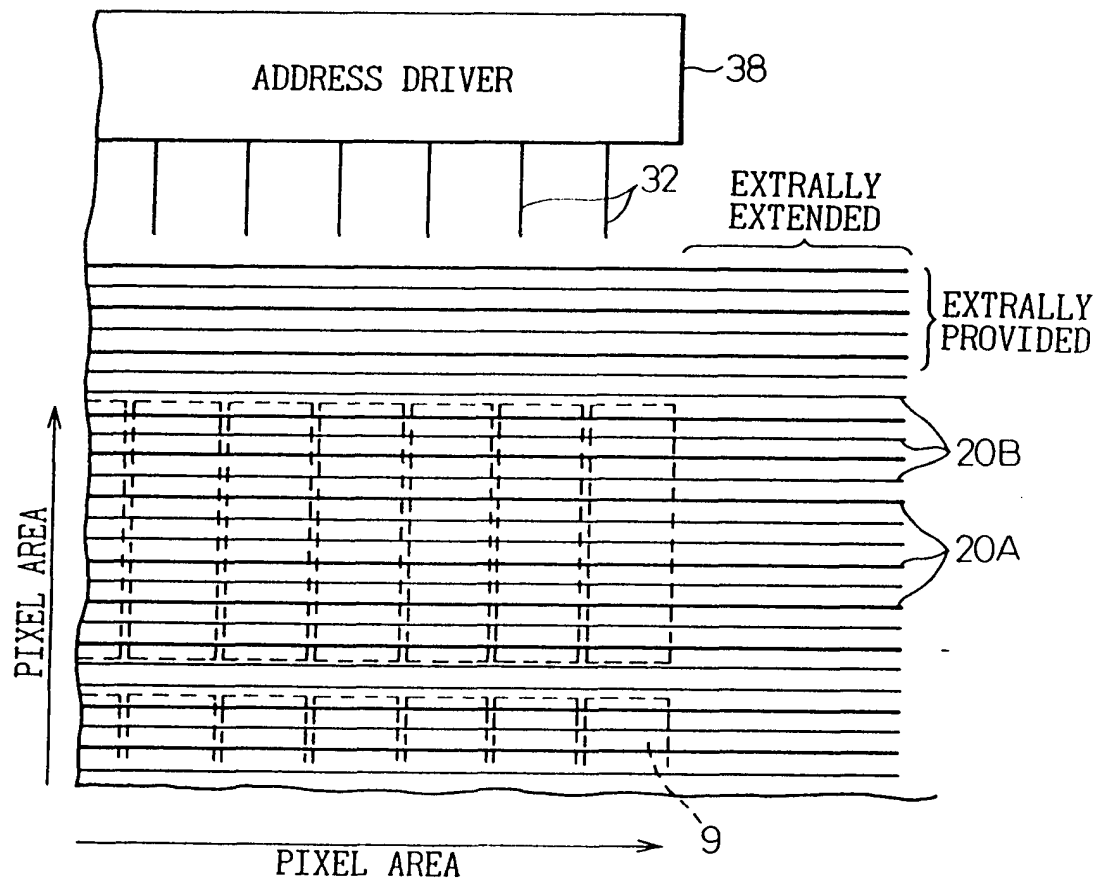




Fig.17

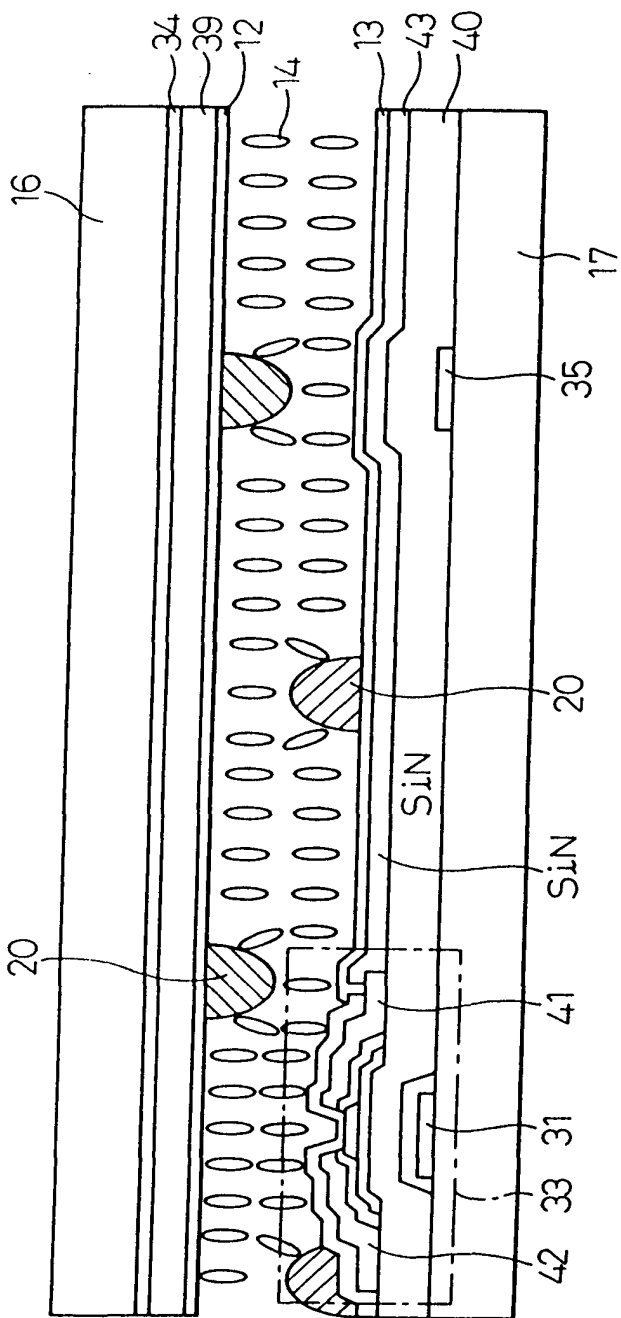


Fig.18A

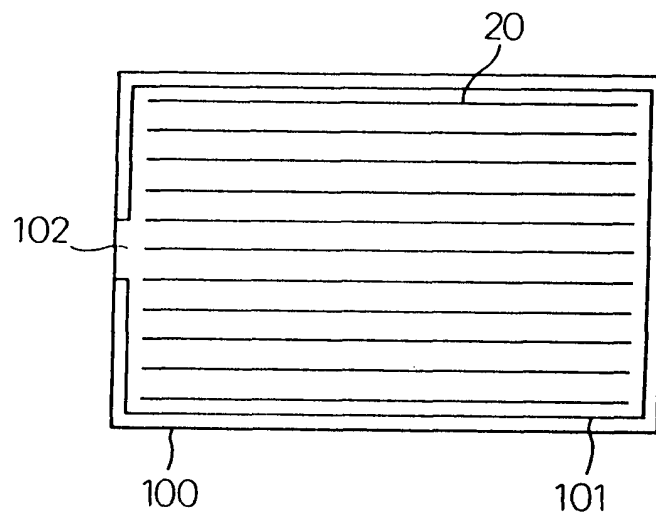


Fig.18B

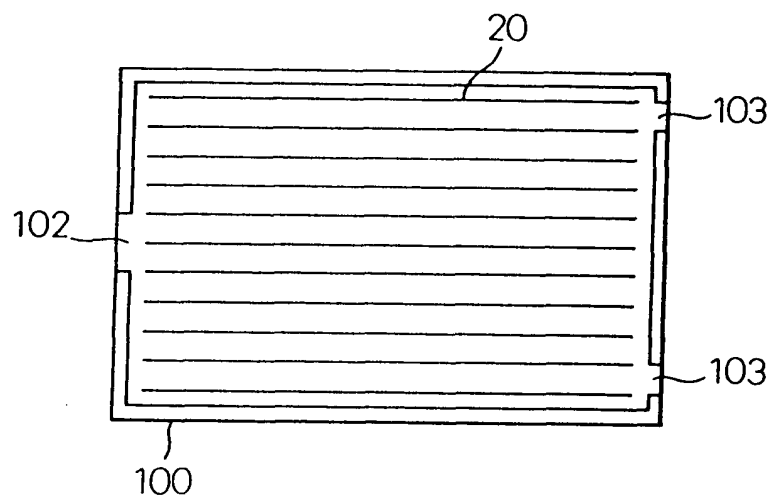
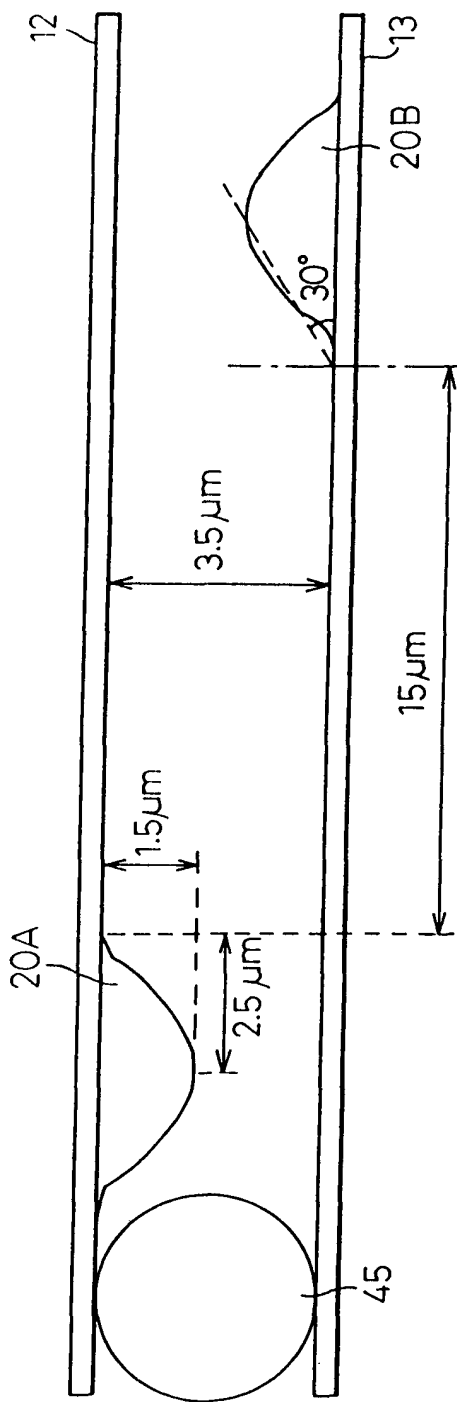


Fig.19



20/246

Fig.20A

ON RESPONSE SPEED

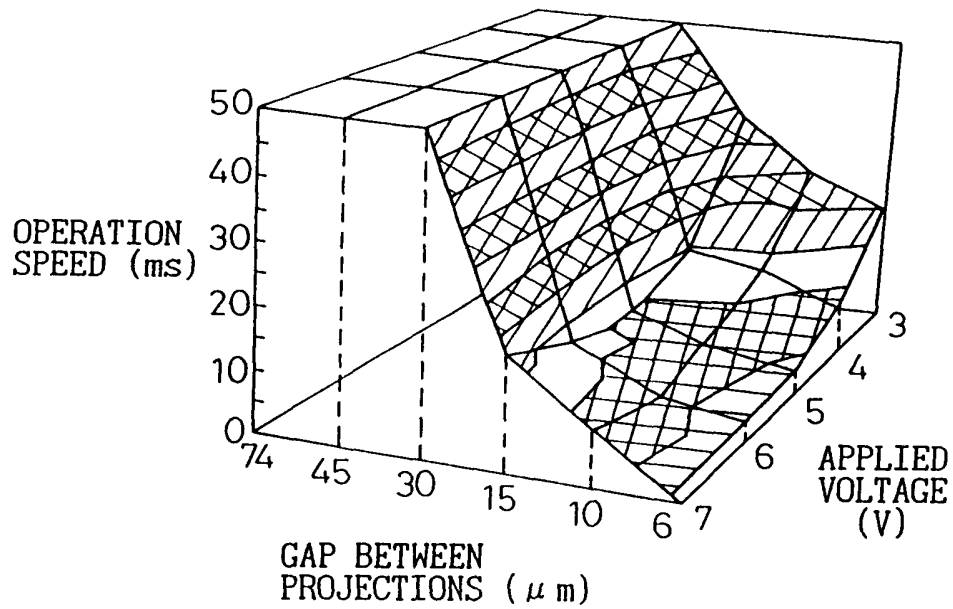
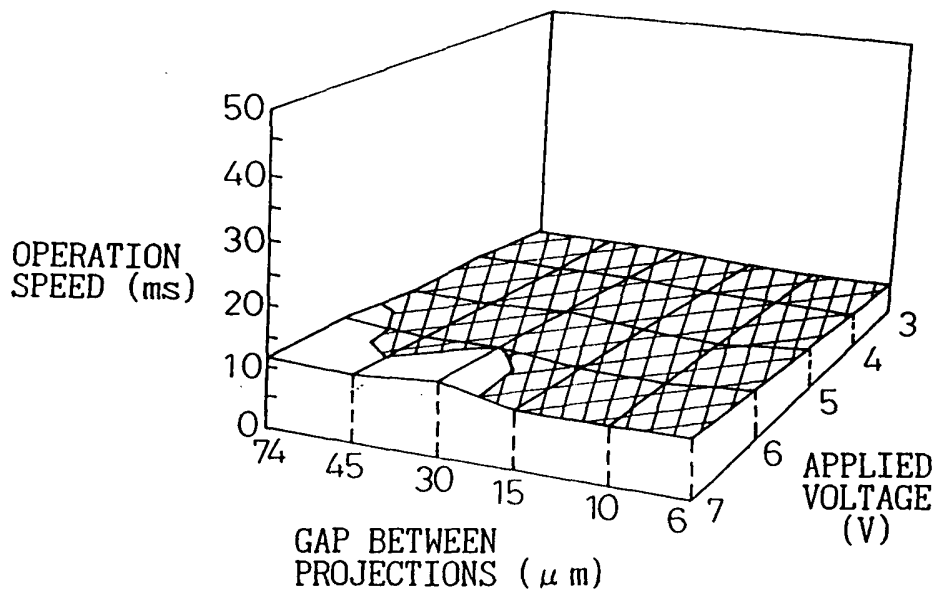


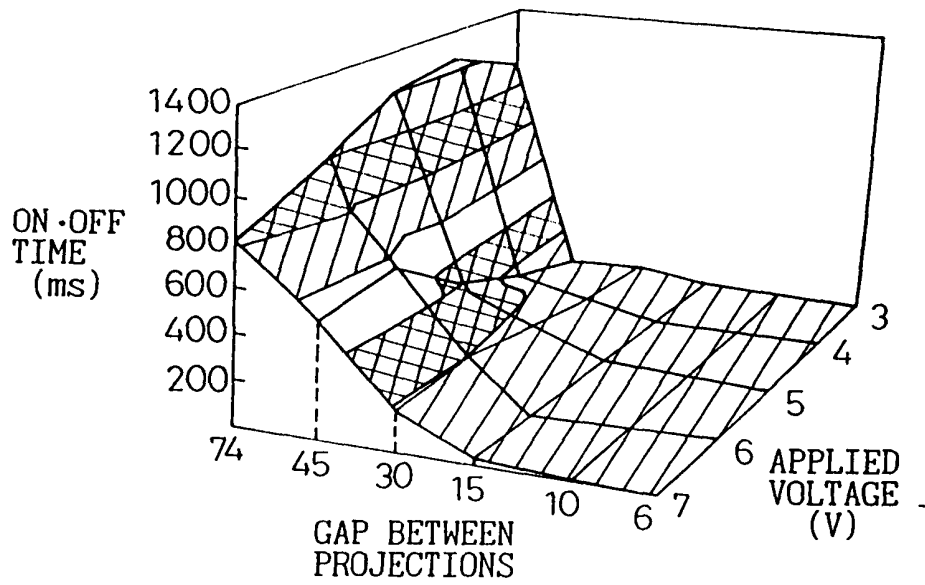
Fig.20B

OFF RESPONSE SPEED



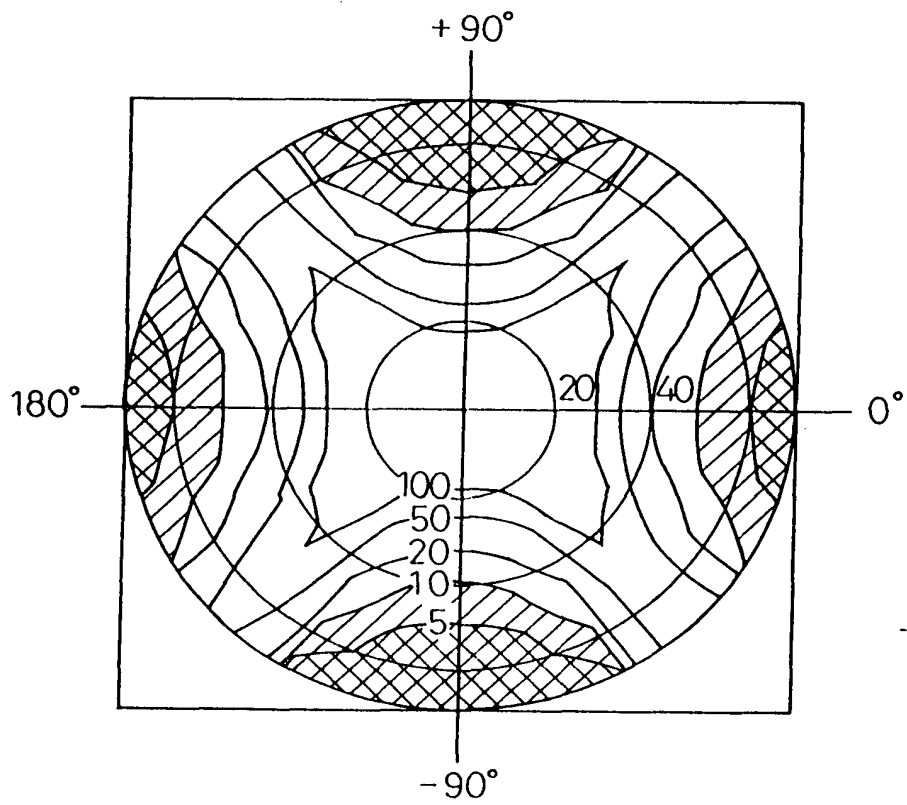
21/246

Fig. 21



22/246

Fig. 22



23/  
246

Fig.23A

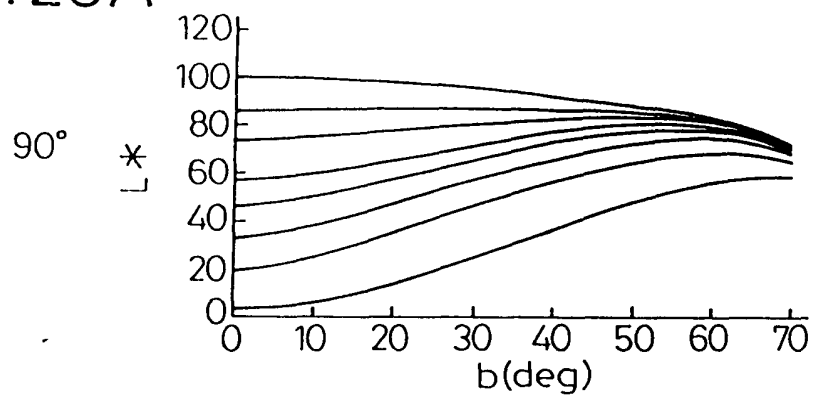


Fig.23B

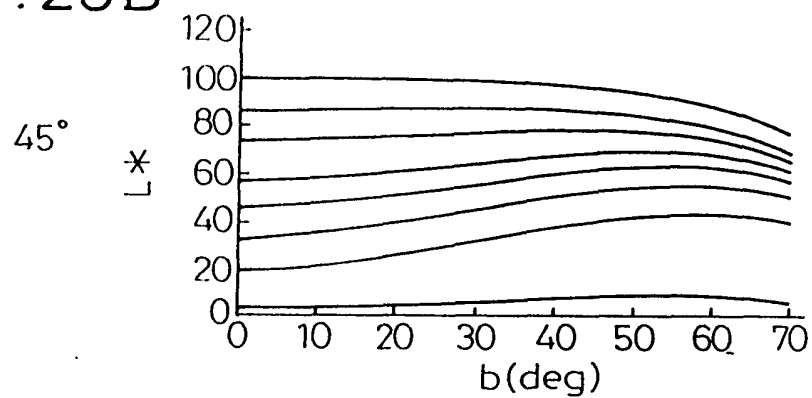
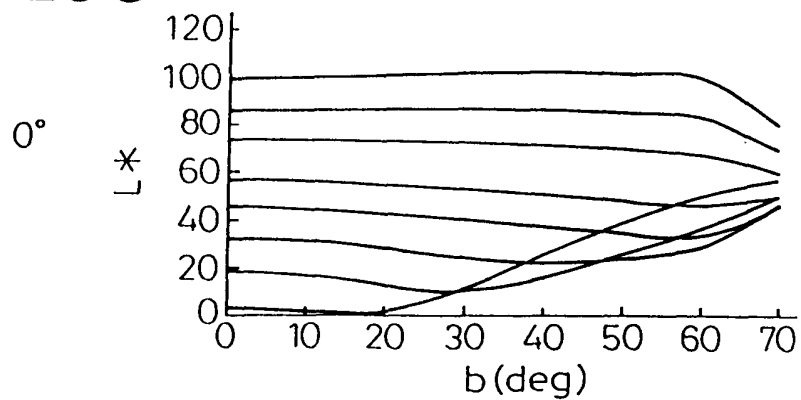
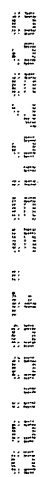
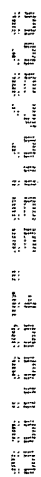


Fig.23C

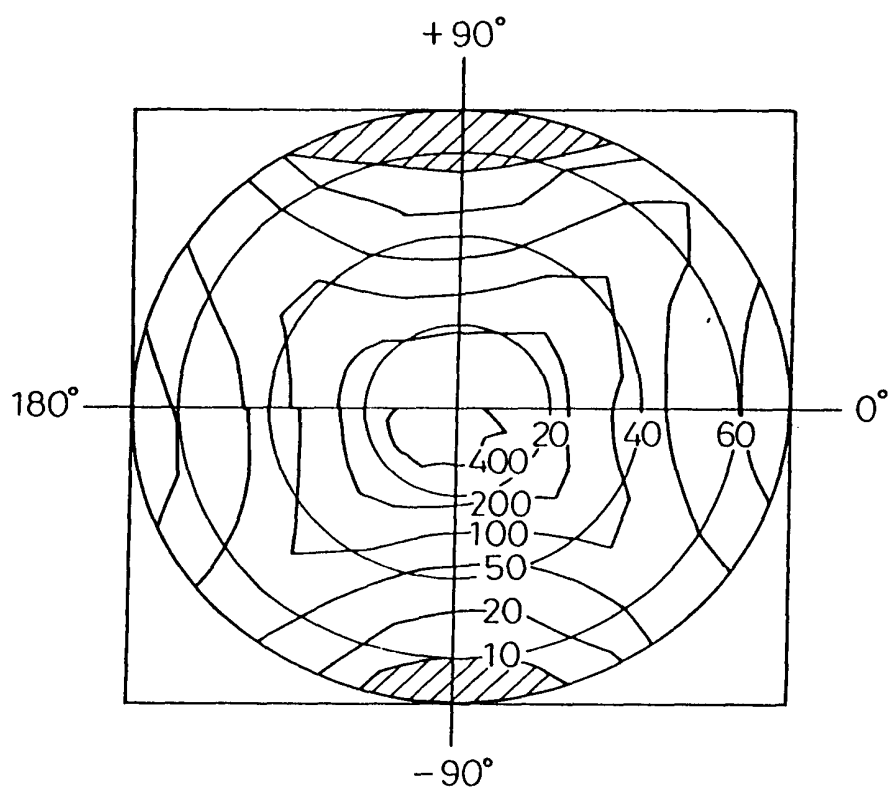


[illegible][illegible][illegible][illegible]



25/  
246

Fig. 25



26/  
246

Fig.26A

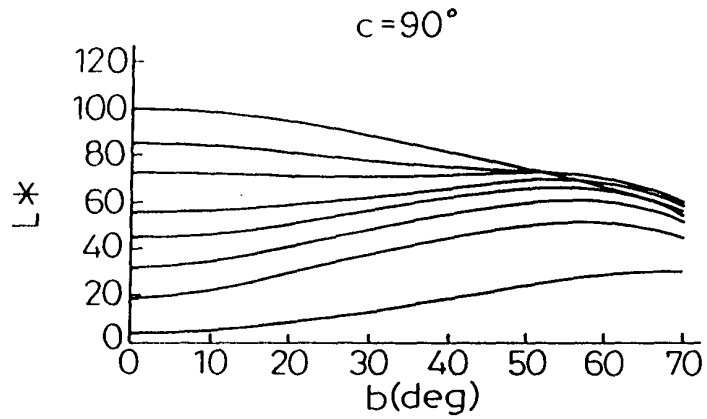


Fig.26B

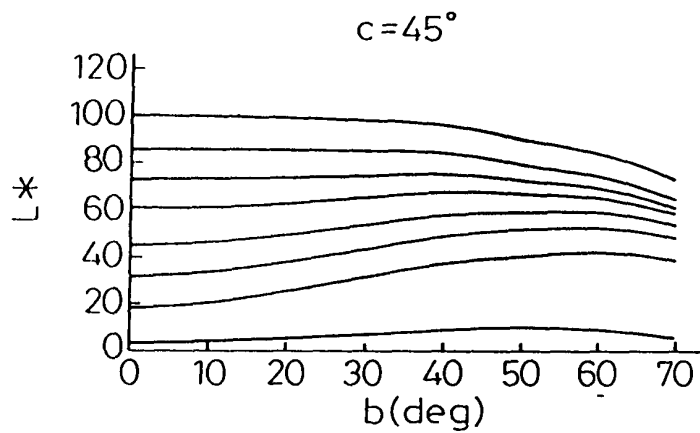
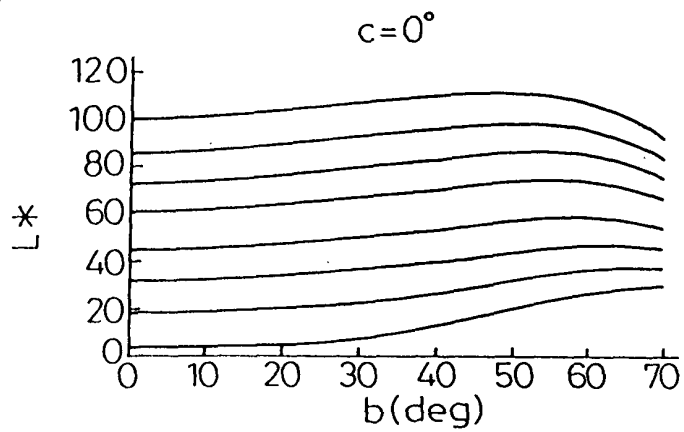
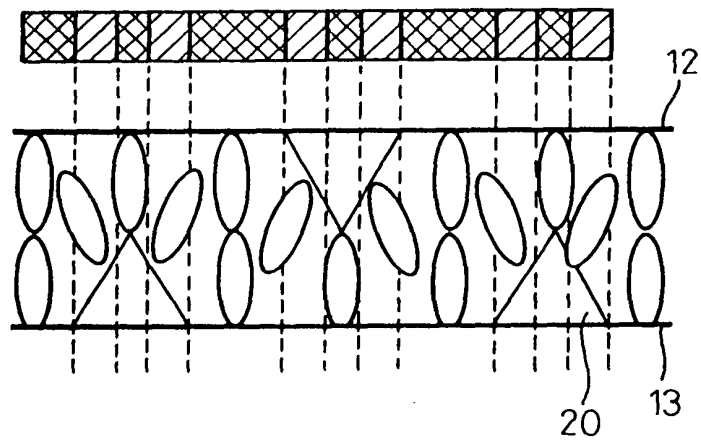


Fig.26C



27/246

Fig. 27



28/246

Fig. 28

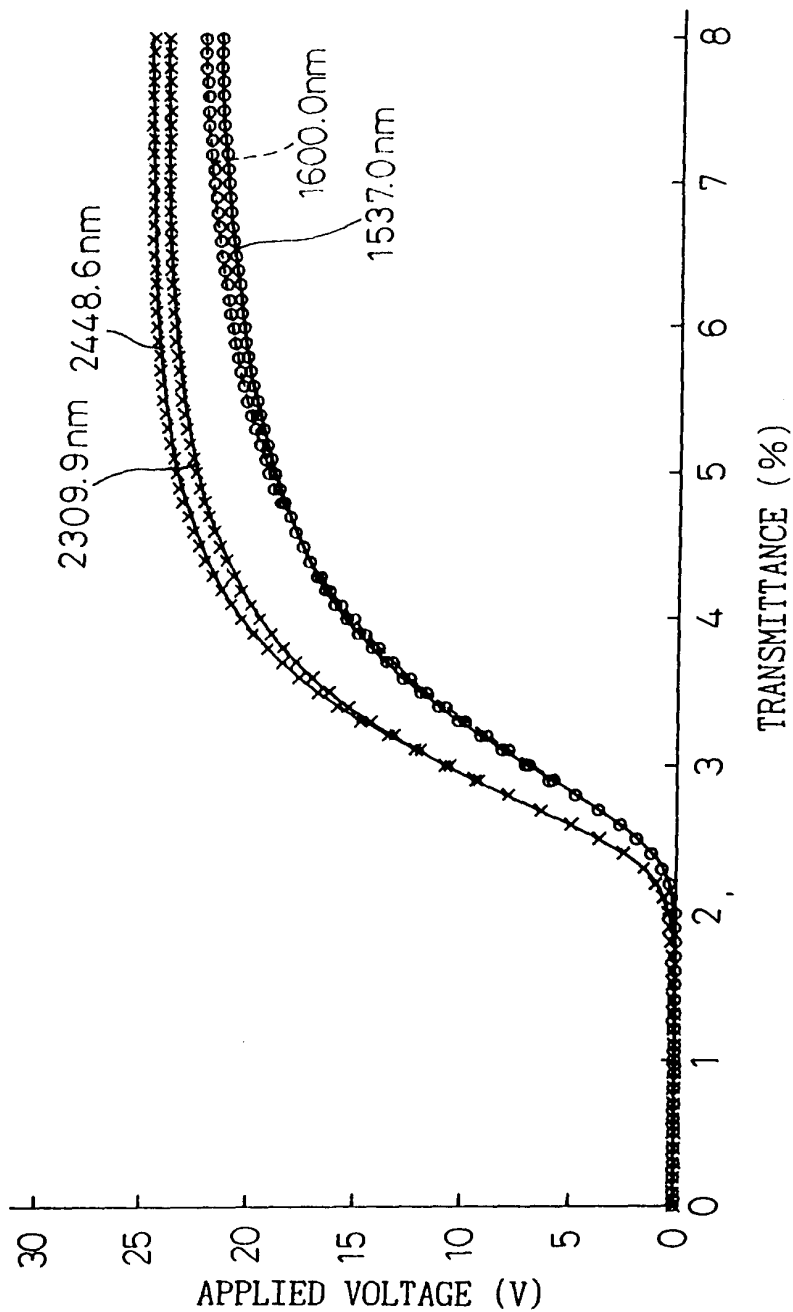
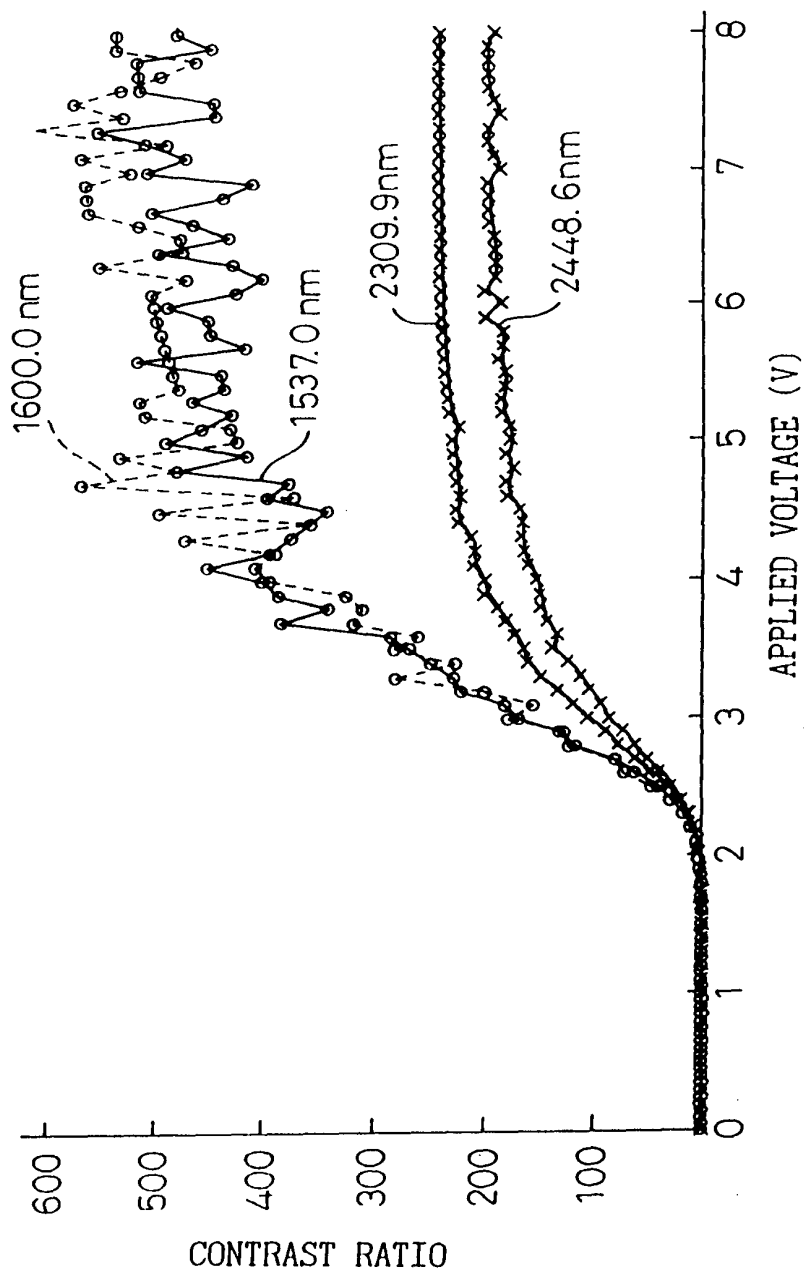


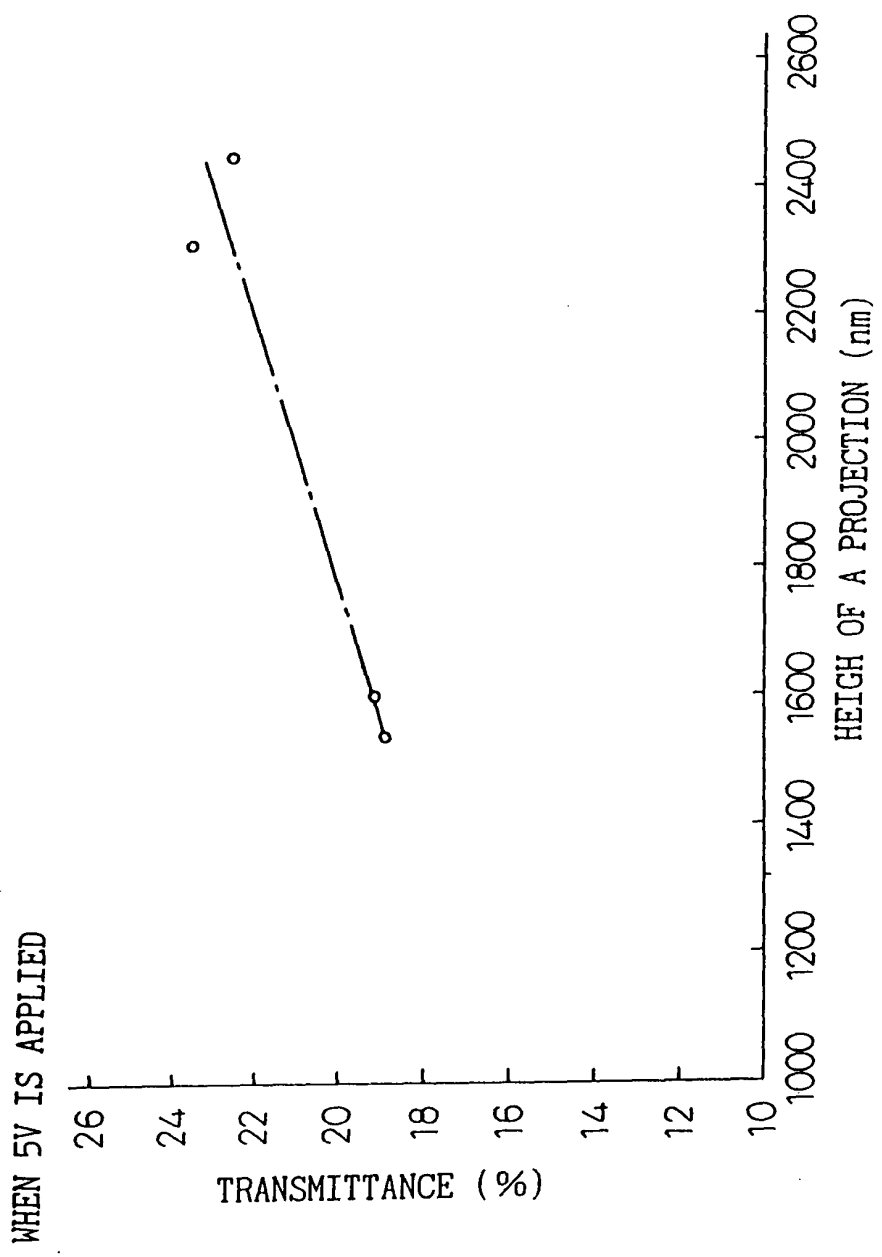
Fig. 29



30/246

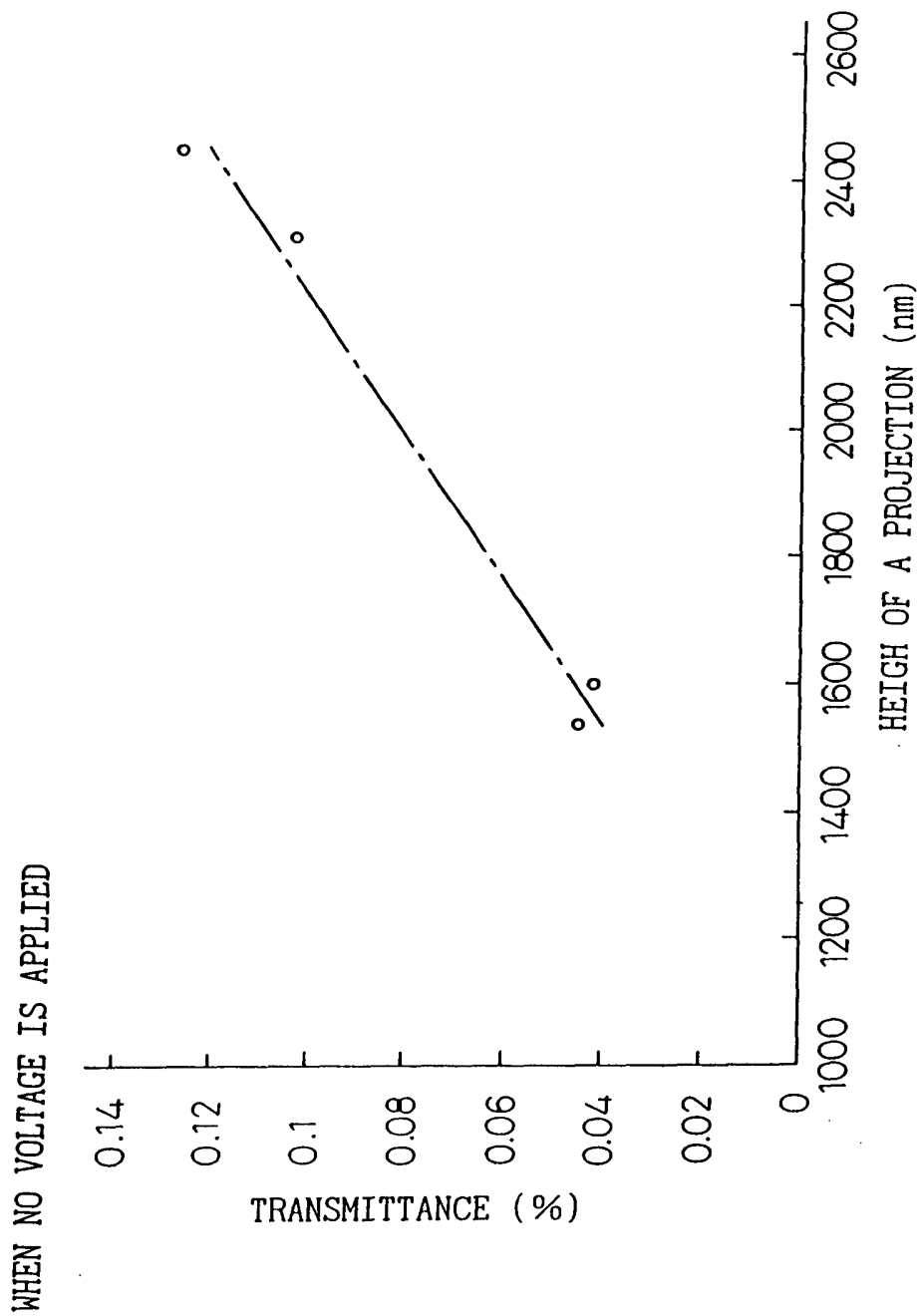
30/246

Fig.30



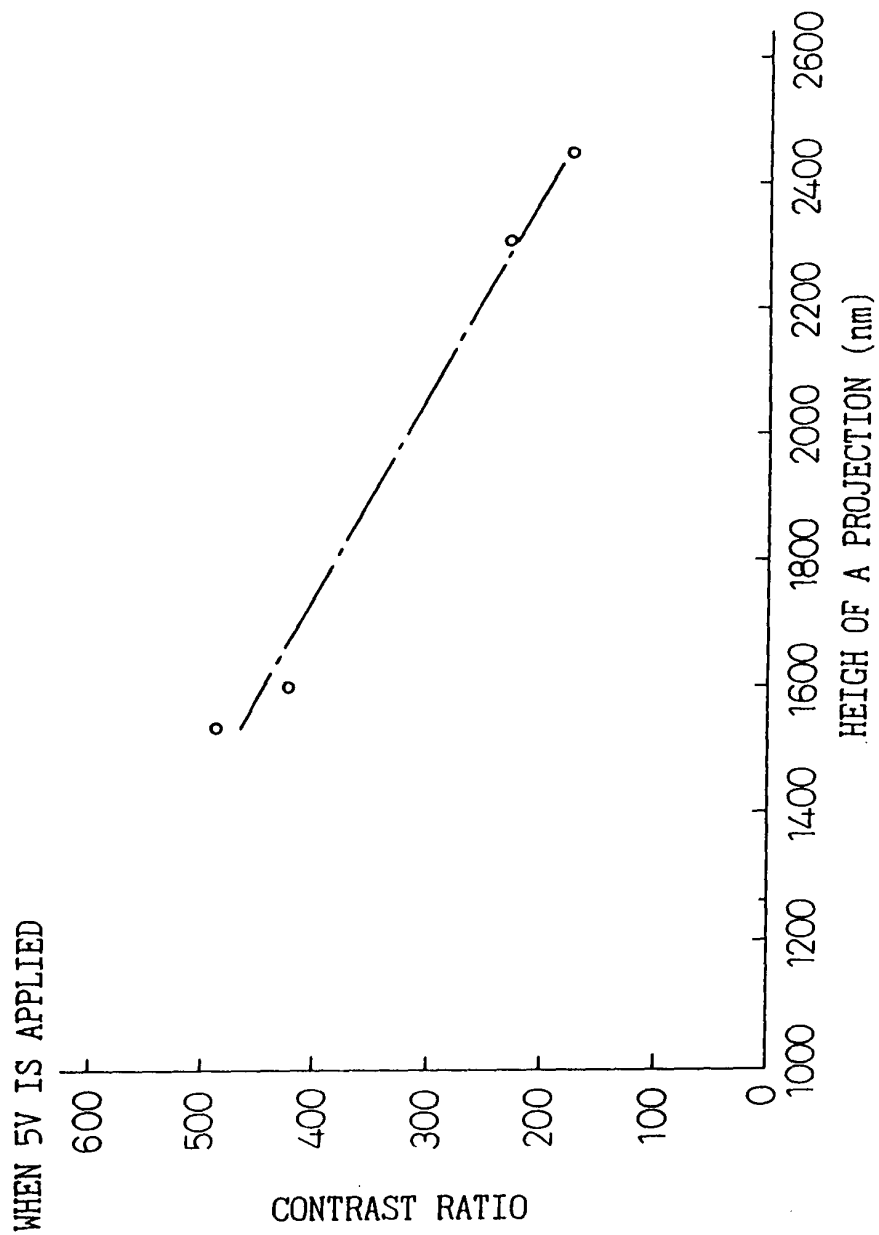
31/246

Fig. 31



1000 1200 1400 1600 1800 2000 2200 2400 2600

Fig. 32

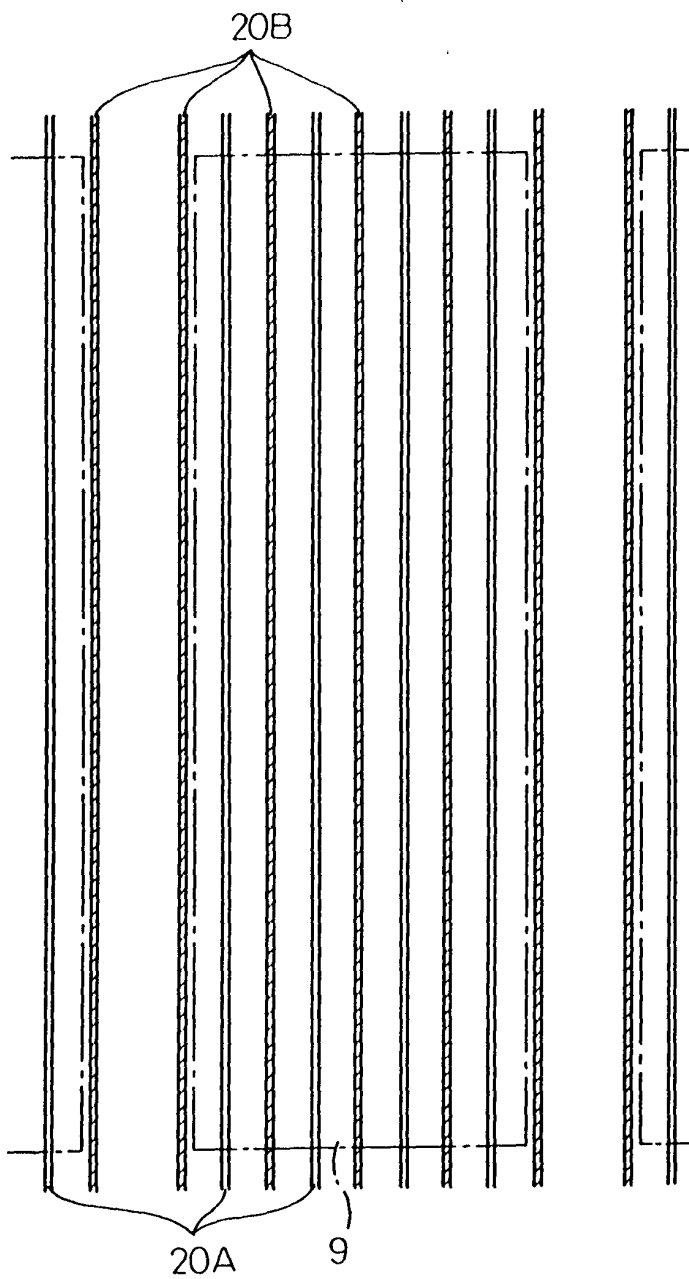


32/246



33/246

Fig. 33



34/  
246

Fig. 34

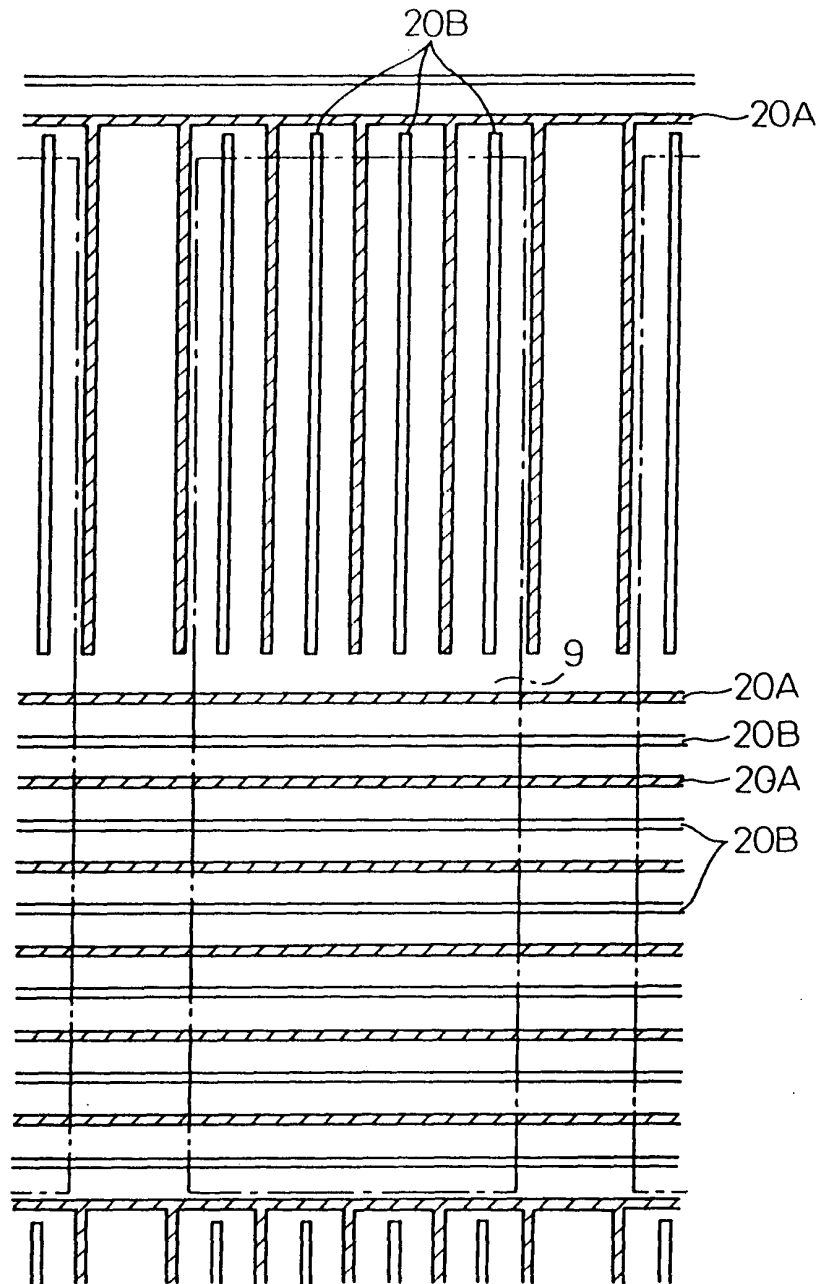
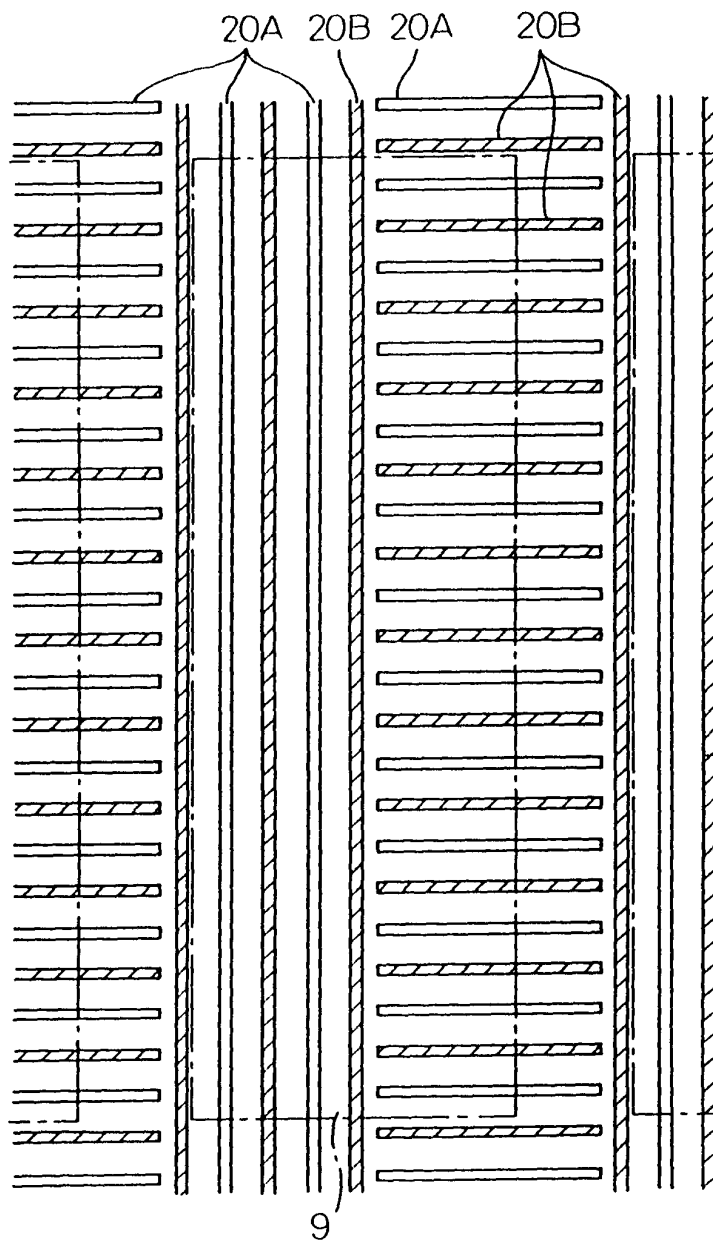


Fig. 35



36/246

Fig. 36

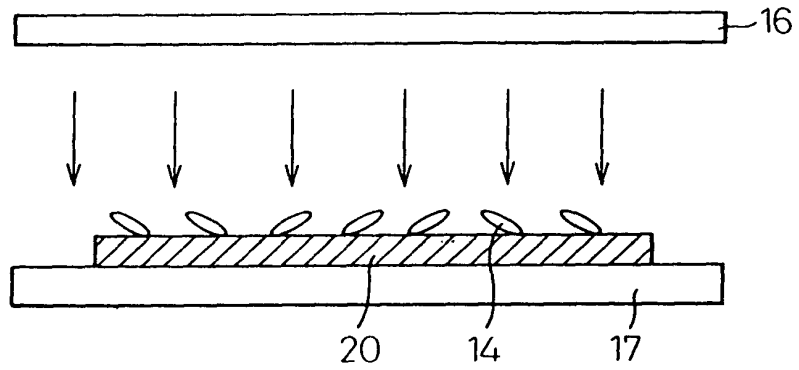


Fig. 37A

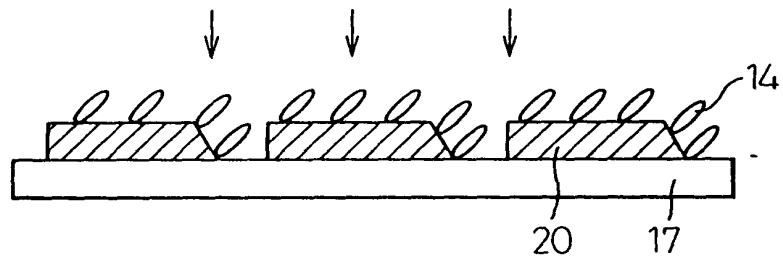


Fig. 37B

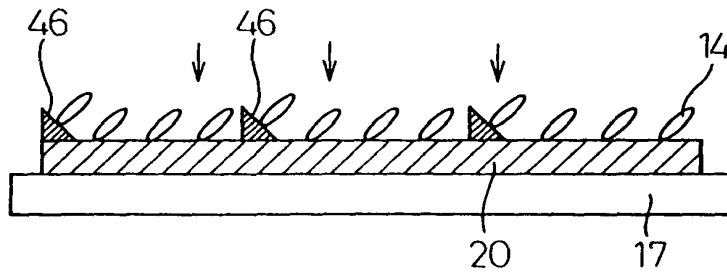


Fig.38A

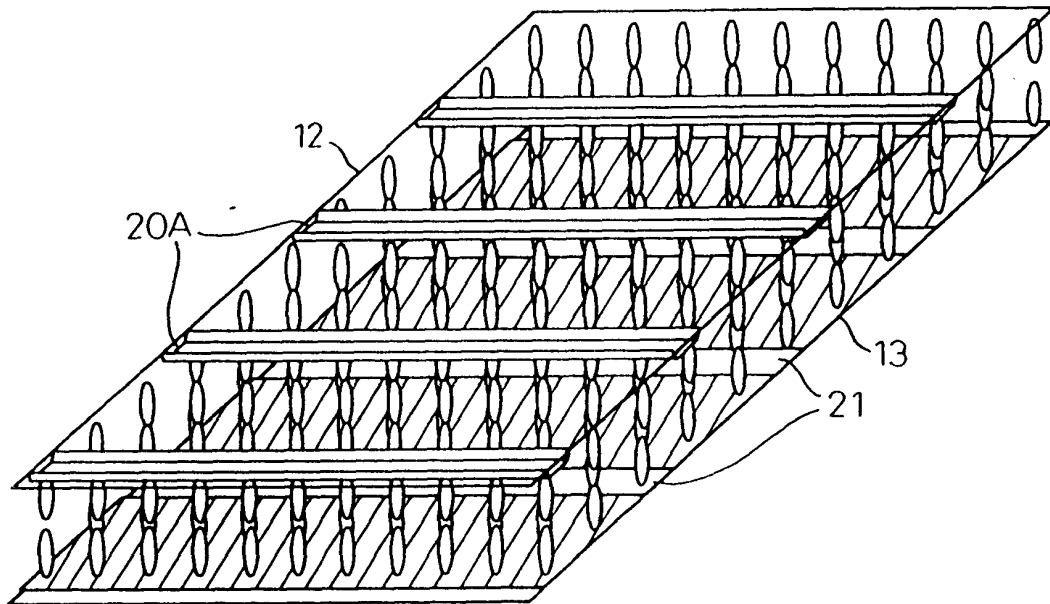


Fig.38B

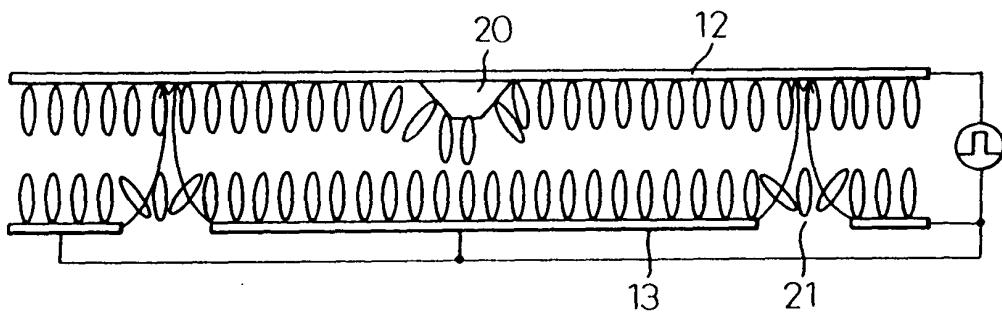


Fig.39

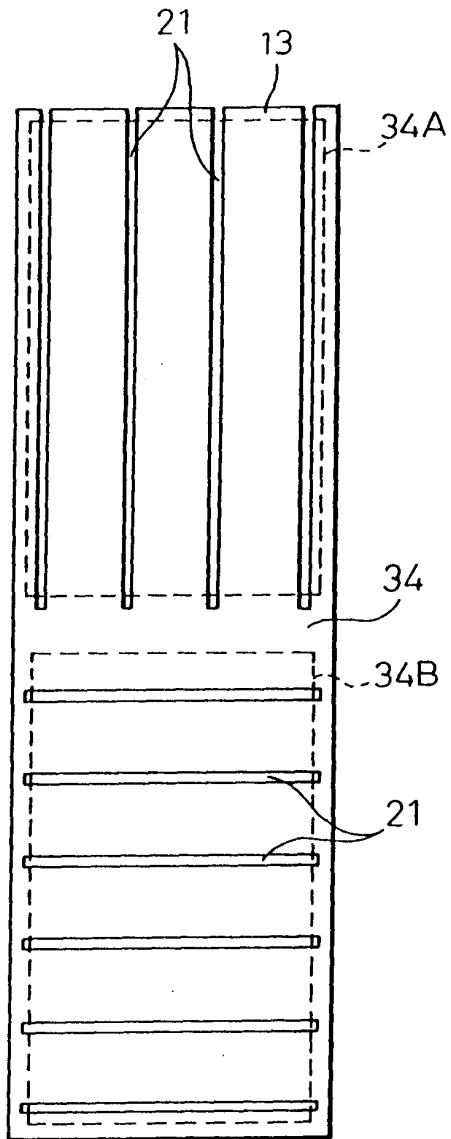


Fig.40

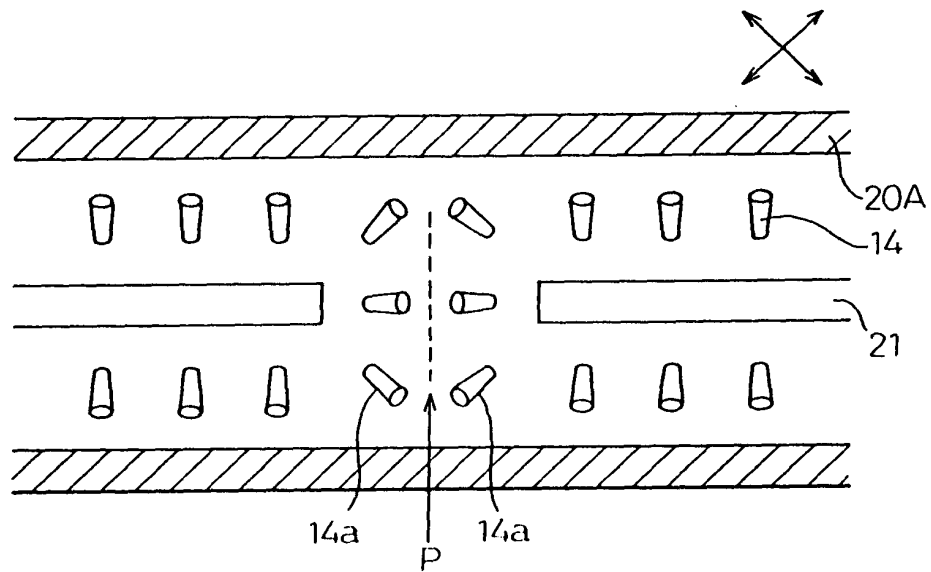


Fig.41

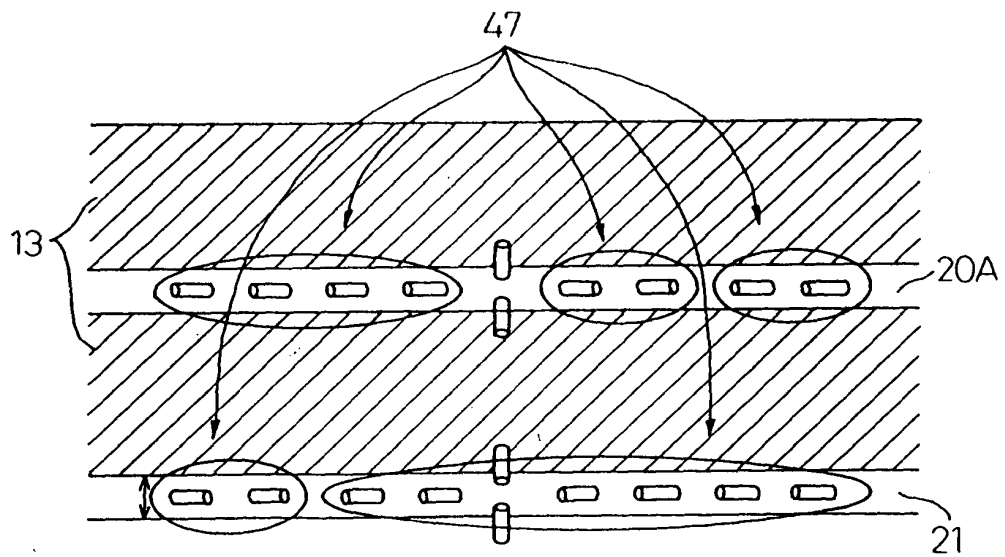
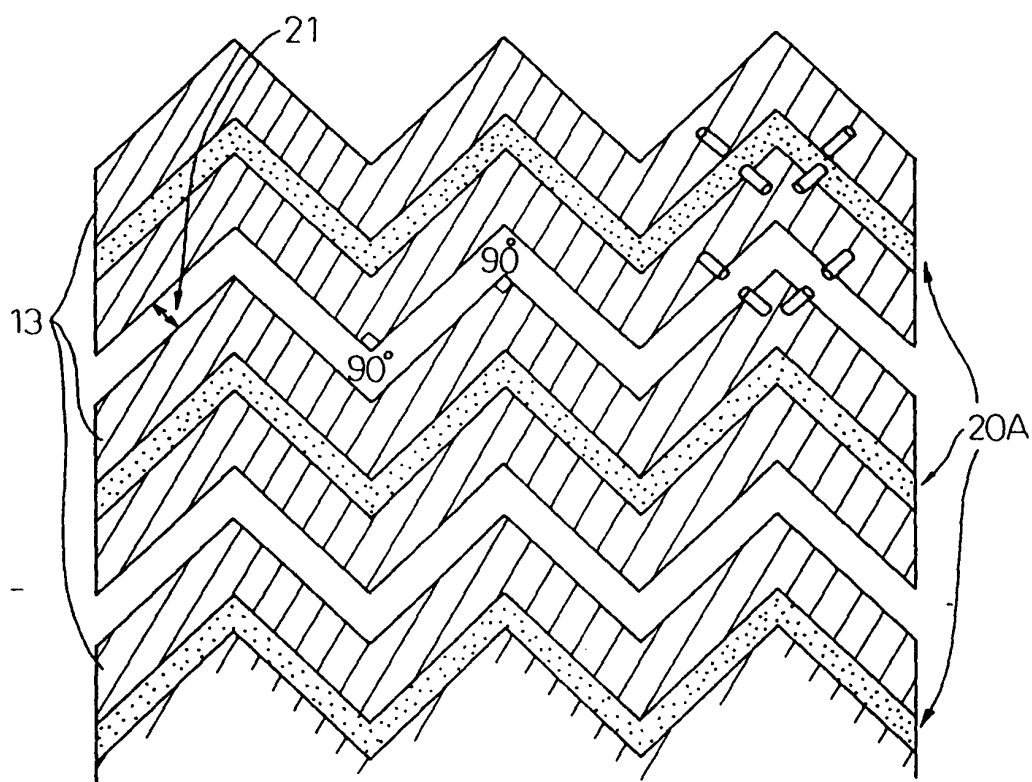


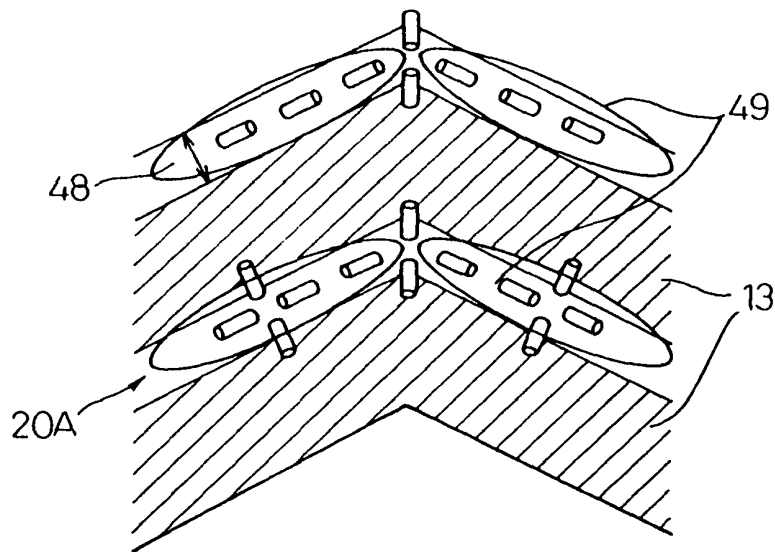
Fig. 42





41/246

Fig. 43



42/  
246

Fig. 44

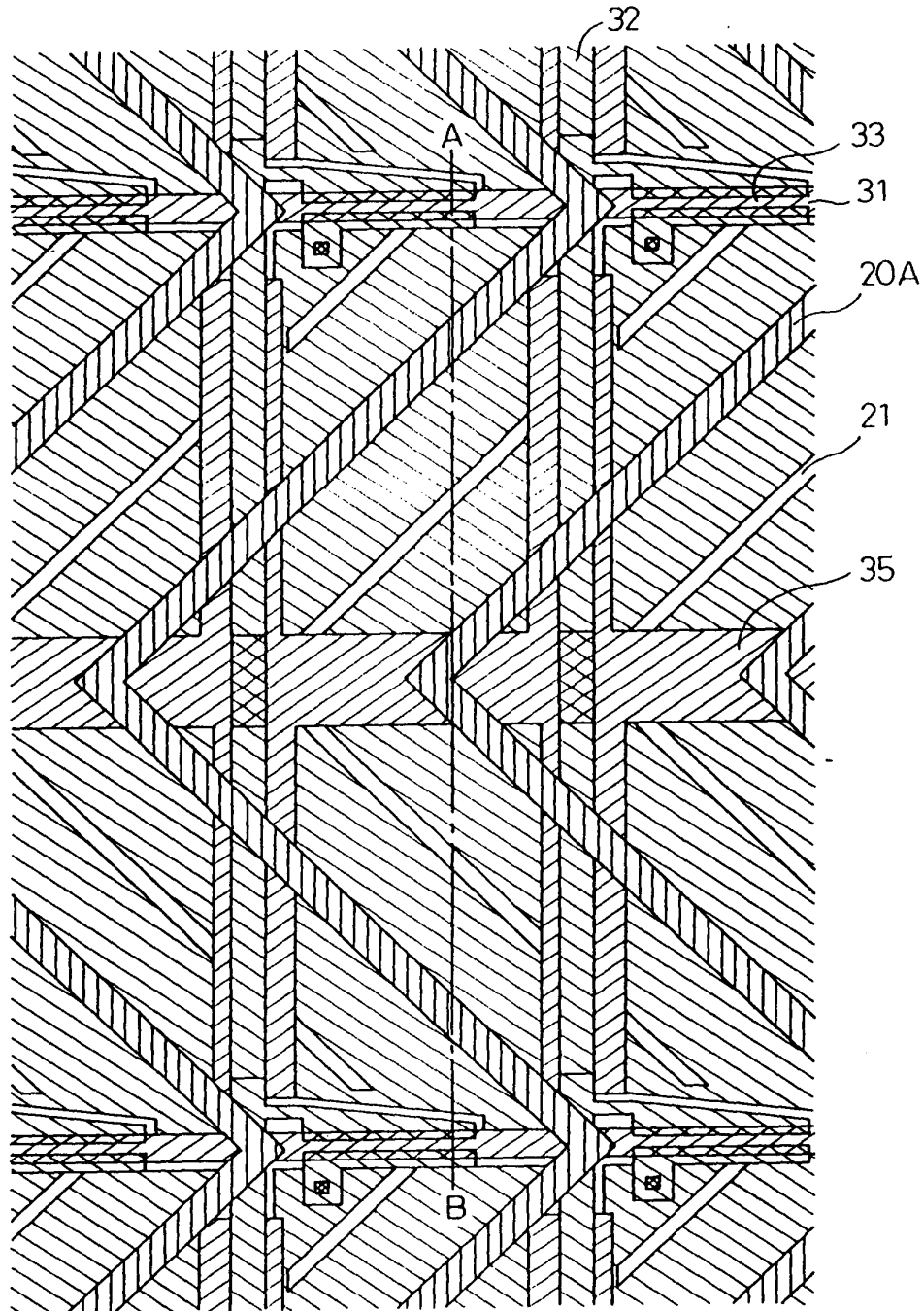


Fig. 45

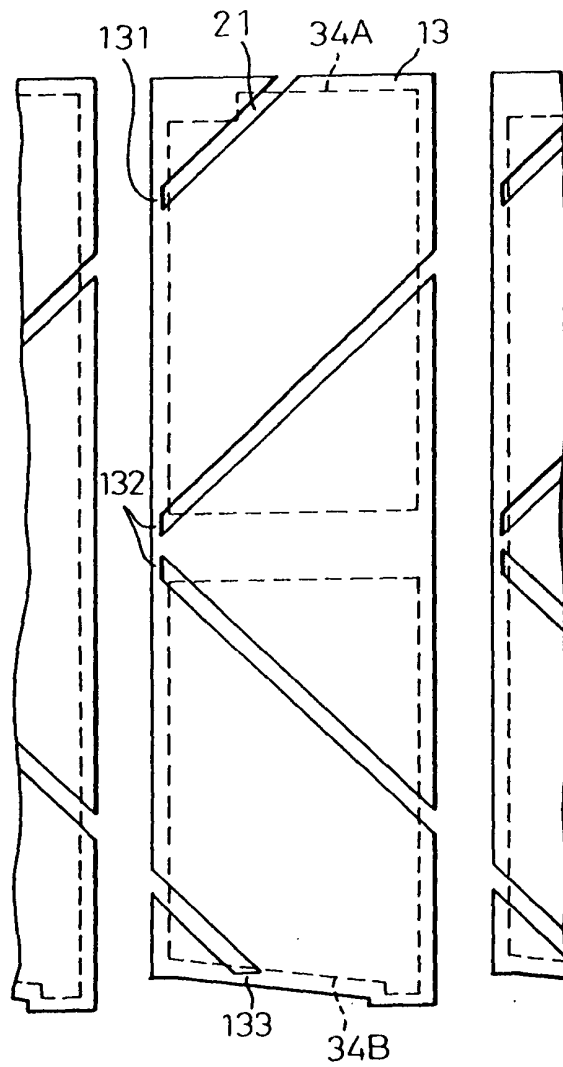
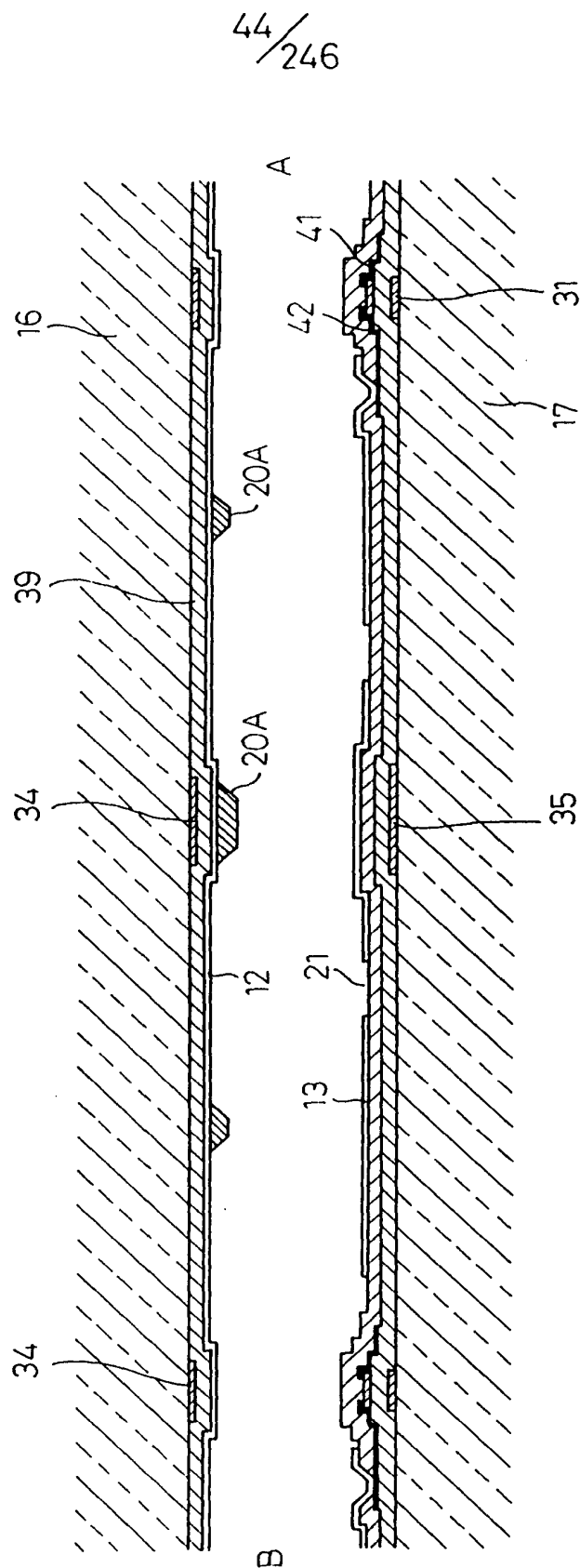
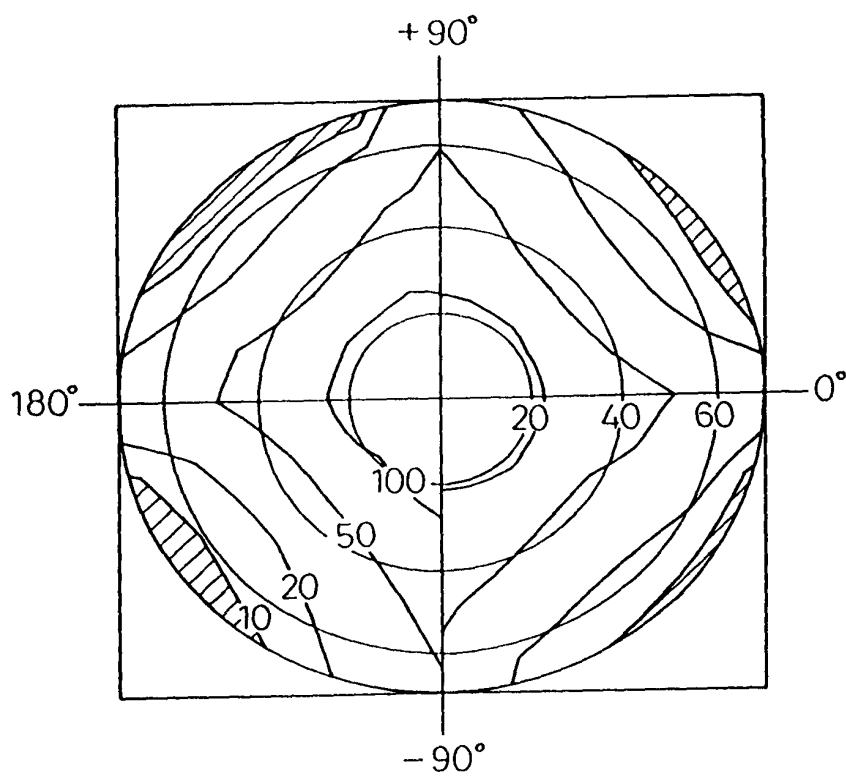


Fig. 46



45/246

Fig.47



46/  
246

Fig.48A

-90°

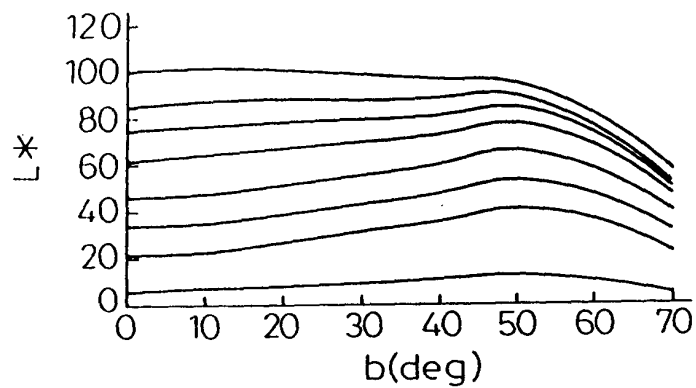


Fig.48B

-45°

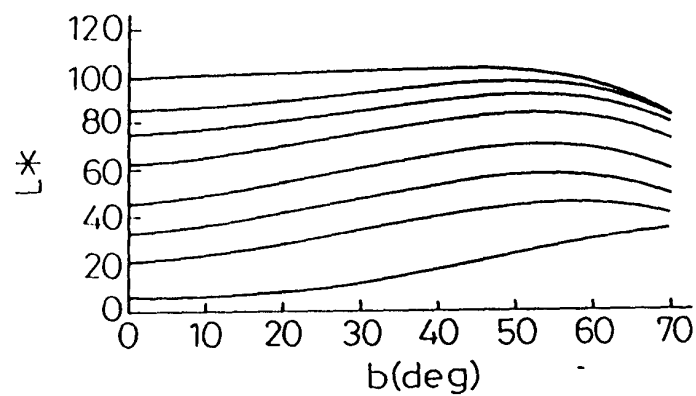


Fig.48C

0°

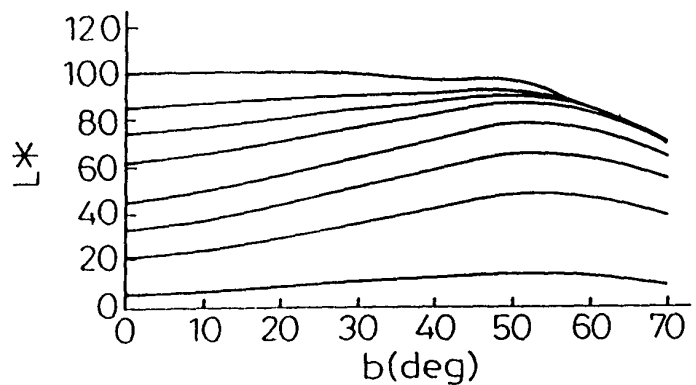


Fig.49A

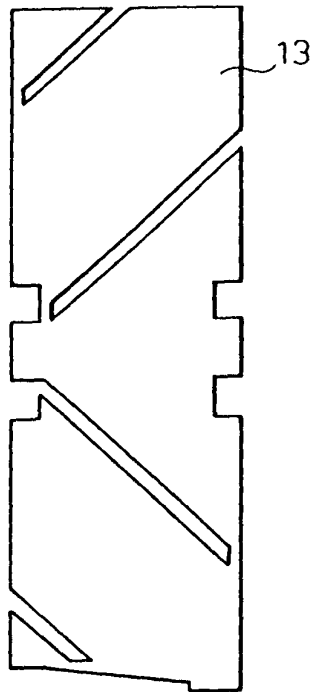


Fig.49B

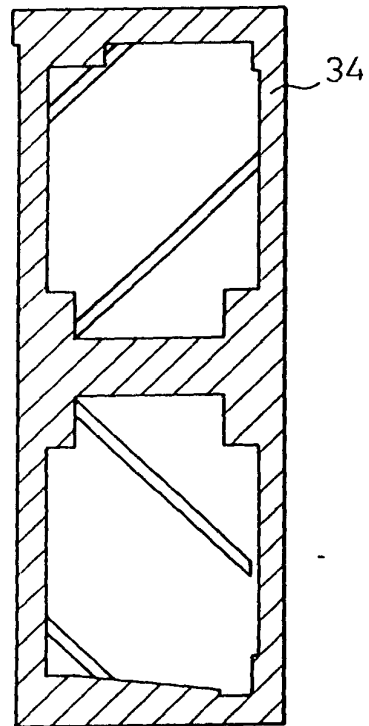


Fig.50A

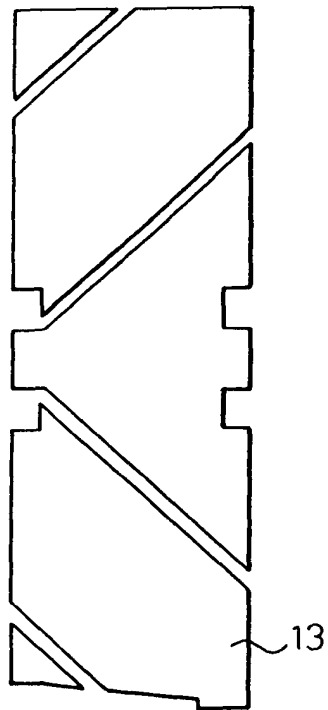
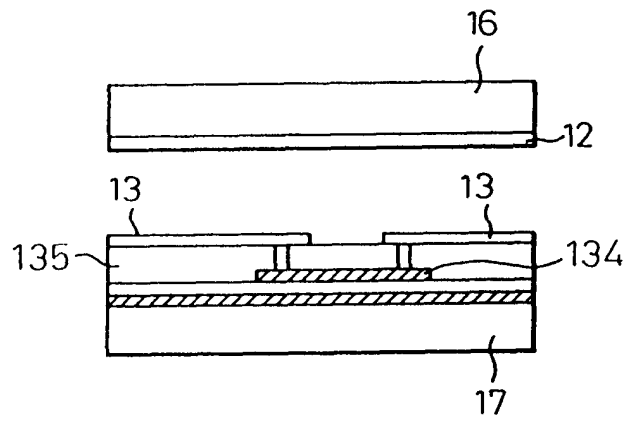


Fig.50B





49/246

Fig. 51

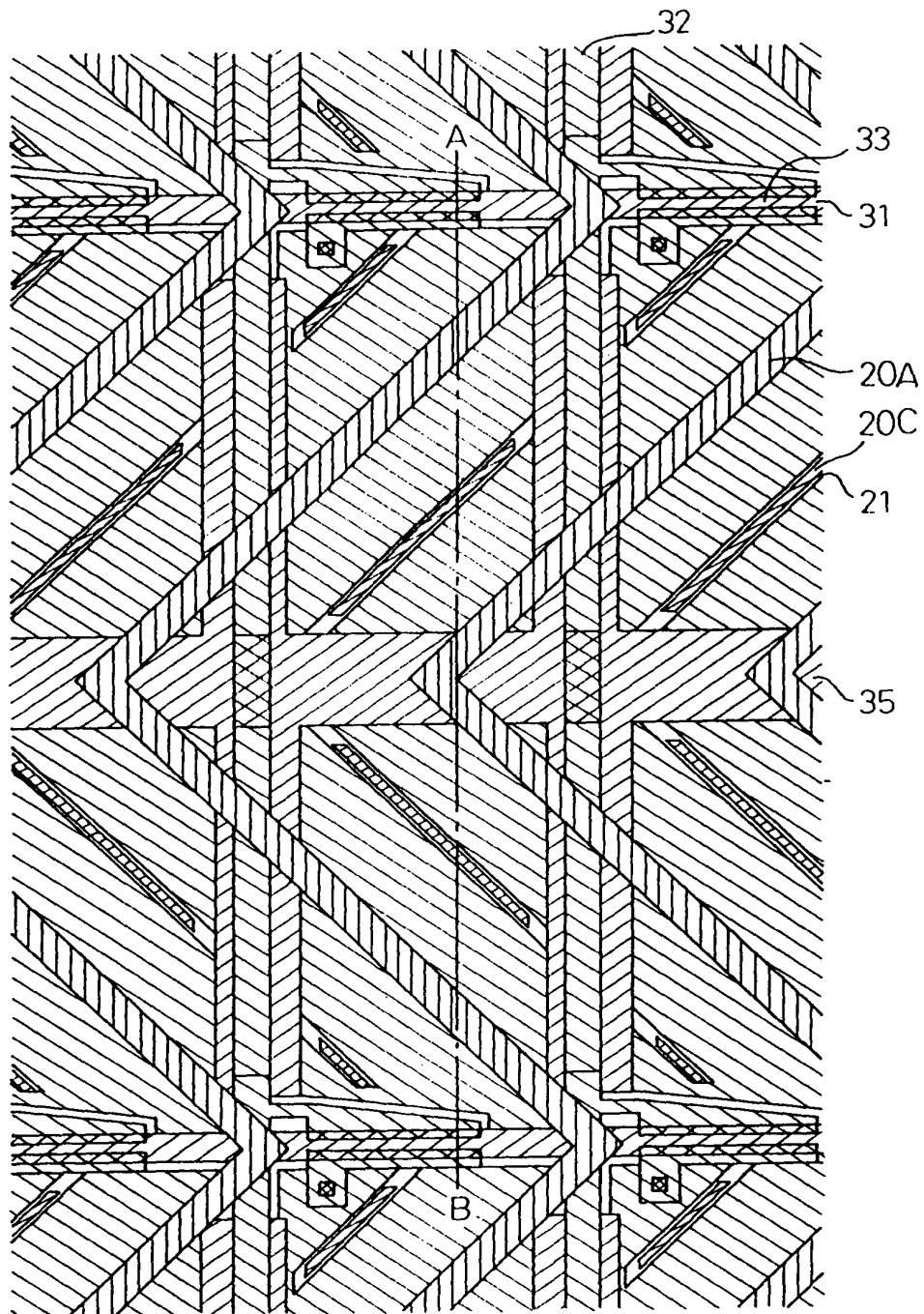
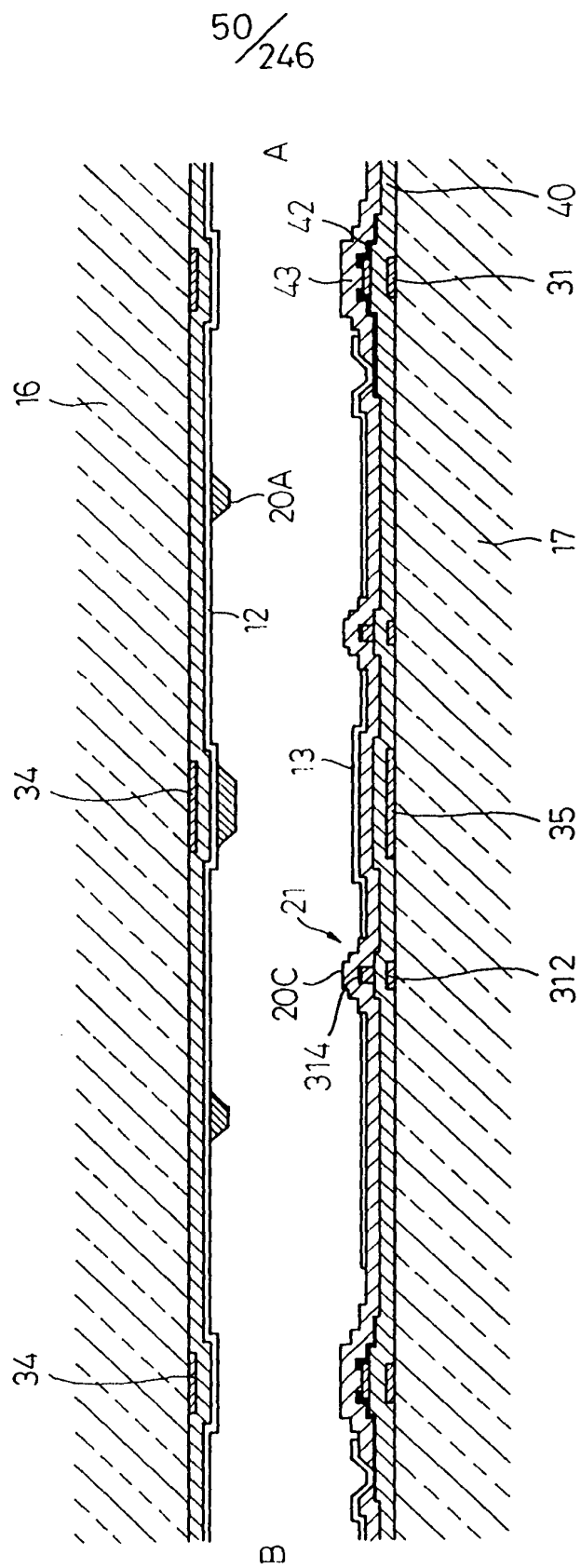


Fig. 52



51/246

Fig. 53A

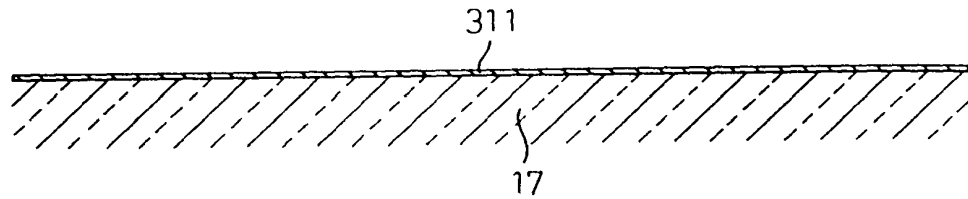


Fig. 53B

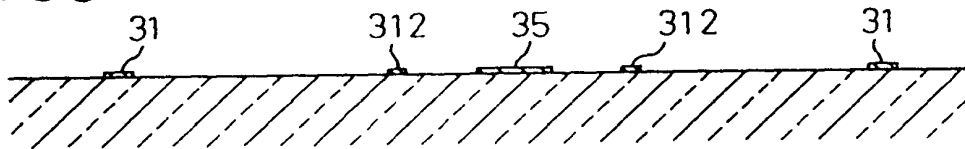


Fig. 53C

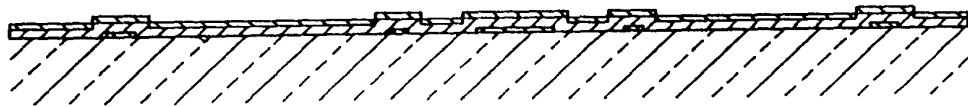


Fig. 53D

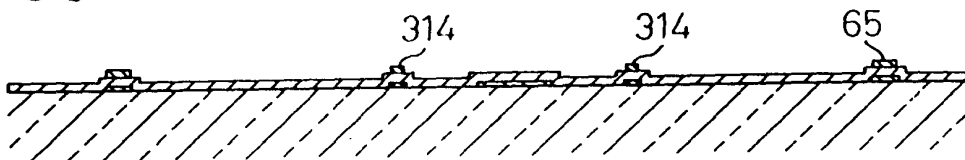


Fig. 53E

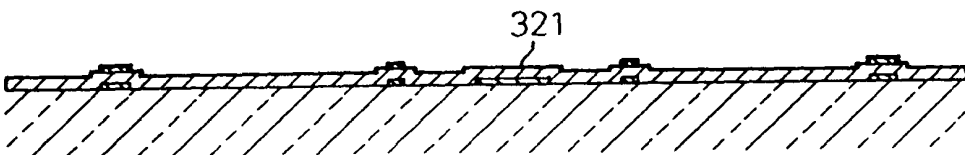


Fig. 53F

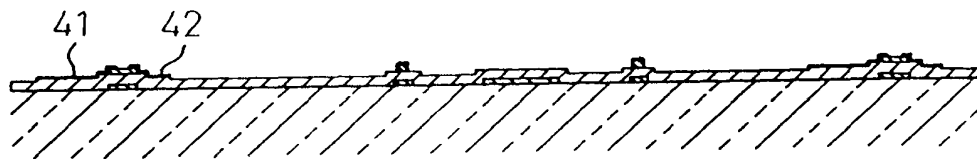


Fig. 53G

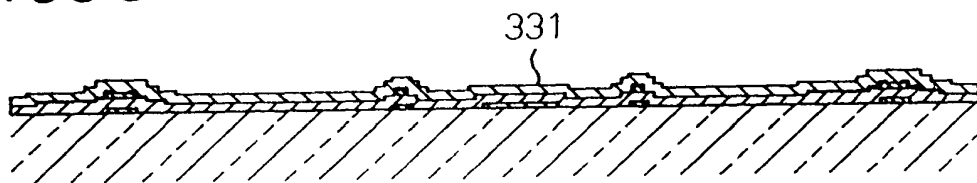


Fig. 53H

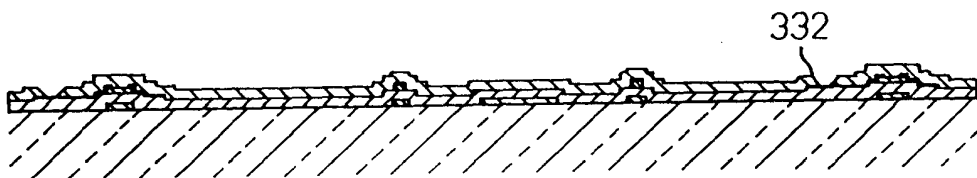


Fig. 53I

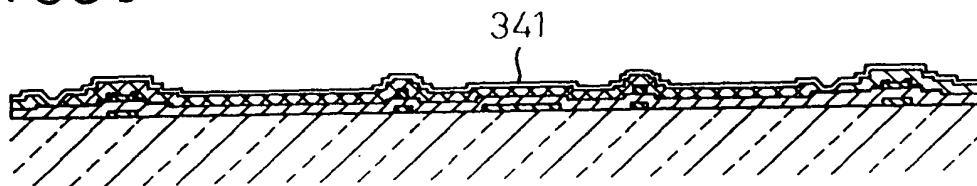


Fig. 53J

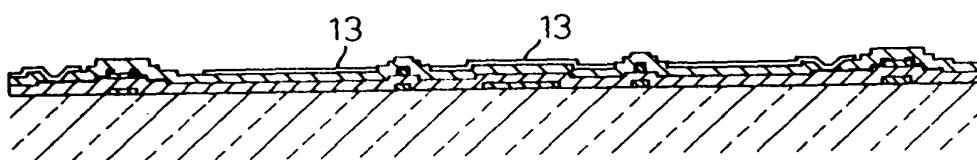
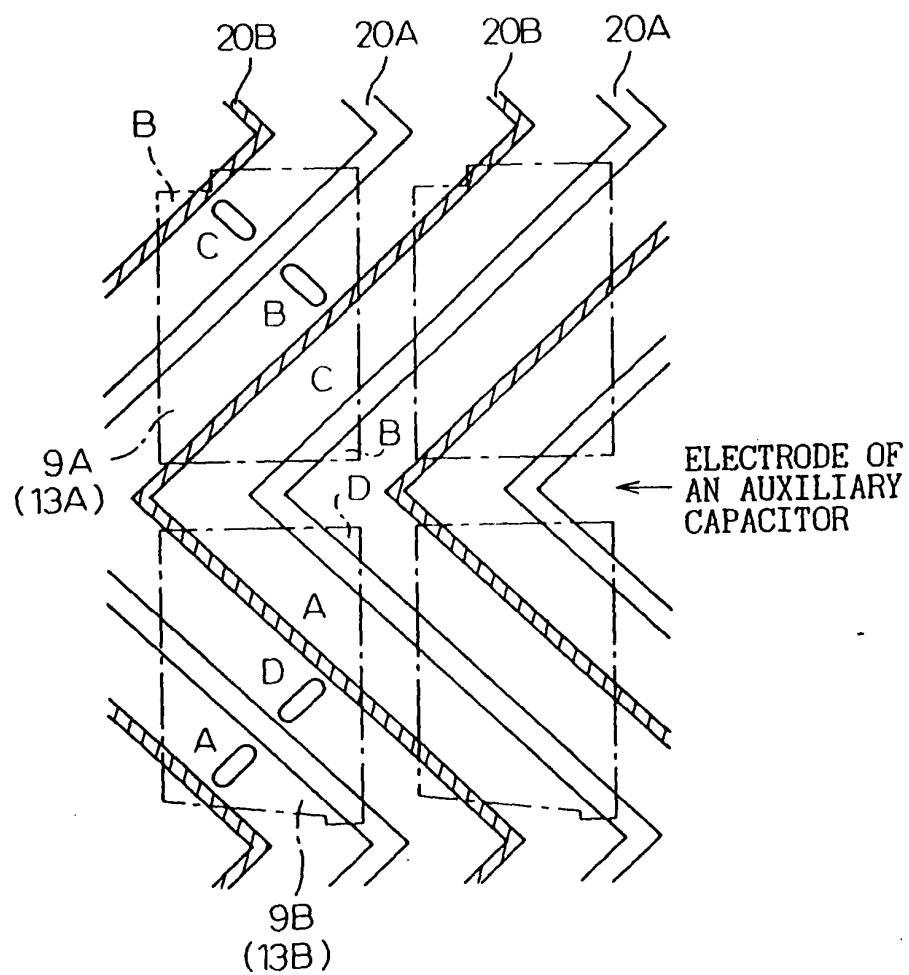
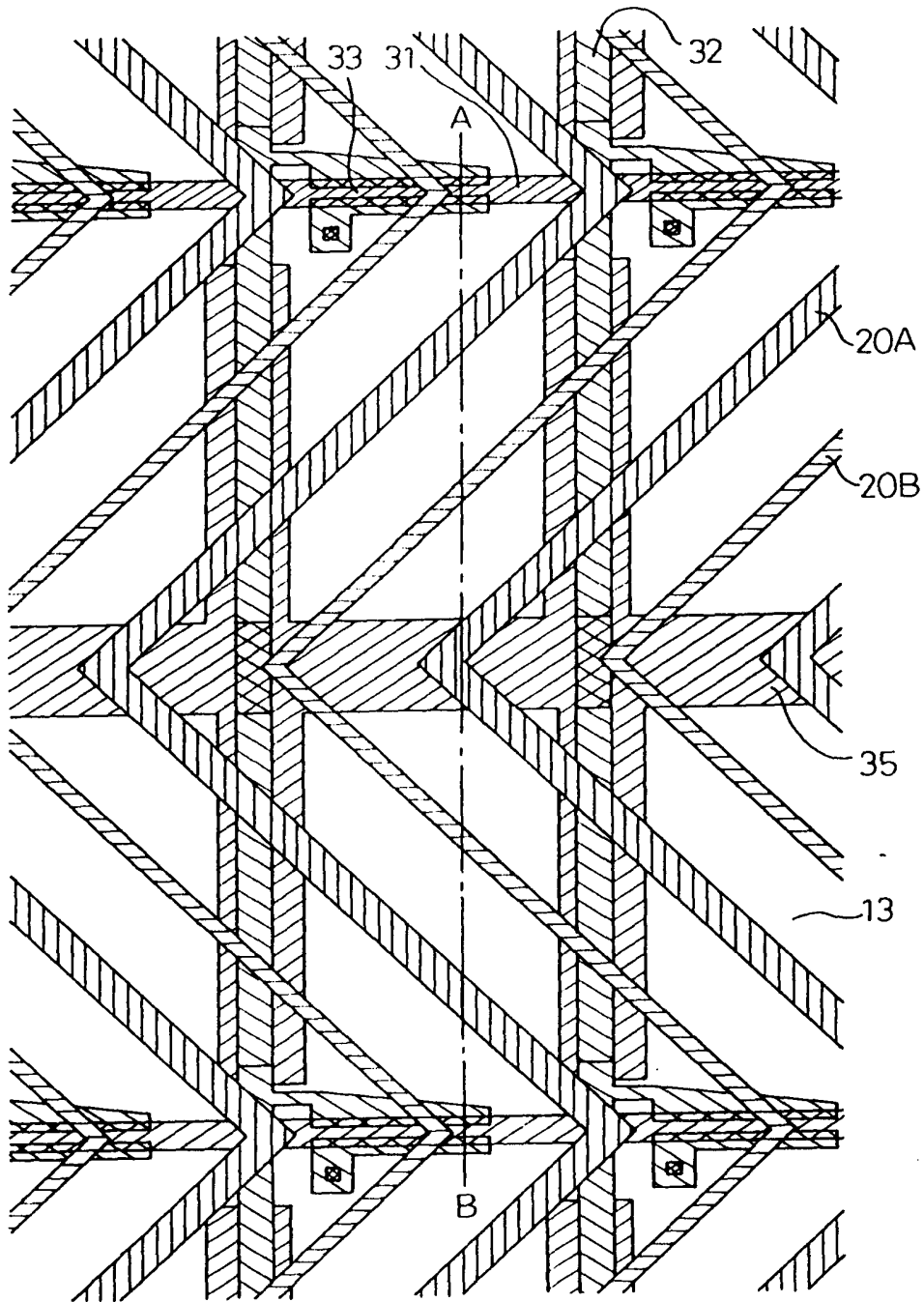


Fig. 54



54/246

Fig.55



55/  
246

Fig. 56

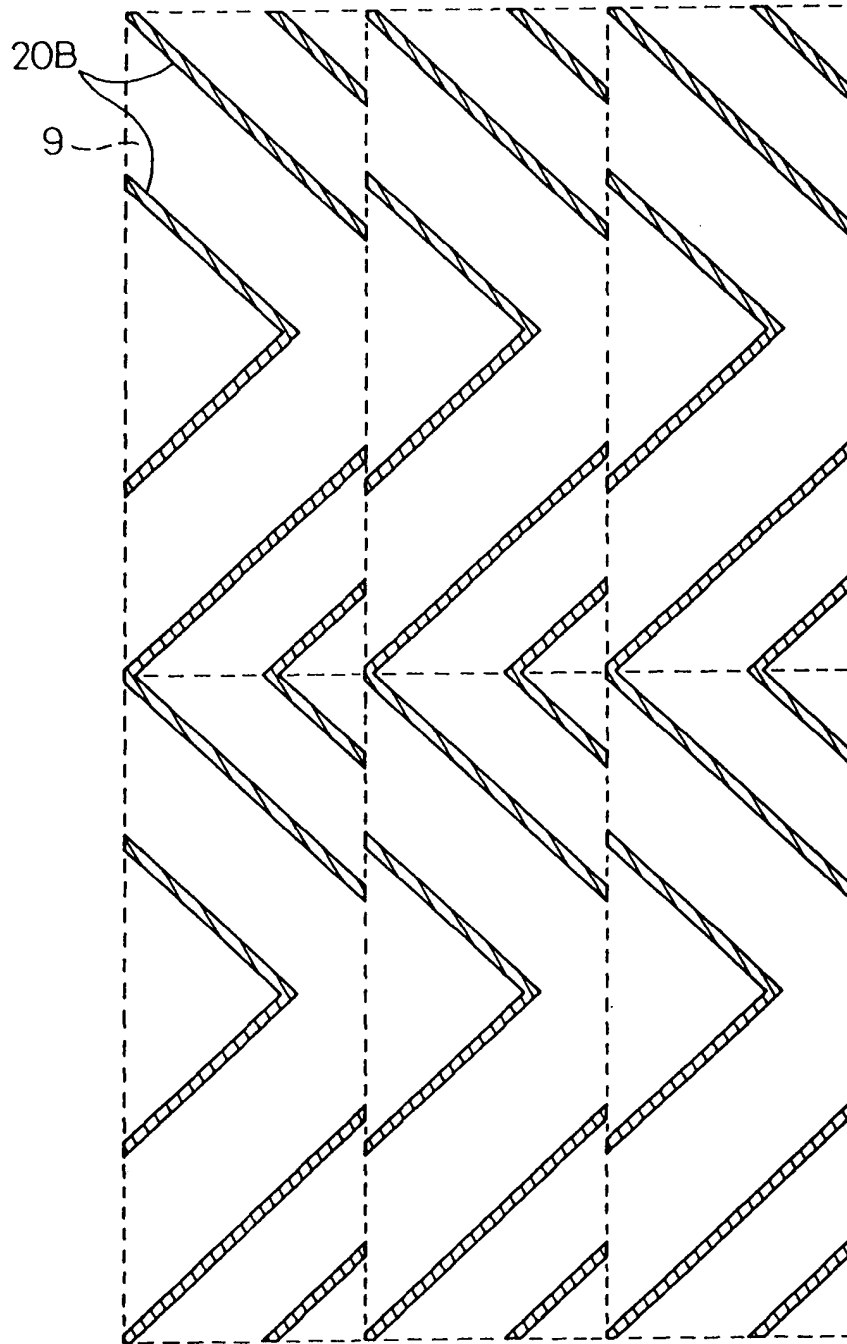


Fig. 57A

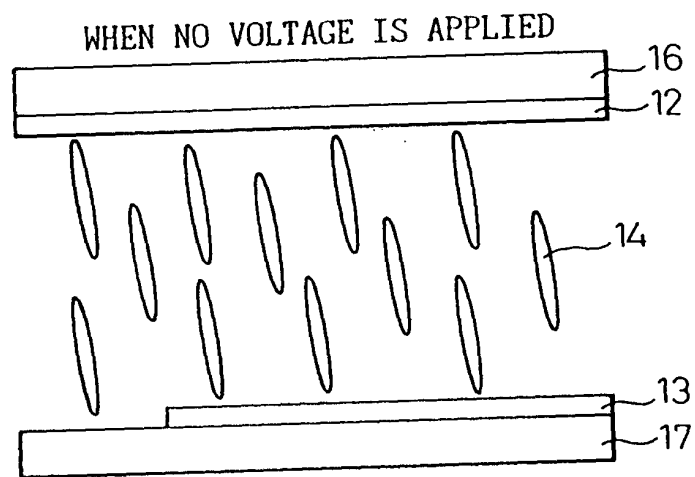


Fig. 57B

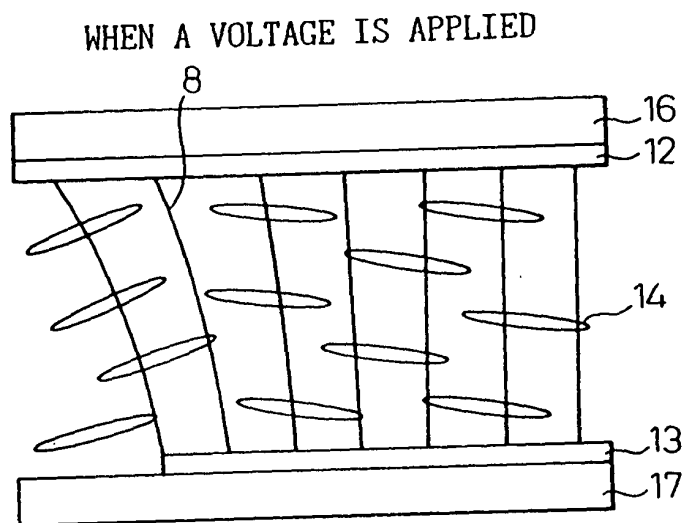




Fig. 58

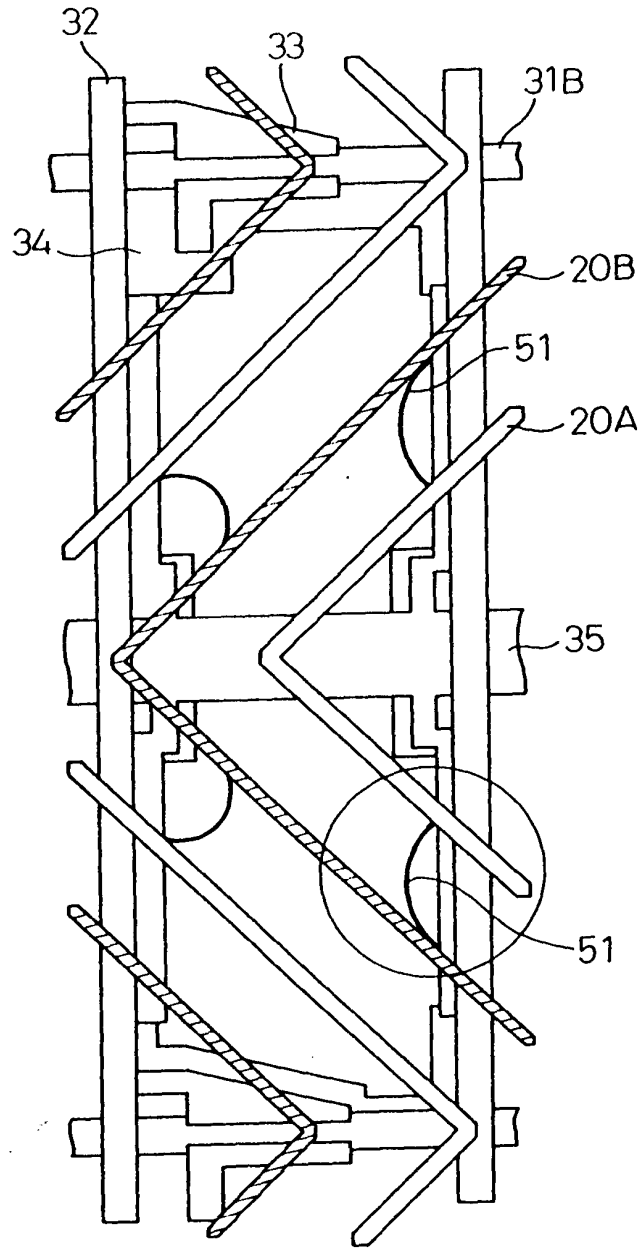


Fig. 59

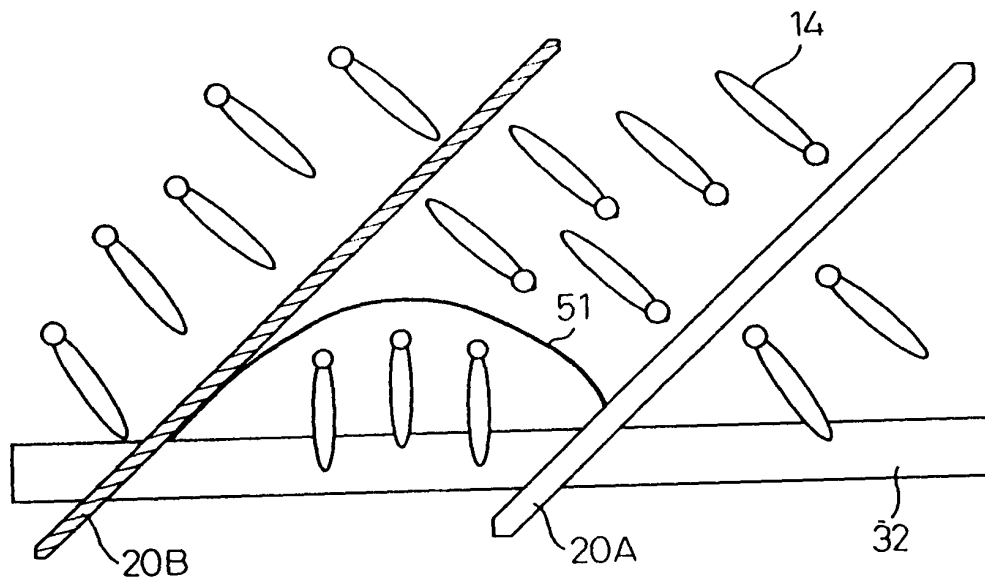
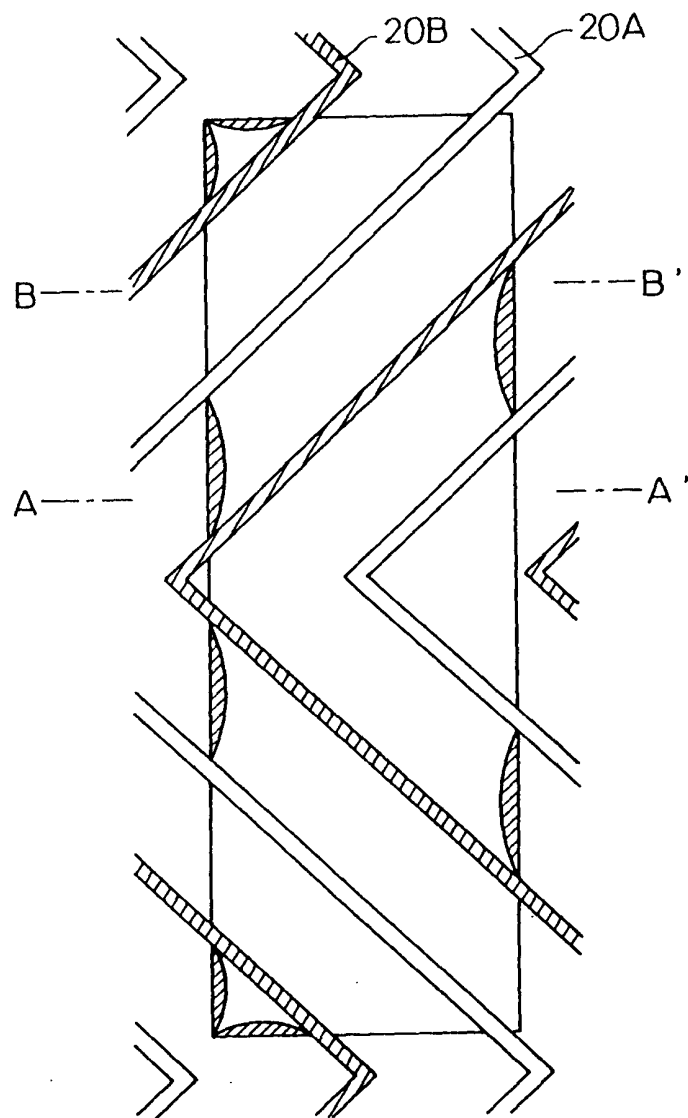


Fig. 60



60/246

Fig. 61A

A - A'

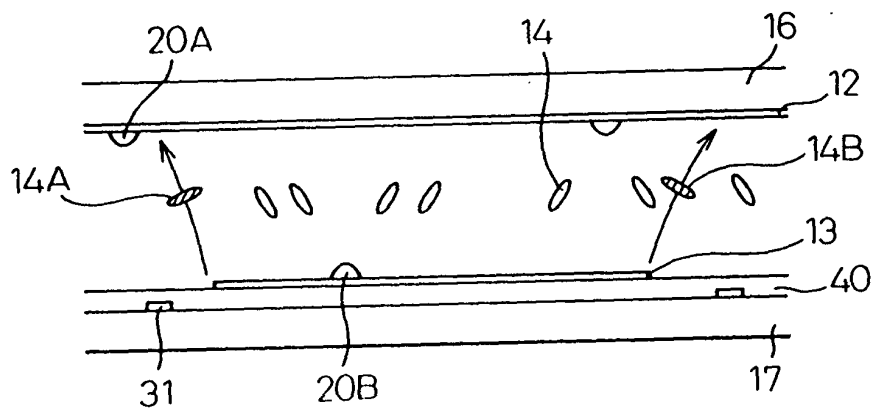


Fig. 61B

B - B'

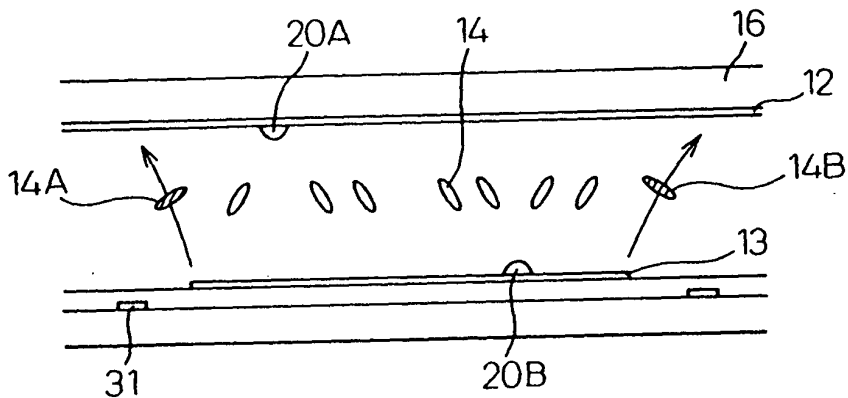


Fig.62A

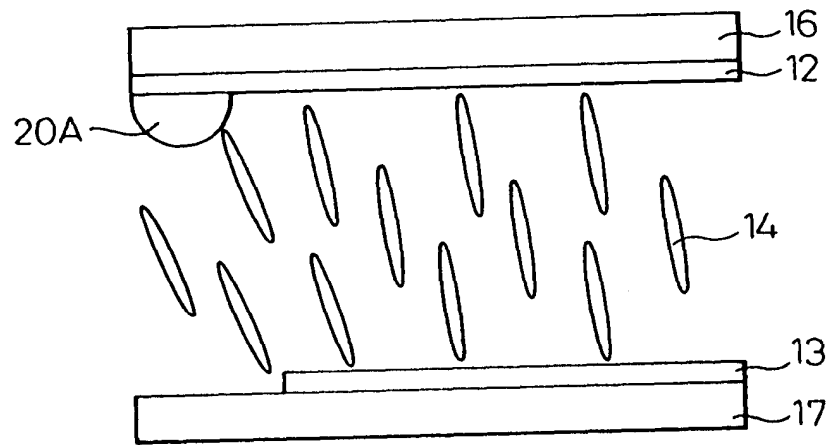


Fig.62B

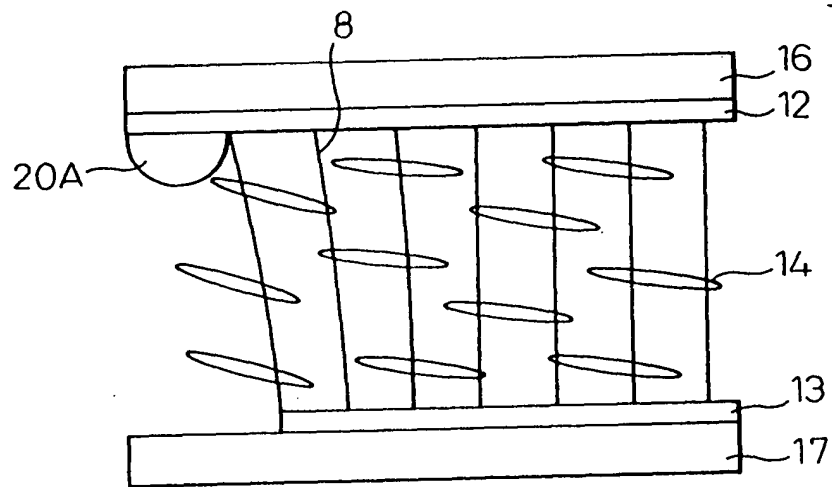


Fig. 63

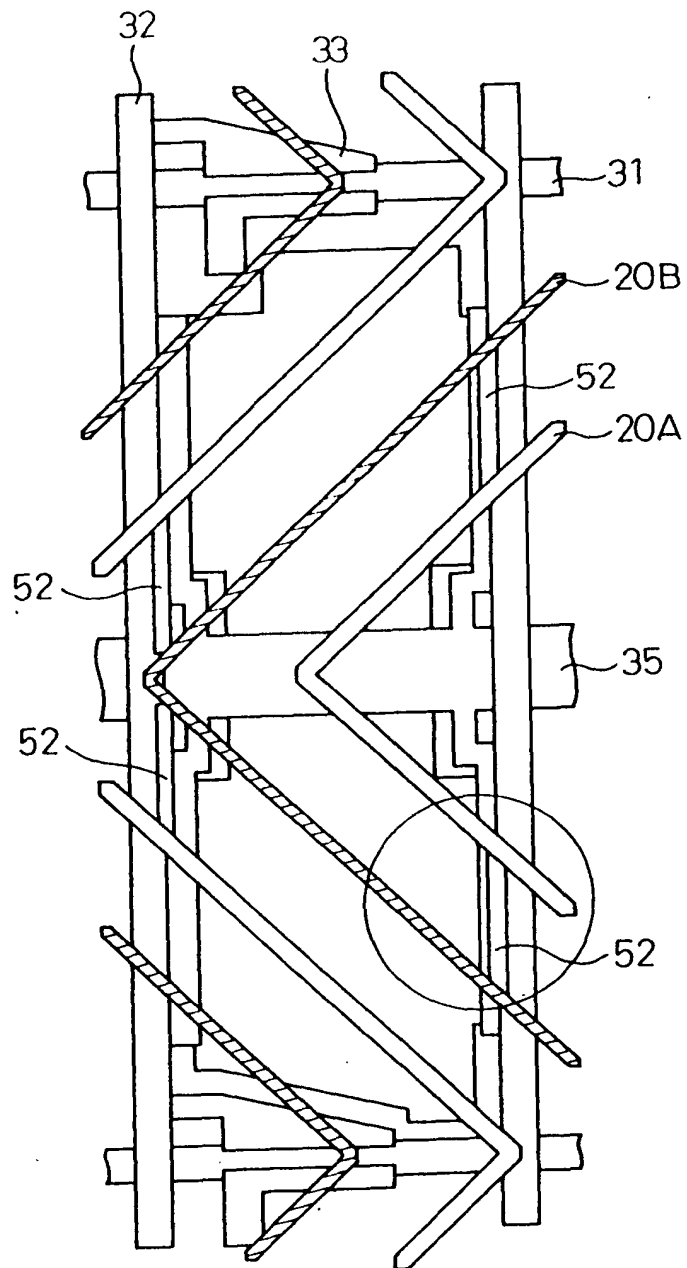


Fig. 64

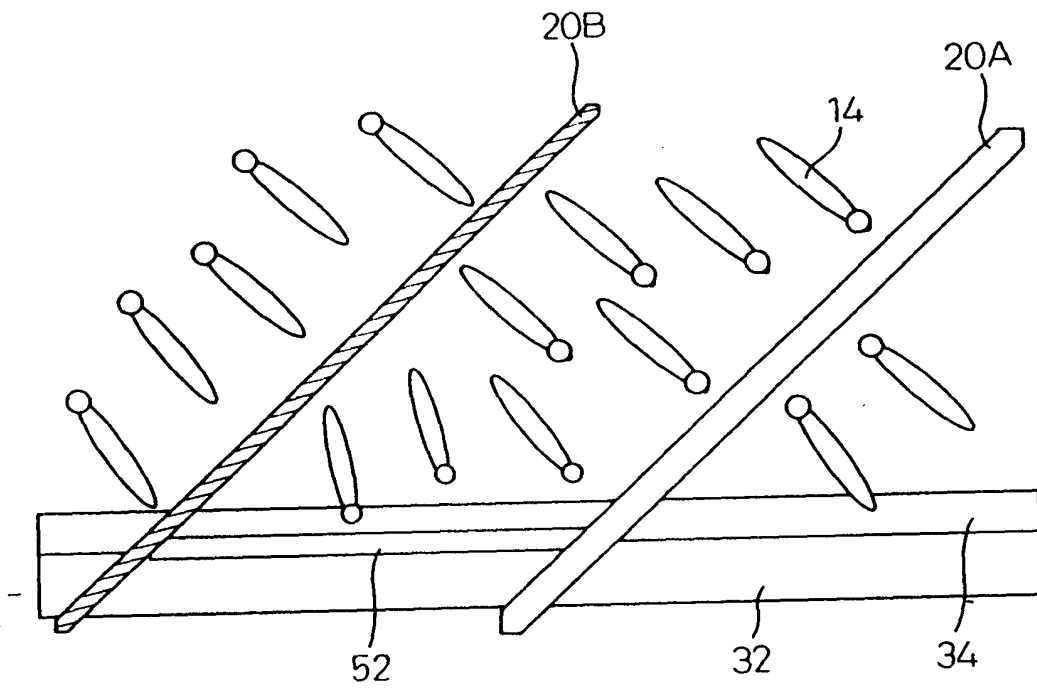


Fig. 65A

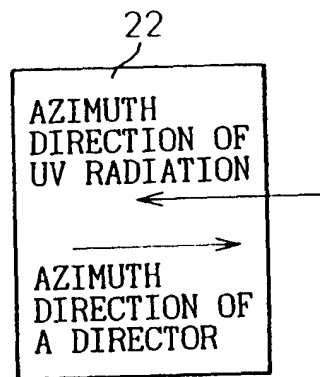
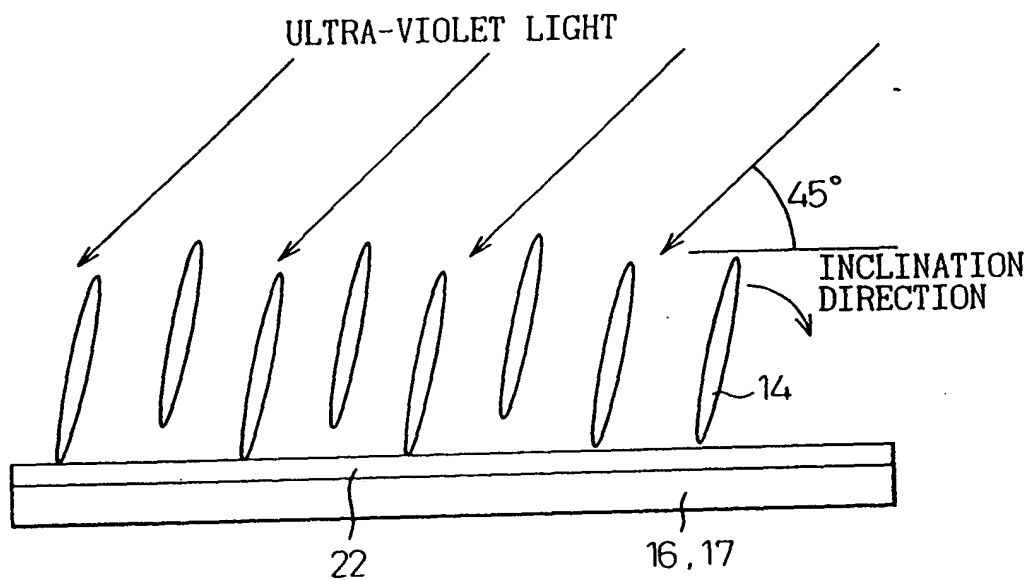


Fig. 65B





65/246

Fig. 66

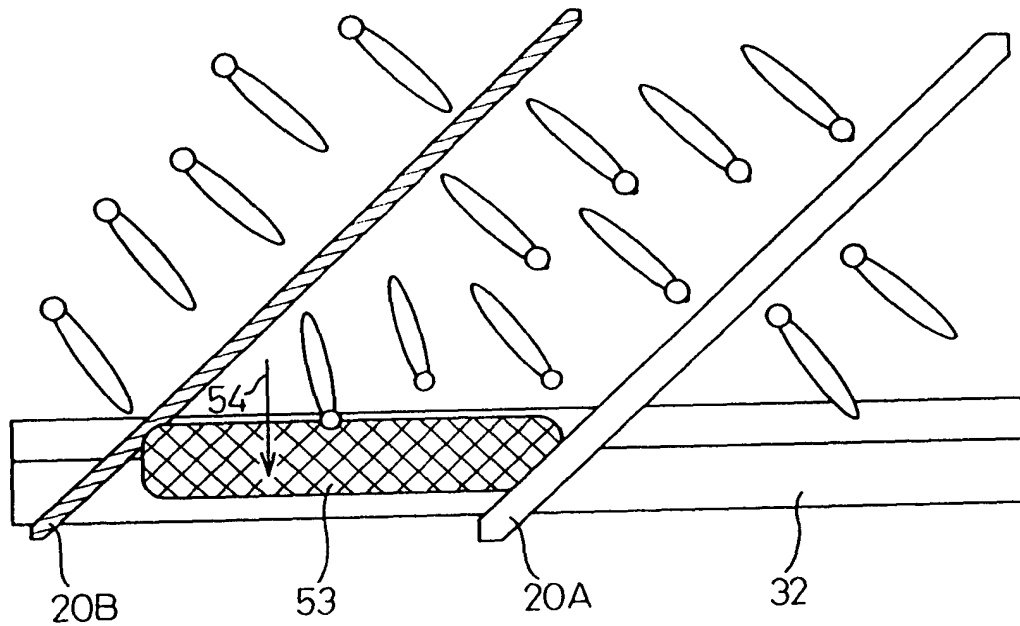


Fig. 67A

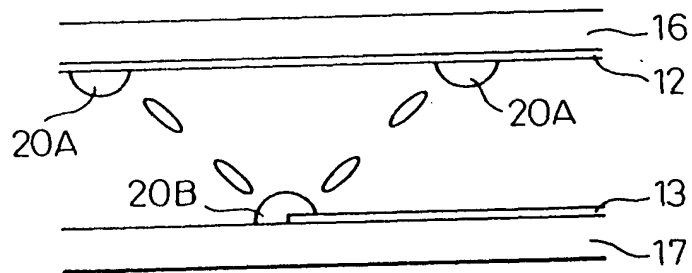


Fig. 67B

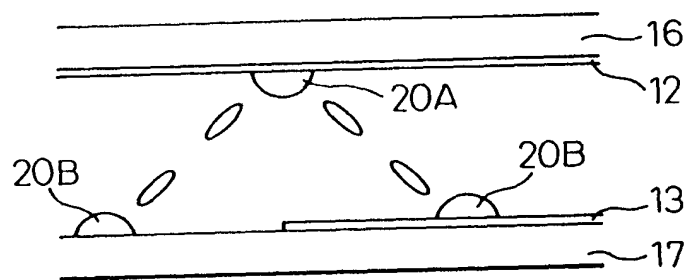


Fig. 67C

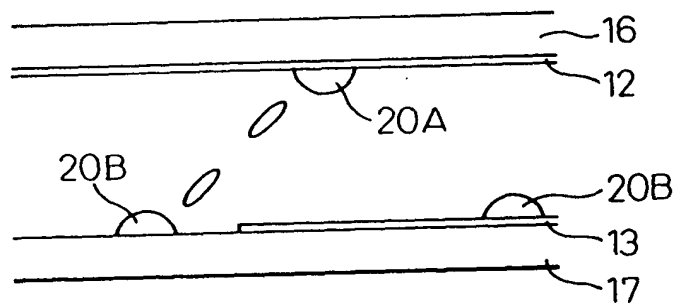
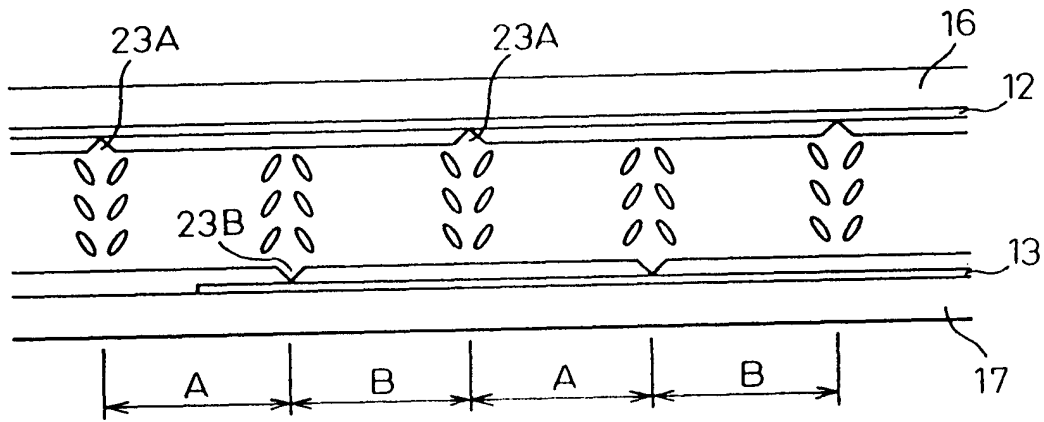


Fig. 68



68/246

Fig. 69A

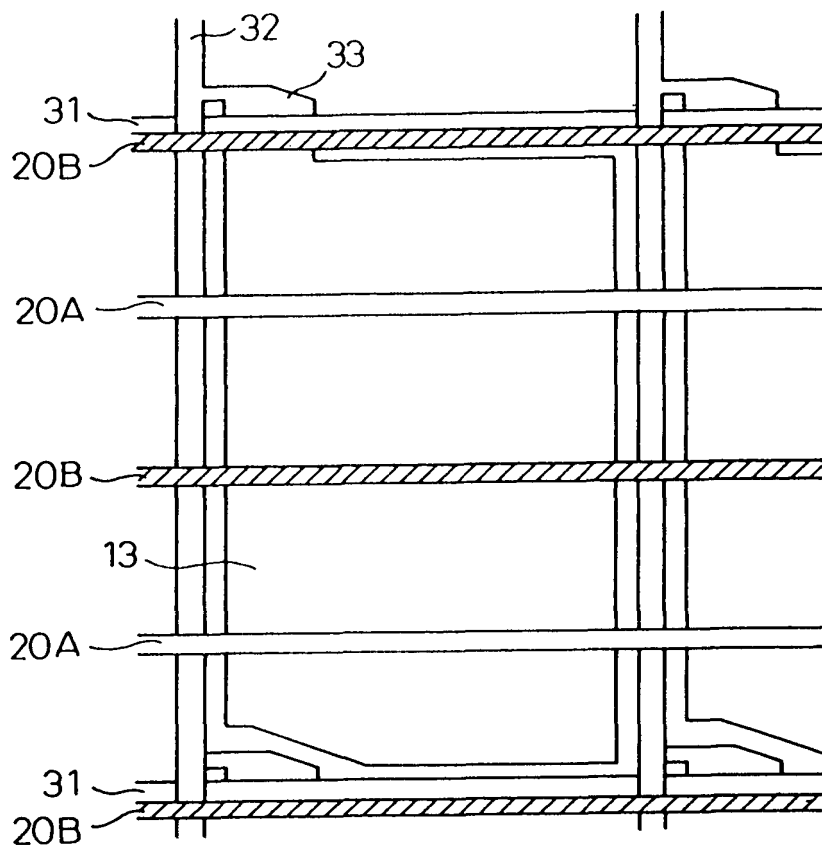


Fig. 69B

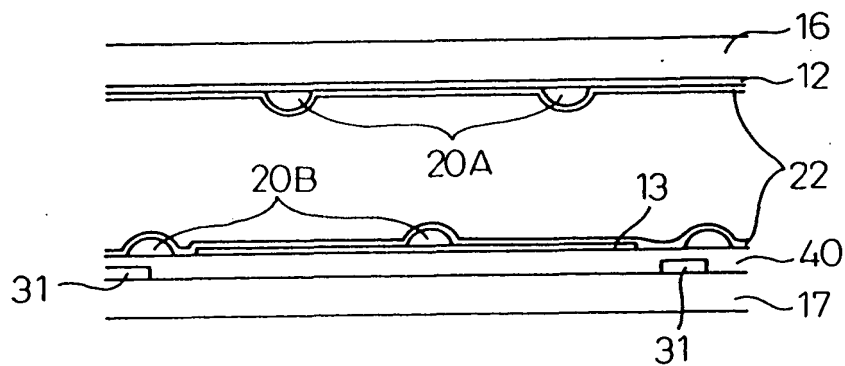


Fig.70A

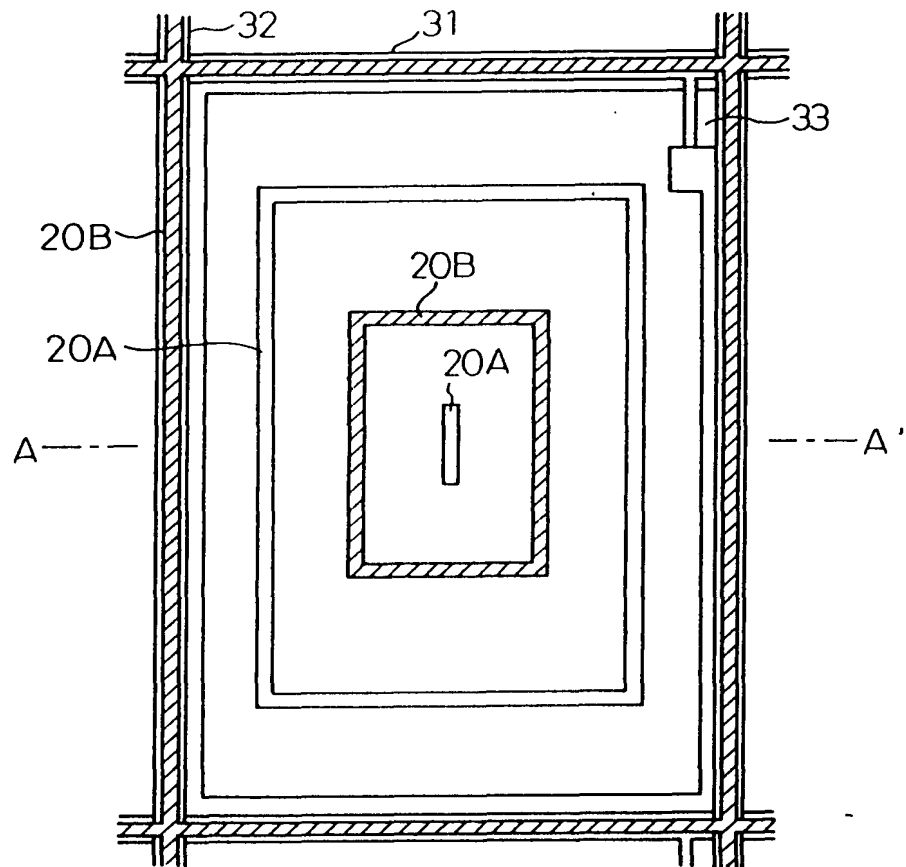
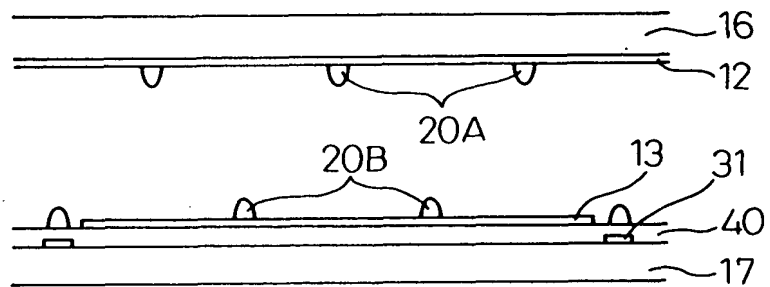
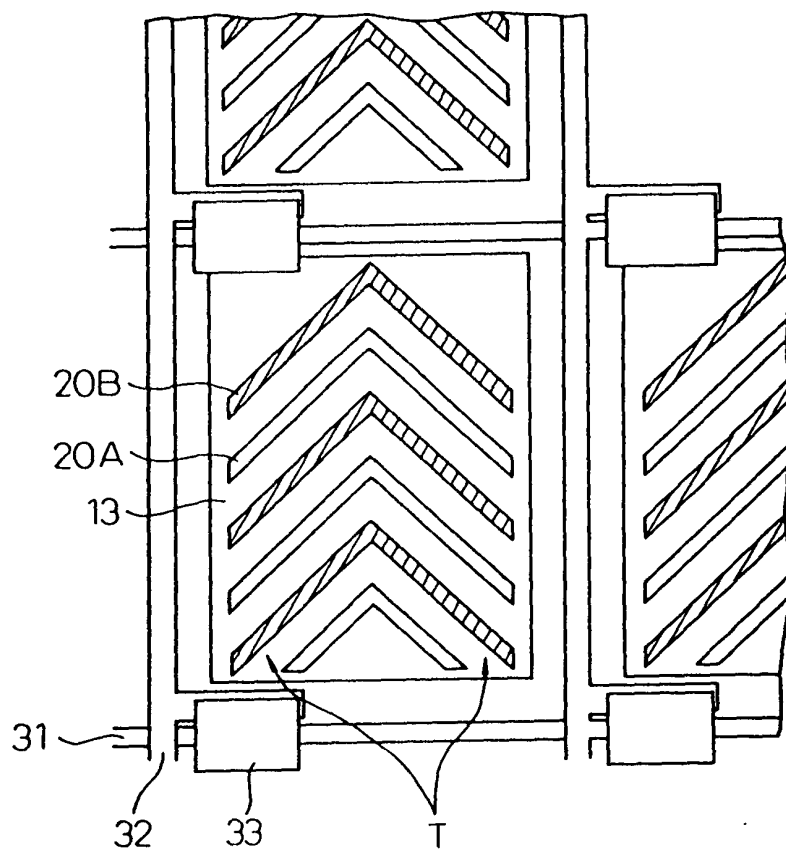


Fig.70B



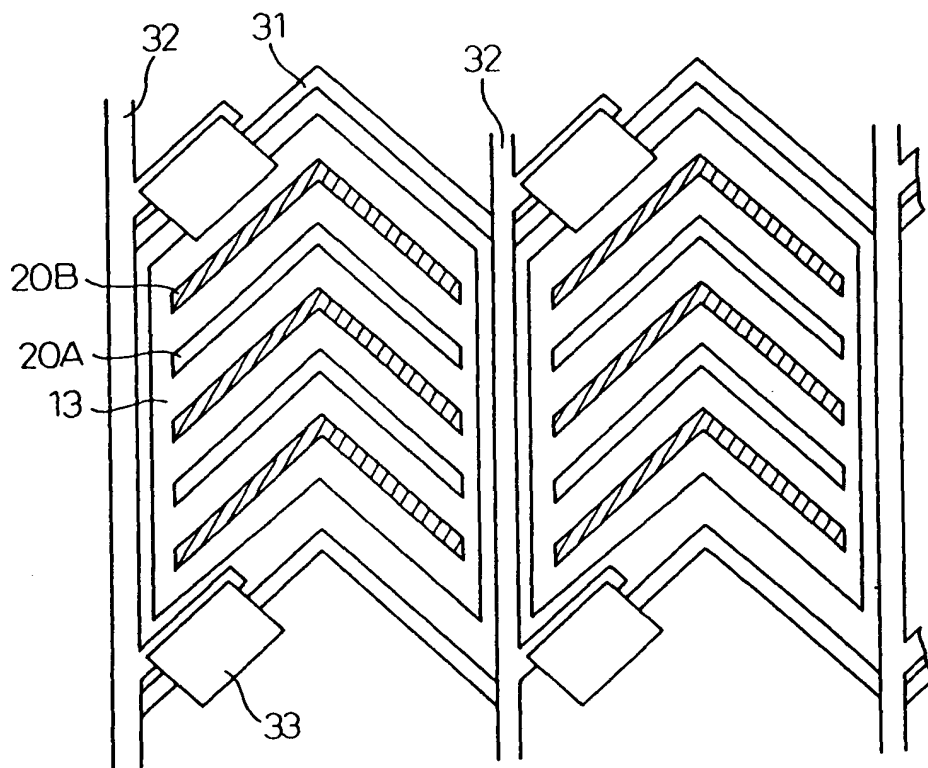
70/246

Fig. 71



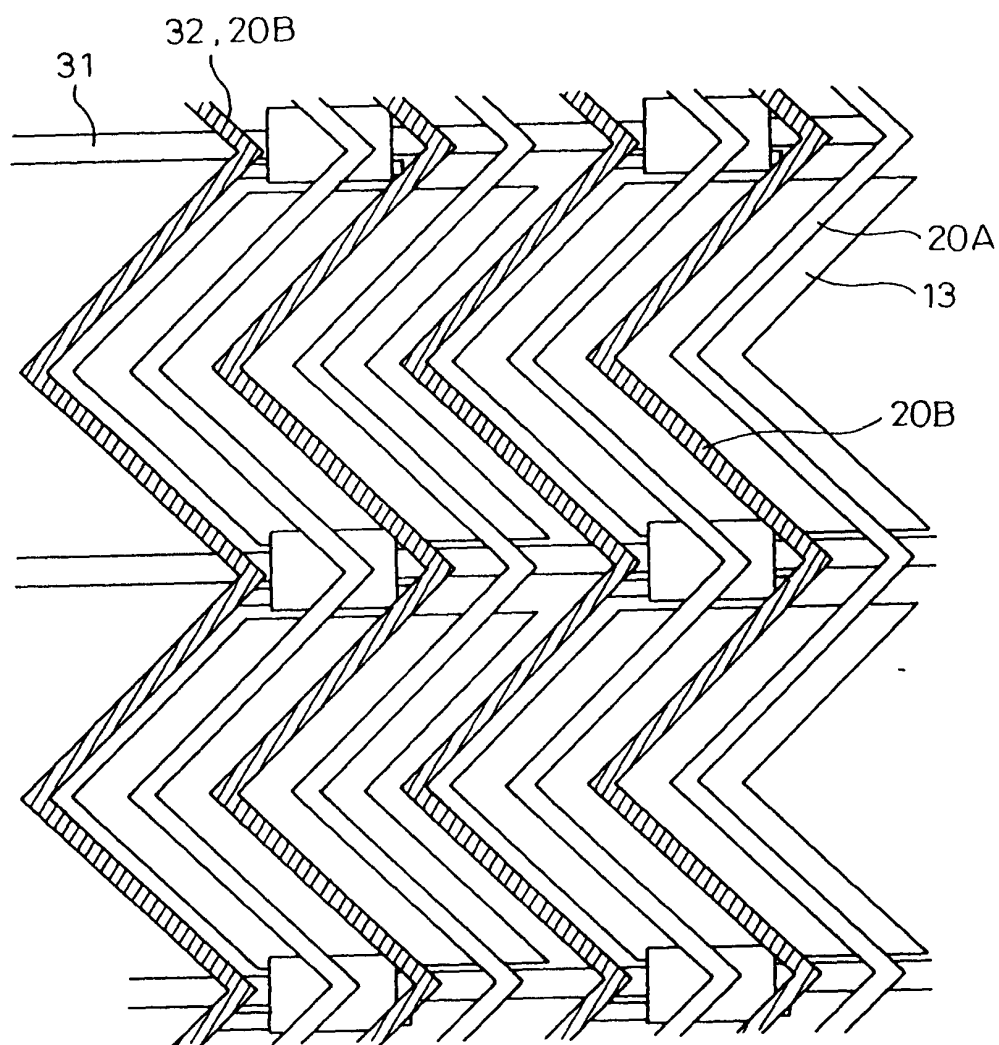
71/246

Fig.72



72/246

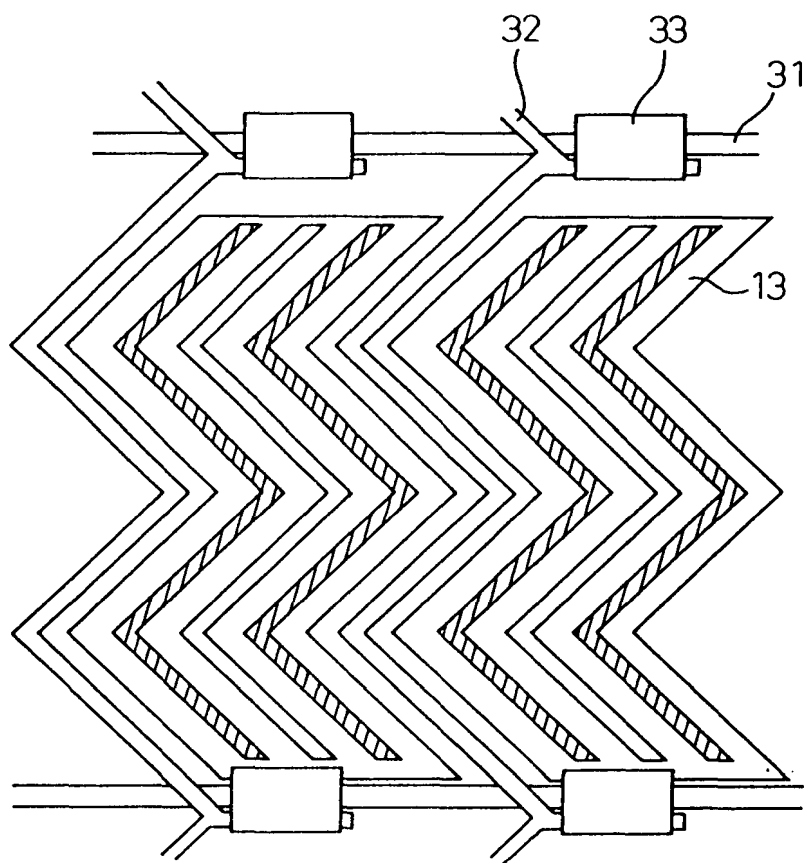
Fig. 73





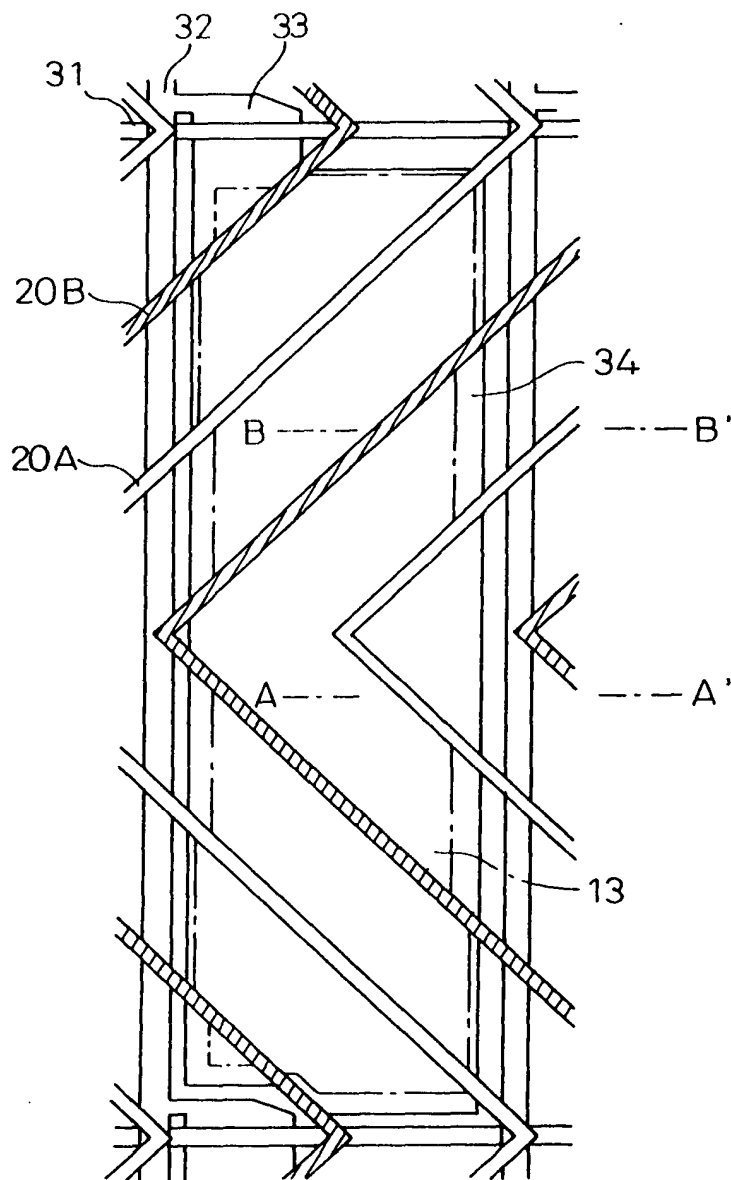
73/246

Fig.74



74/246

Fig. 75



75/  
246

Fig.76A

A-A'

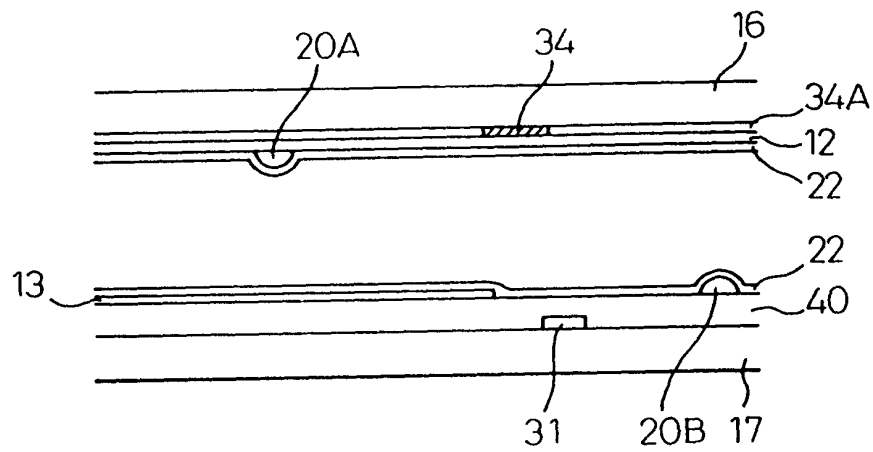


Fig.76B

B-B'

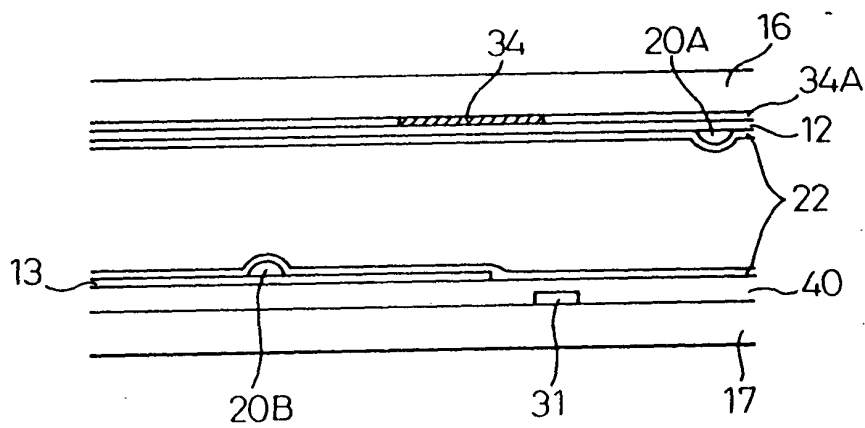


Fig.77A

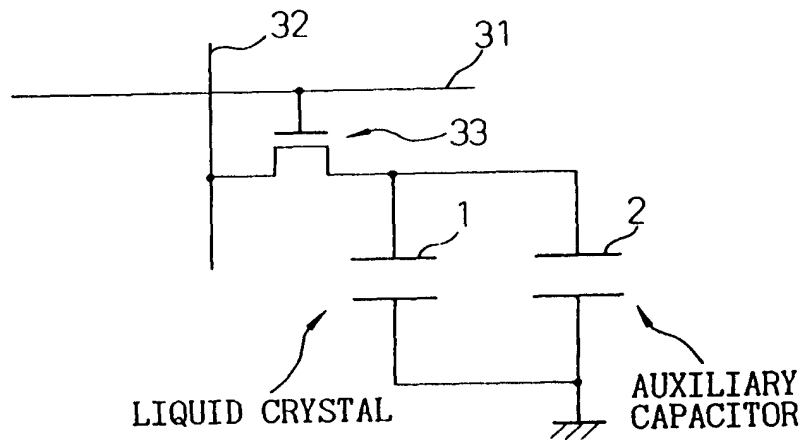


Fig.77B

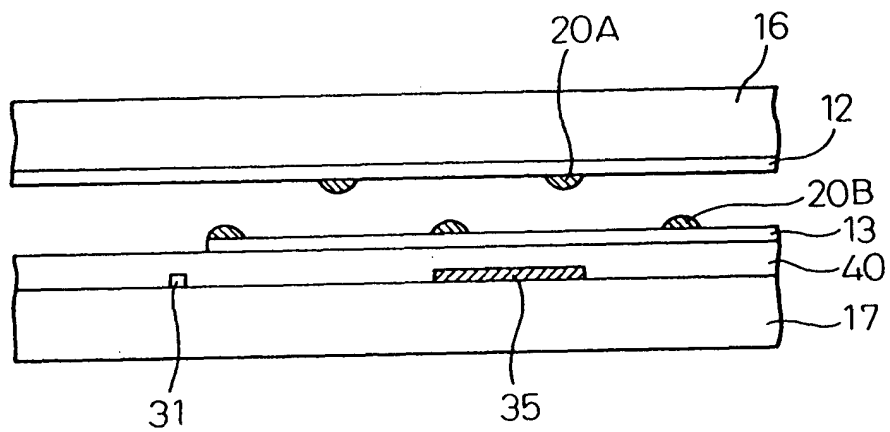


Fig.78A

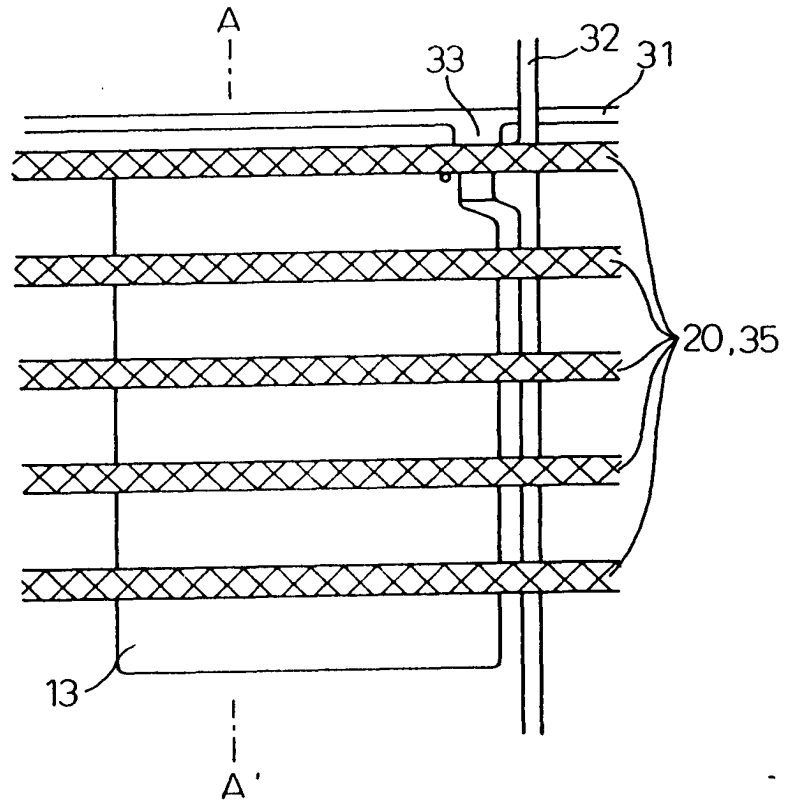
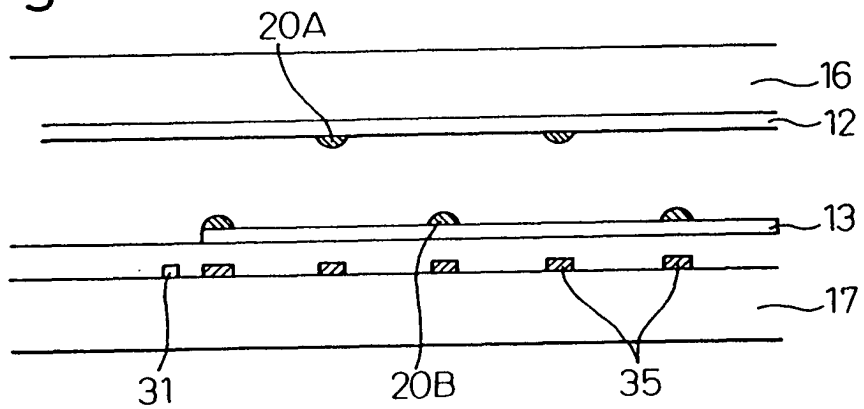


Fig.78B



78/246

Fig.79A

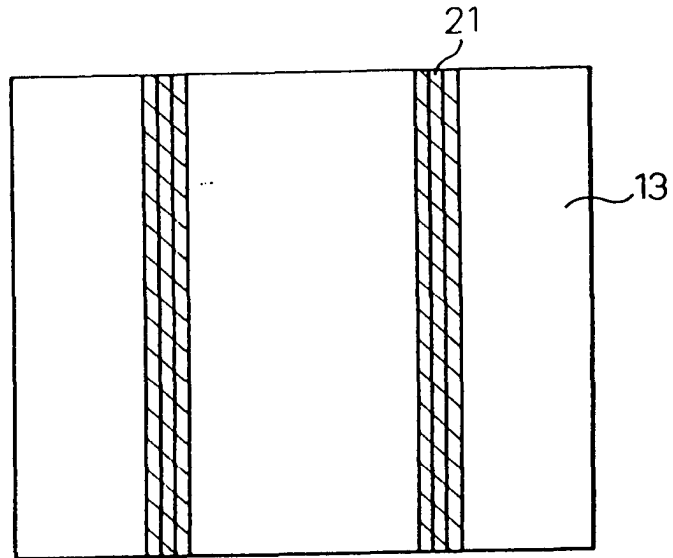
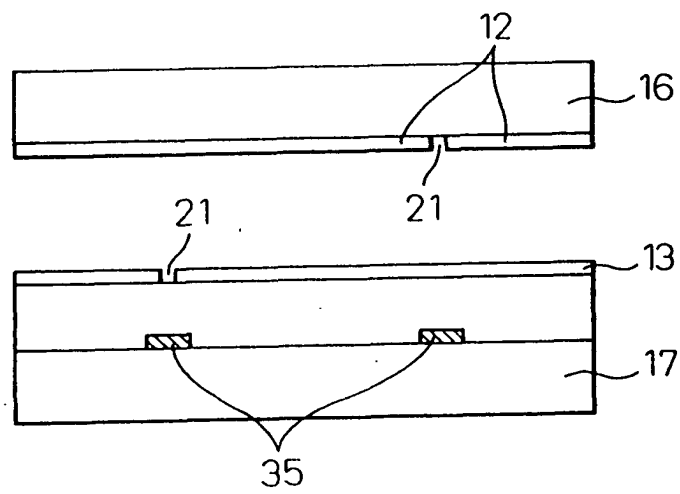


Fig.79B



79/246

Fig.80A

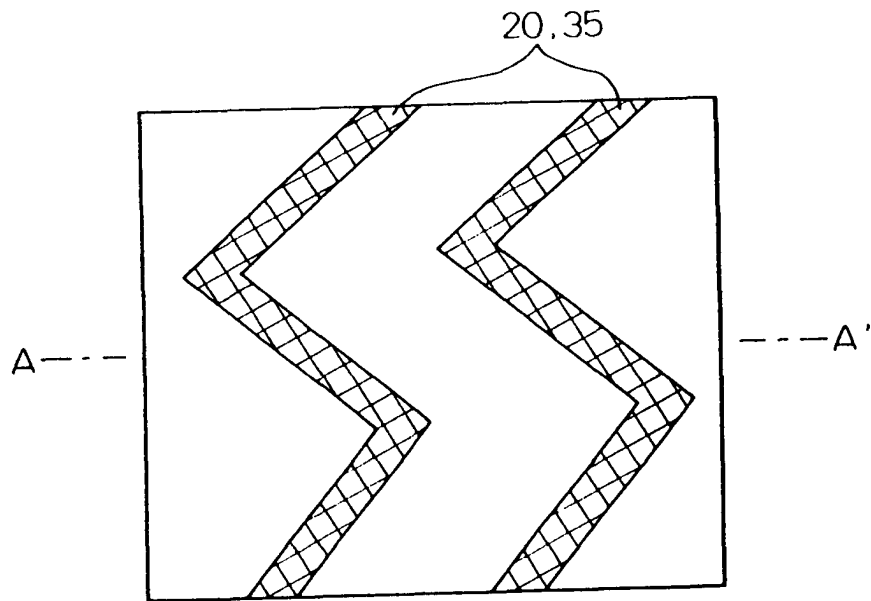
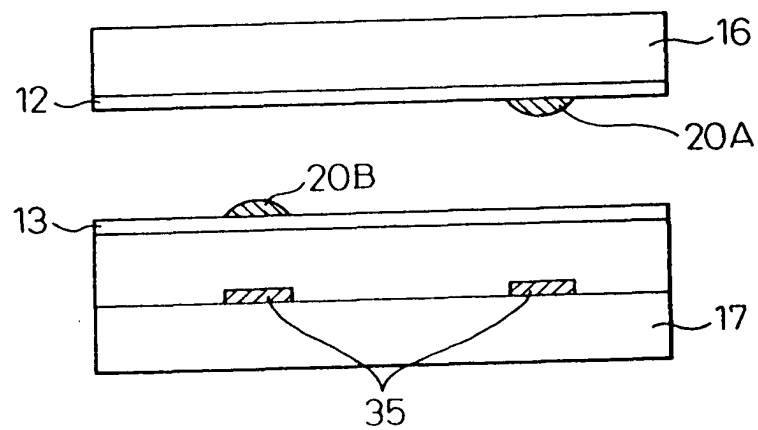


Fig.80B



80/246

Fig.81A

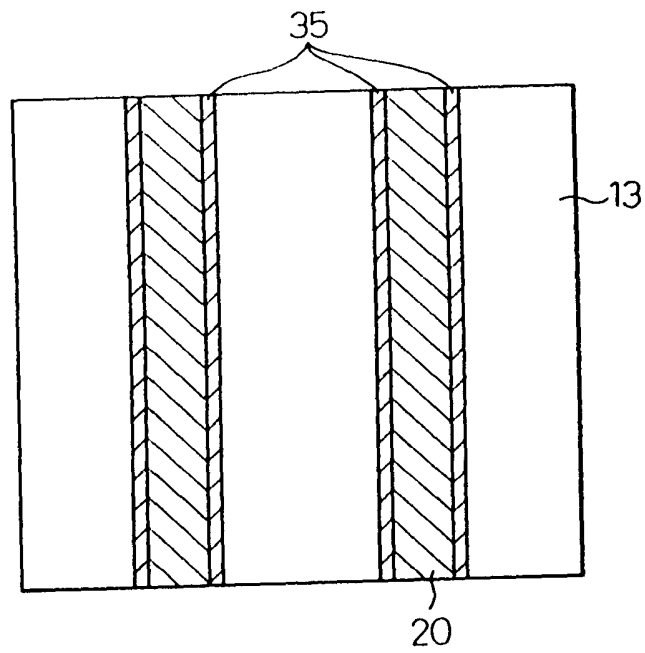


Fig.81B

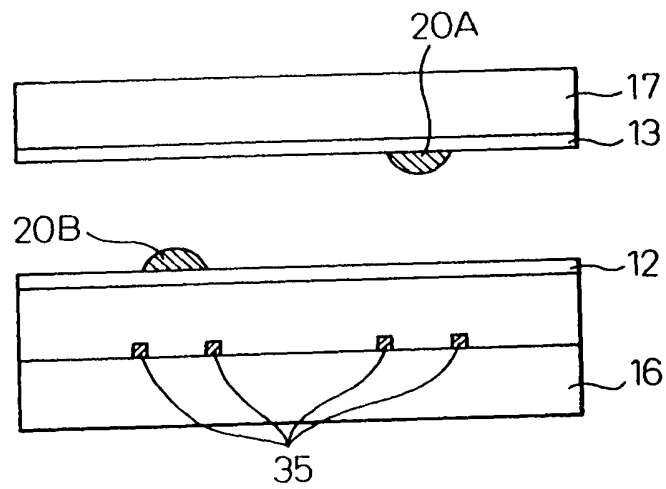
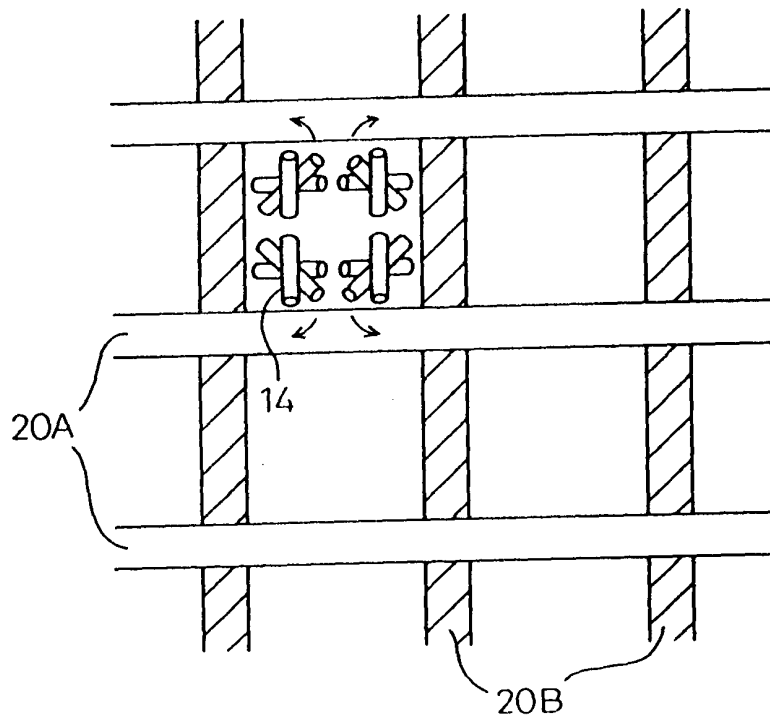




Fig. 82



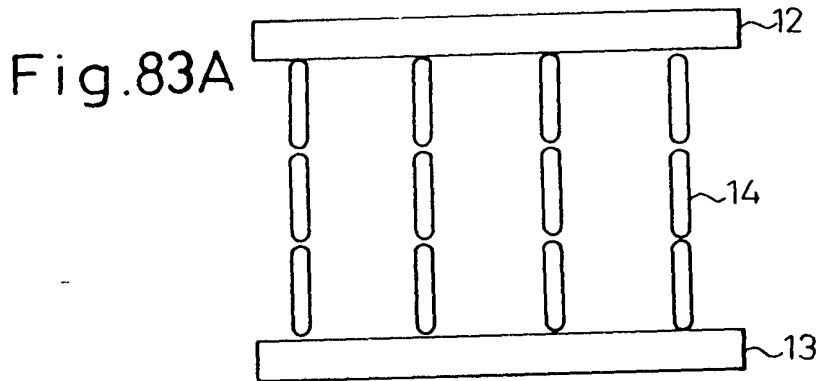


Fig.83B

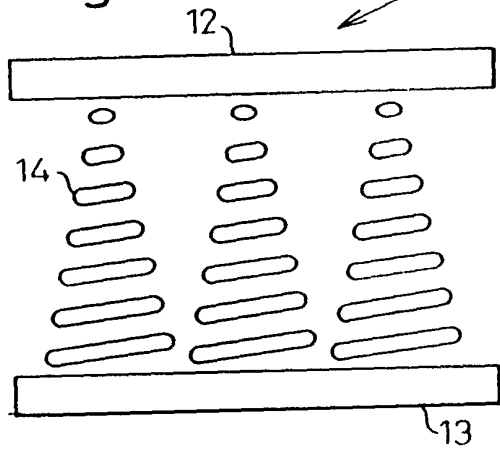


Fig.83C

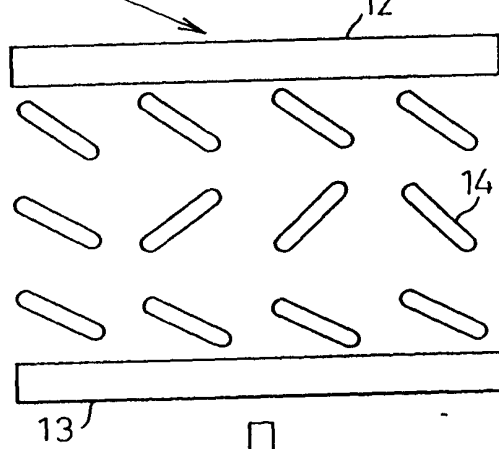
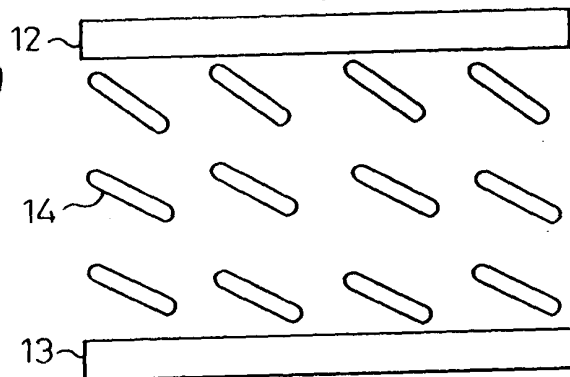
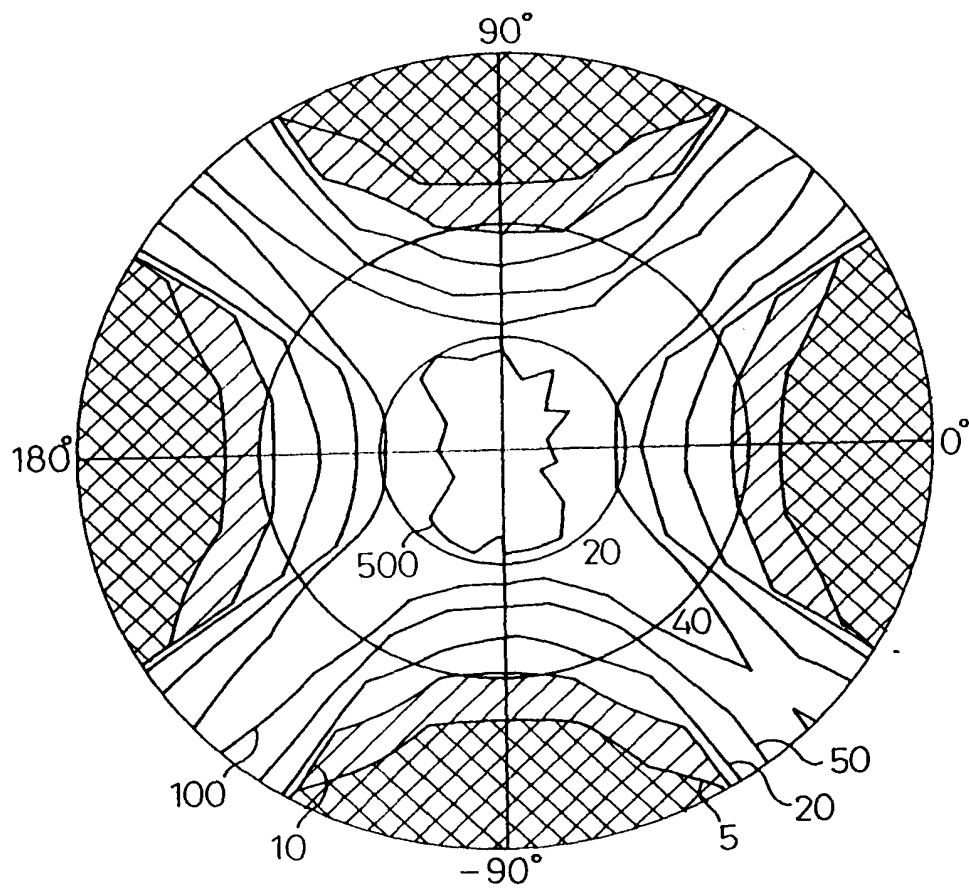


Fig.83D



83/246

Fig. 84



84/246

Fig.85A

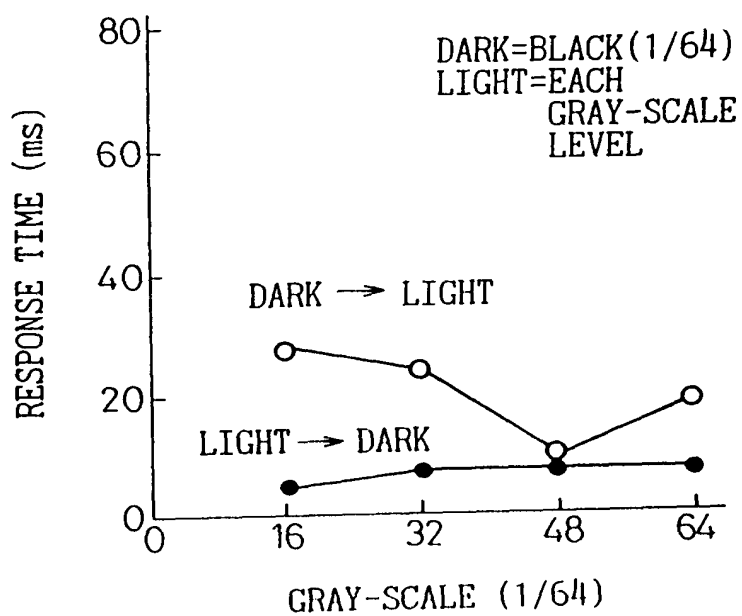
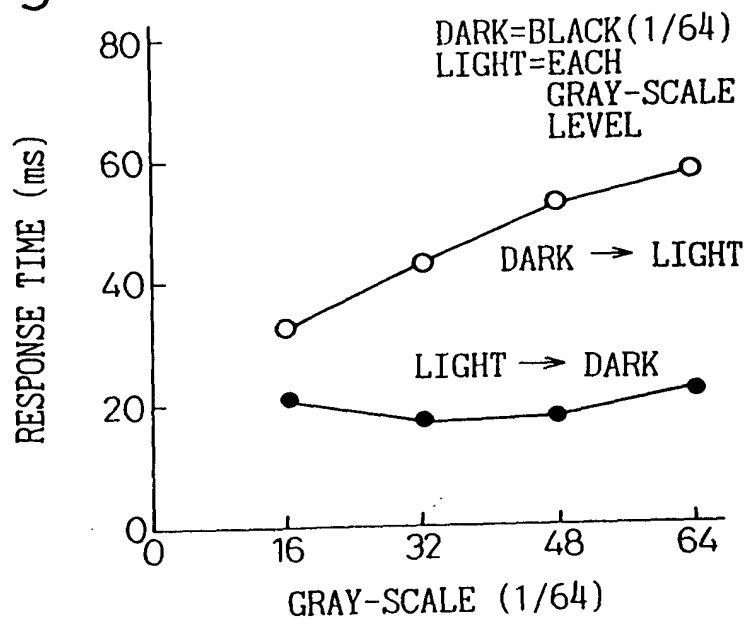


Fig.85B



85/246

Fig. 85C

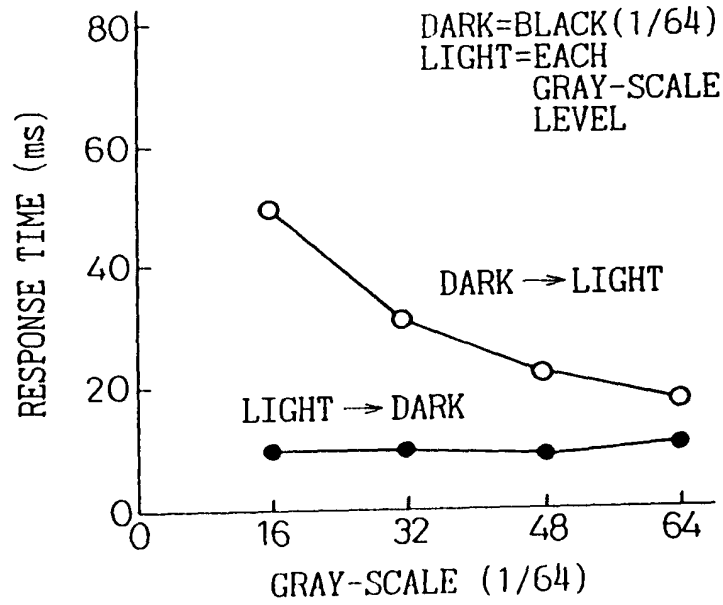
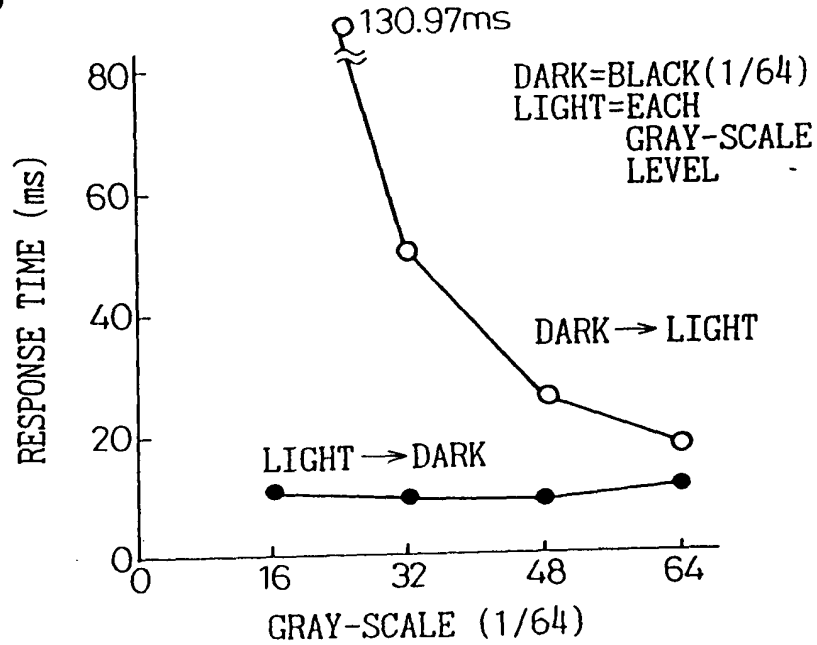


Fig. 85D



86/  
246

Fig.86A

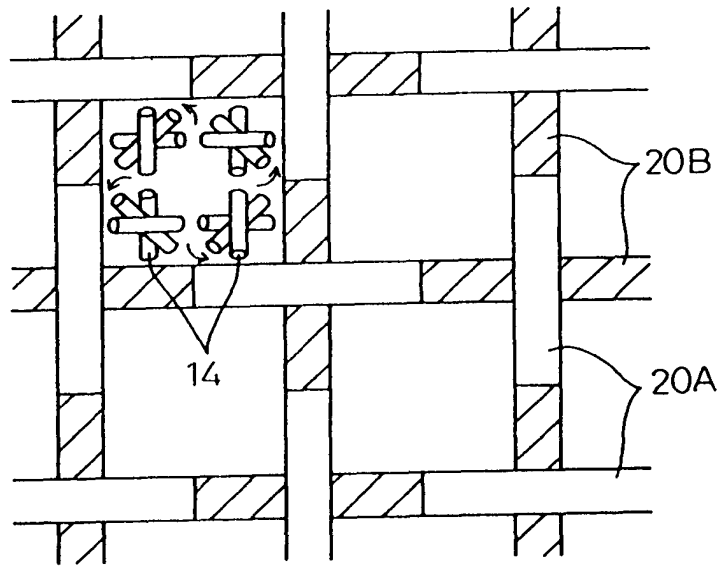
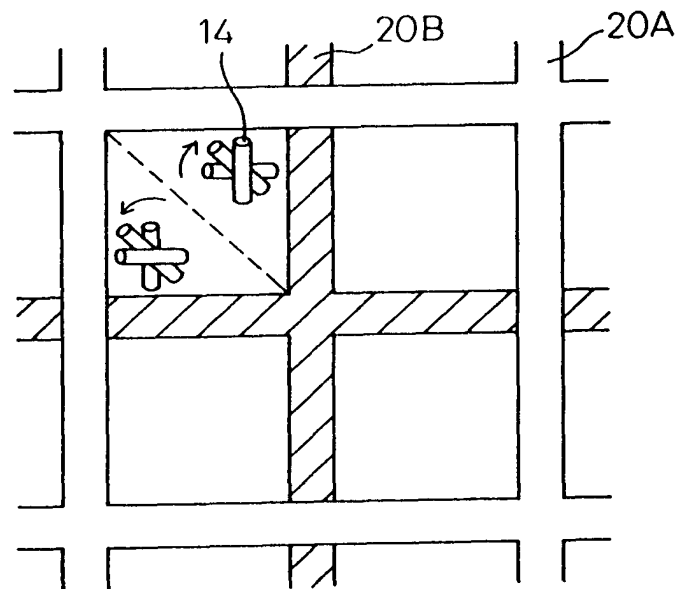


Fig.86B



87/246

Fig. 87

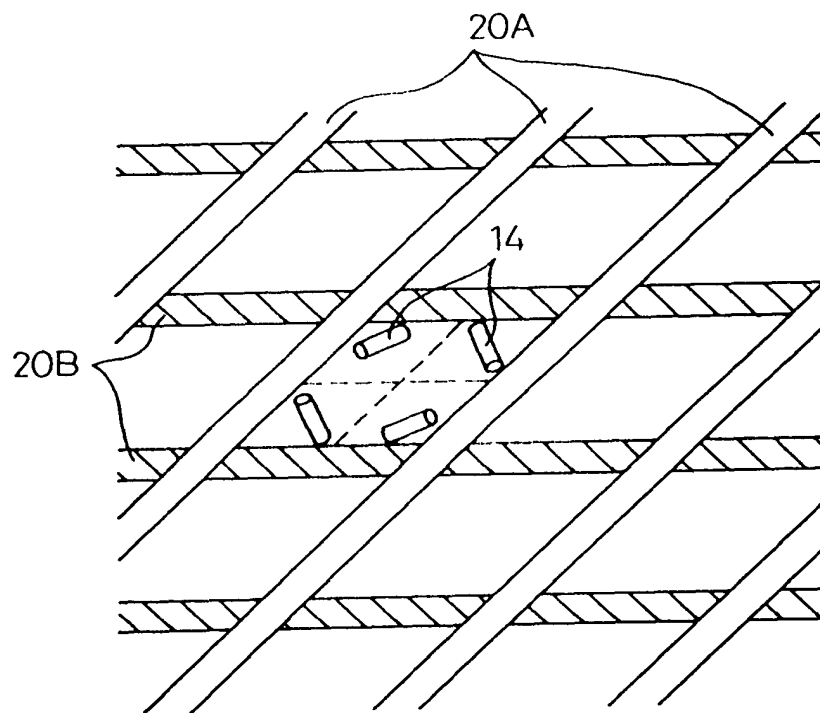


Fig. 88

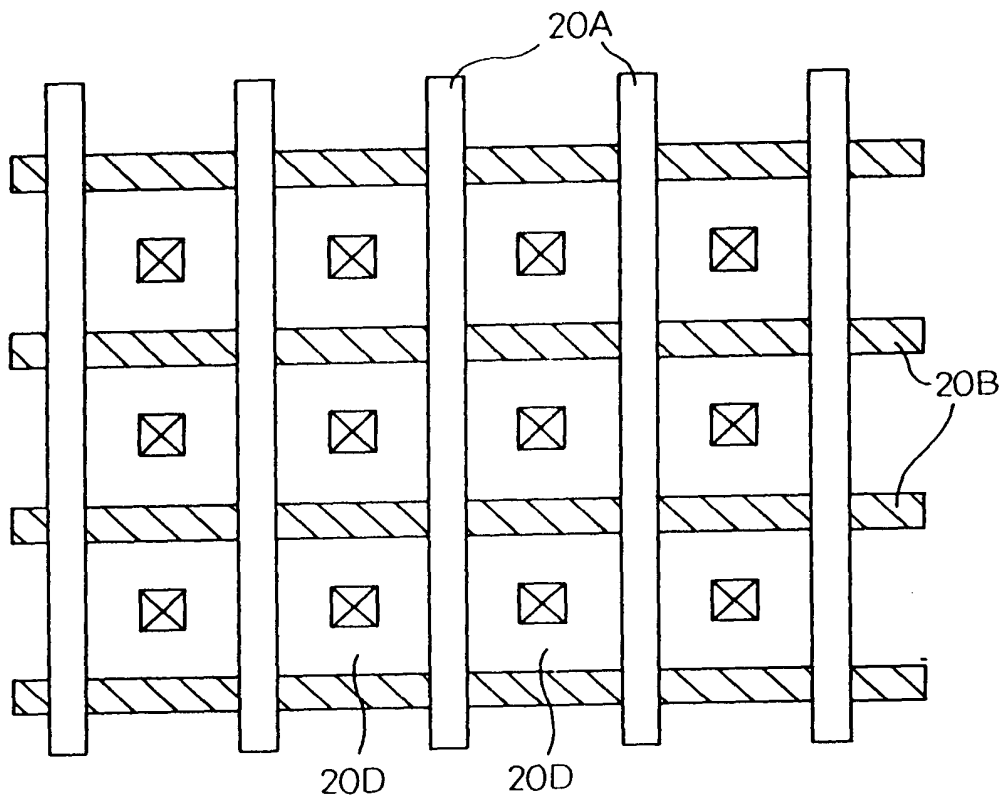
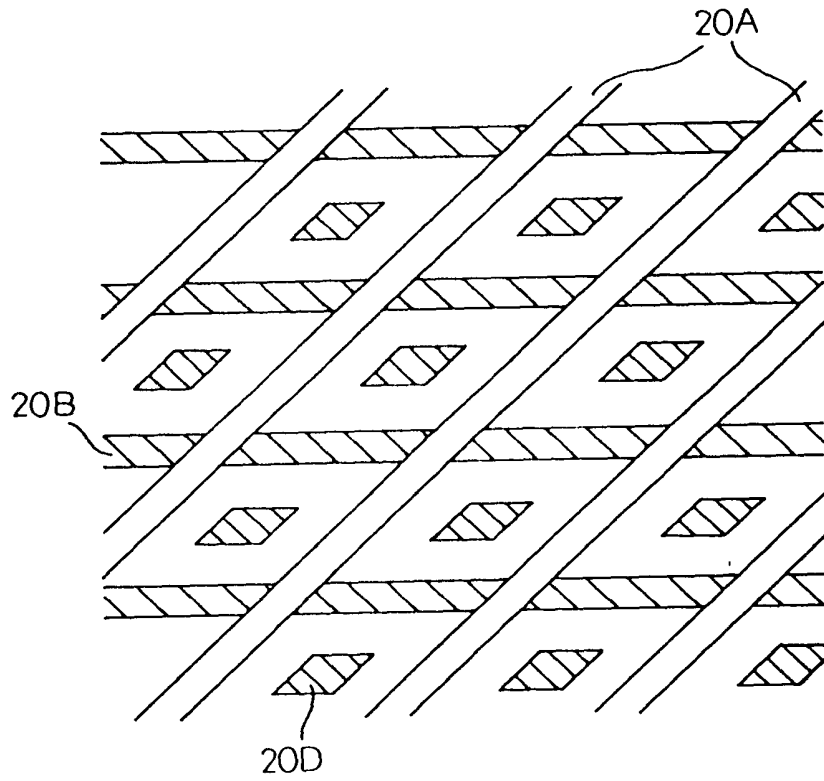




Fig. 89



90/  
246

Fig.90A

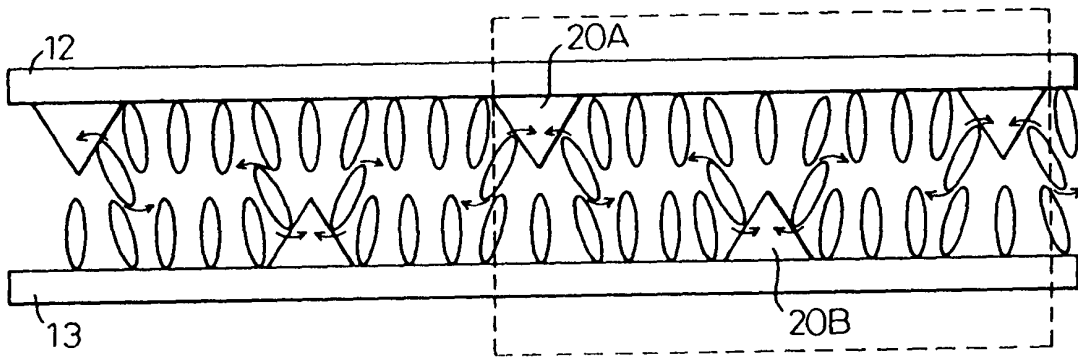
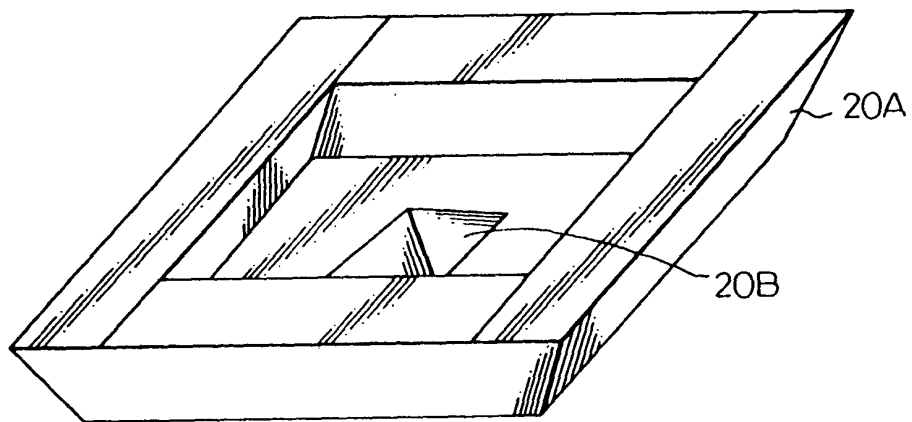
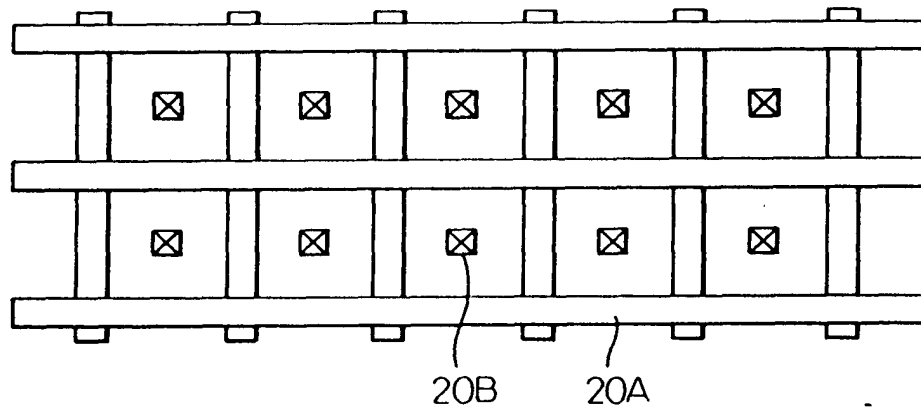


Fig.90B



91/246

Fig.91



92/246

Fig.92A

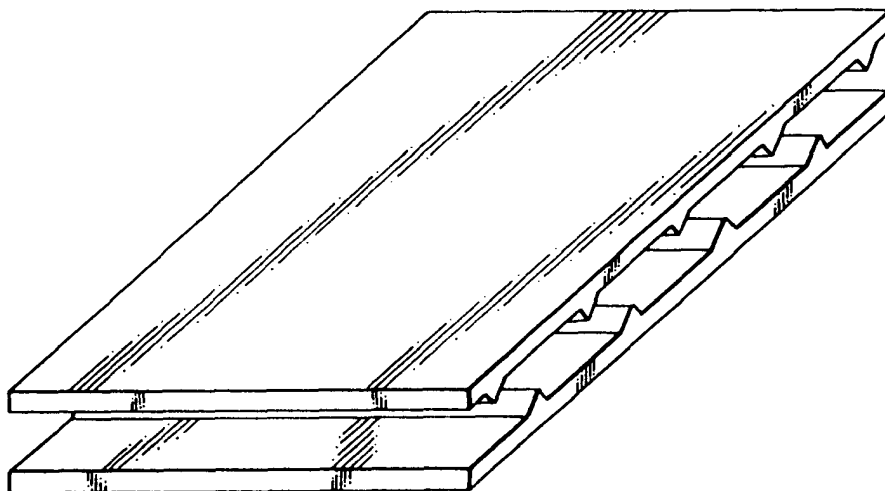


Fig.92B

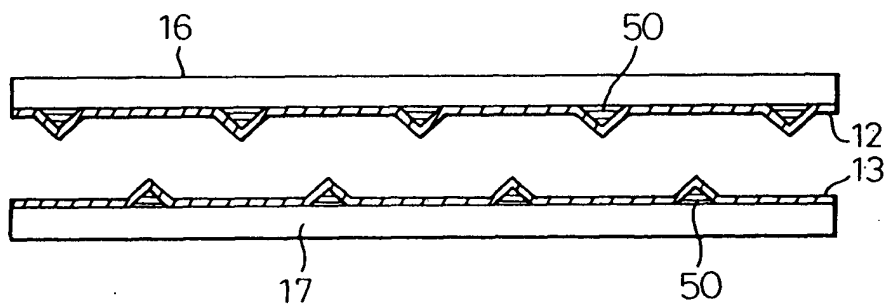
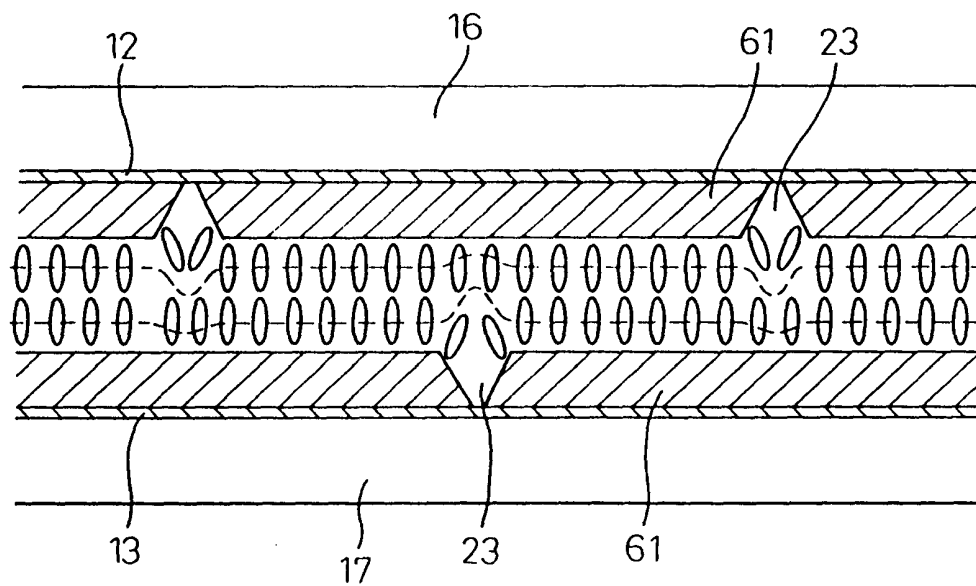


Fig. 93



94/246

Fig.94

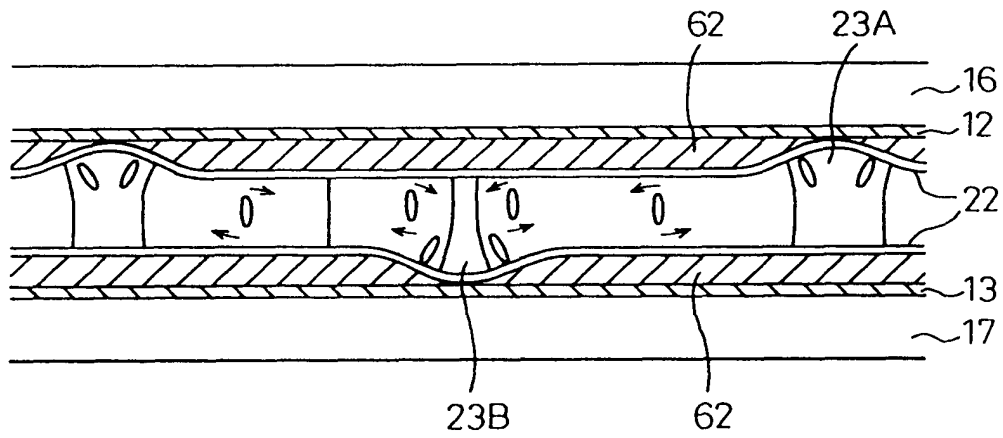


Fig.95

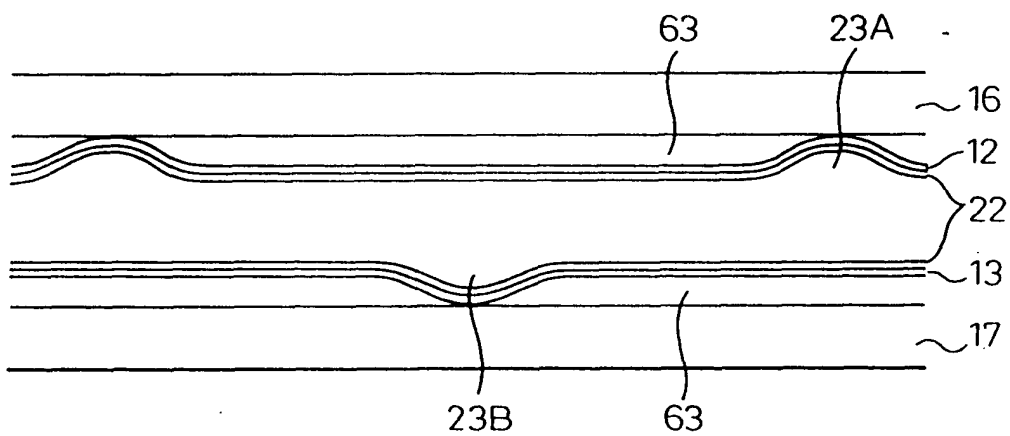


Fig.96

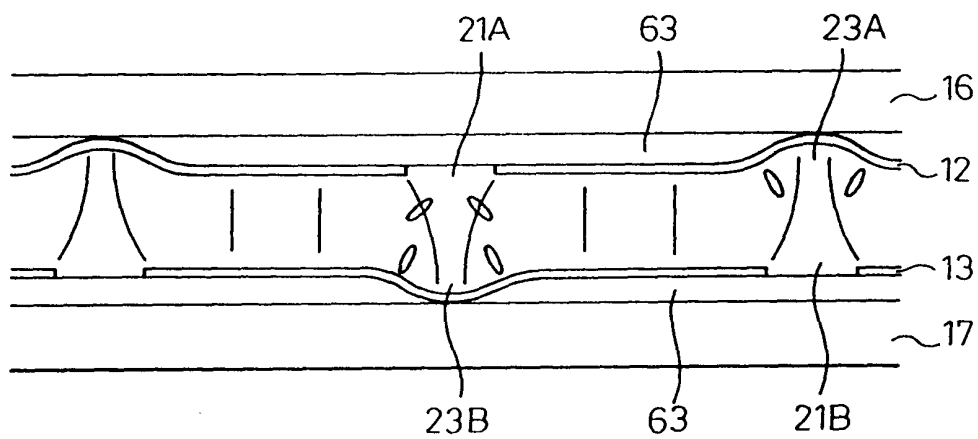


Fig.97

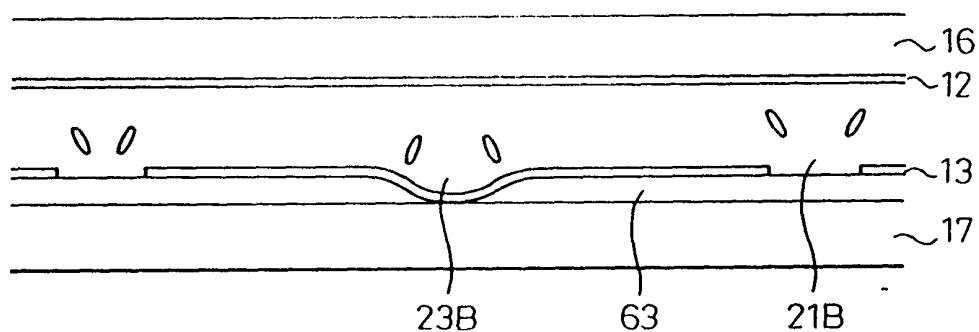
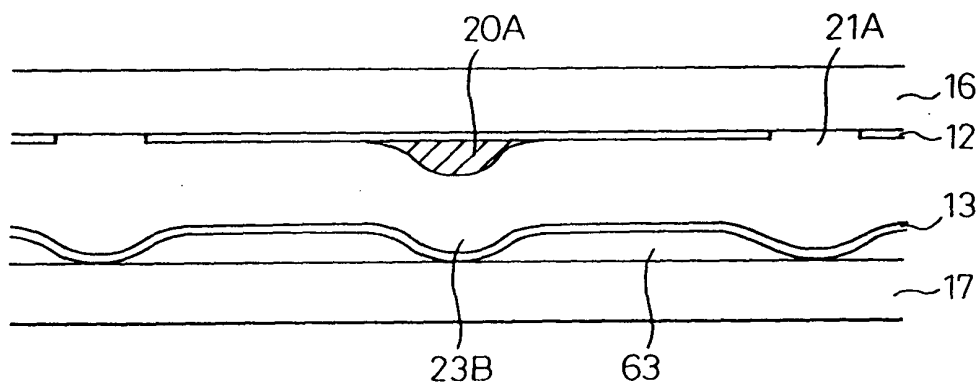


Fig.98



96/246

Fig.99A

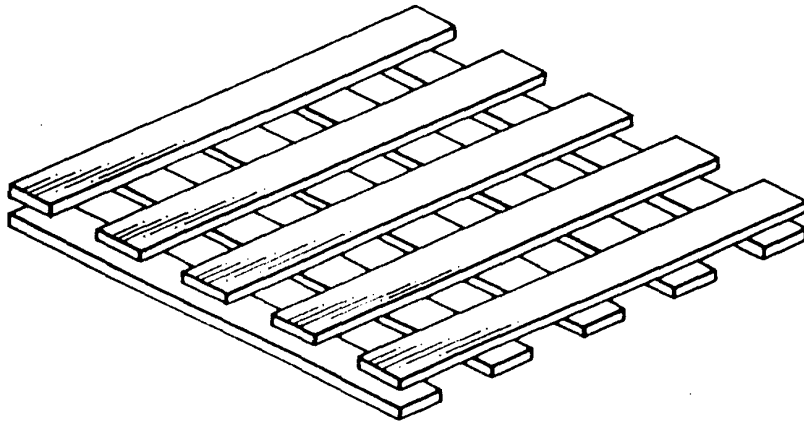


Fig.99B

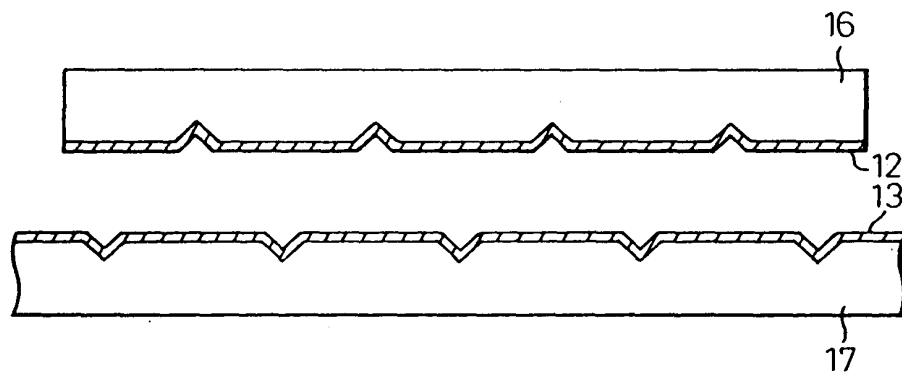




Fig.100A

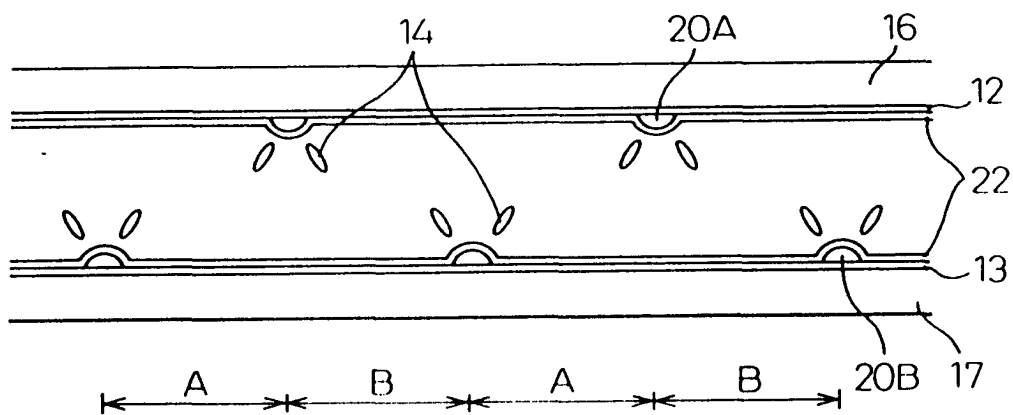


Fig.100B

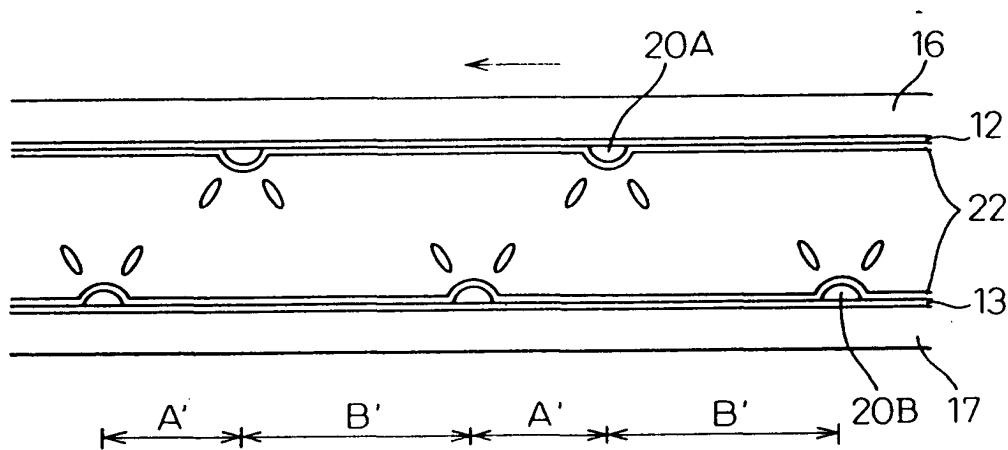


Fig. 101A

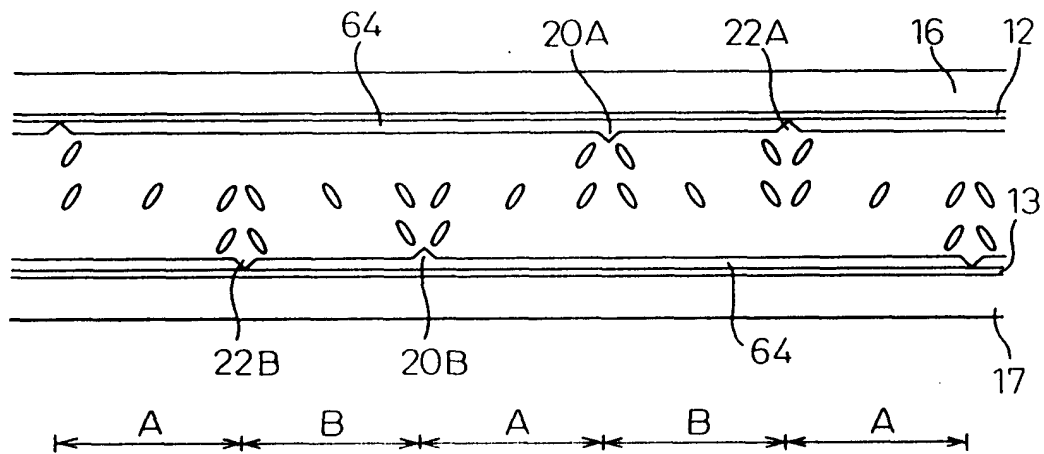
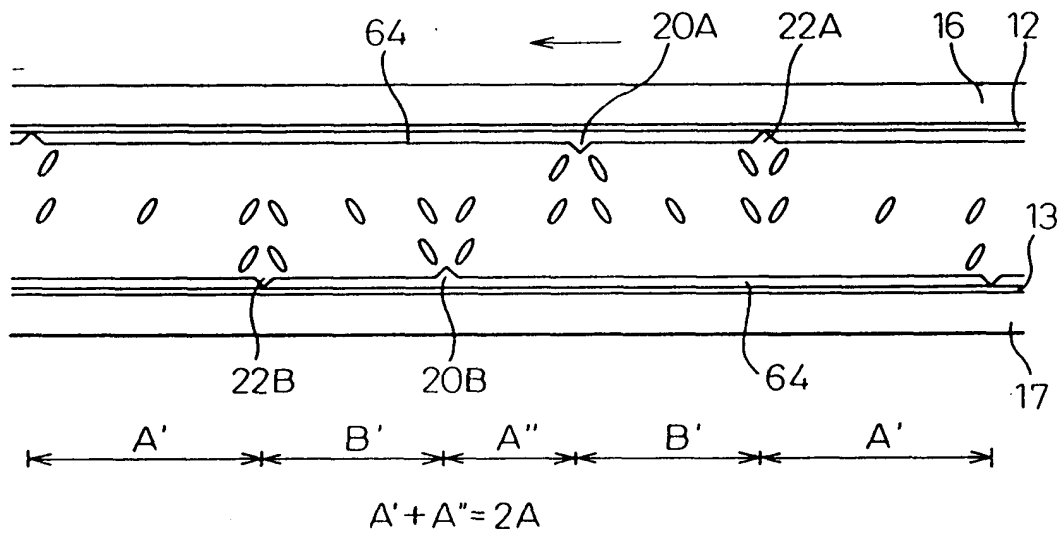
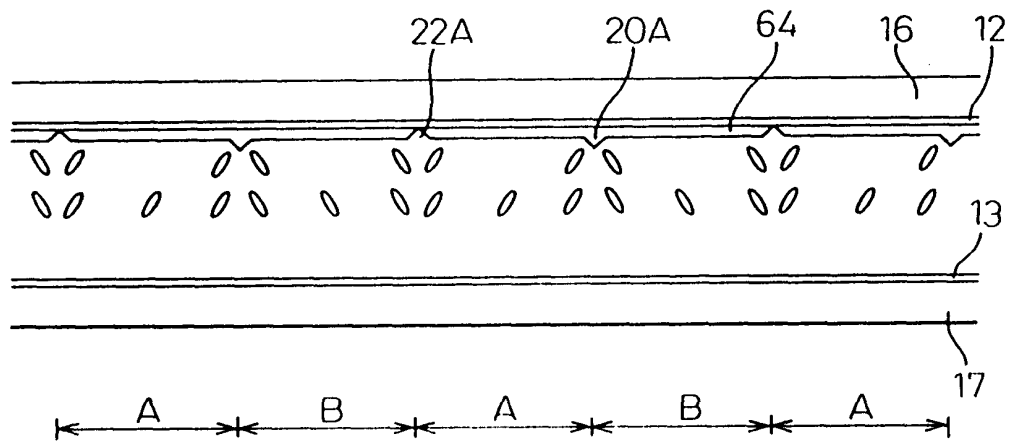


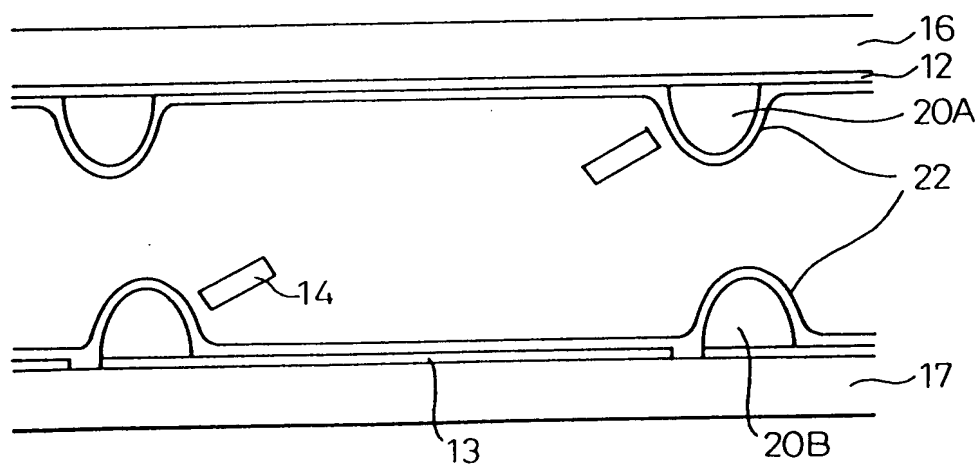
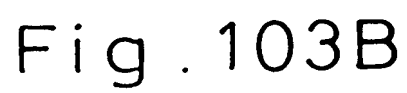
Fig. 101B



99/246

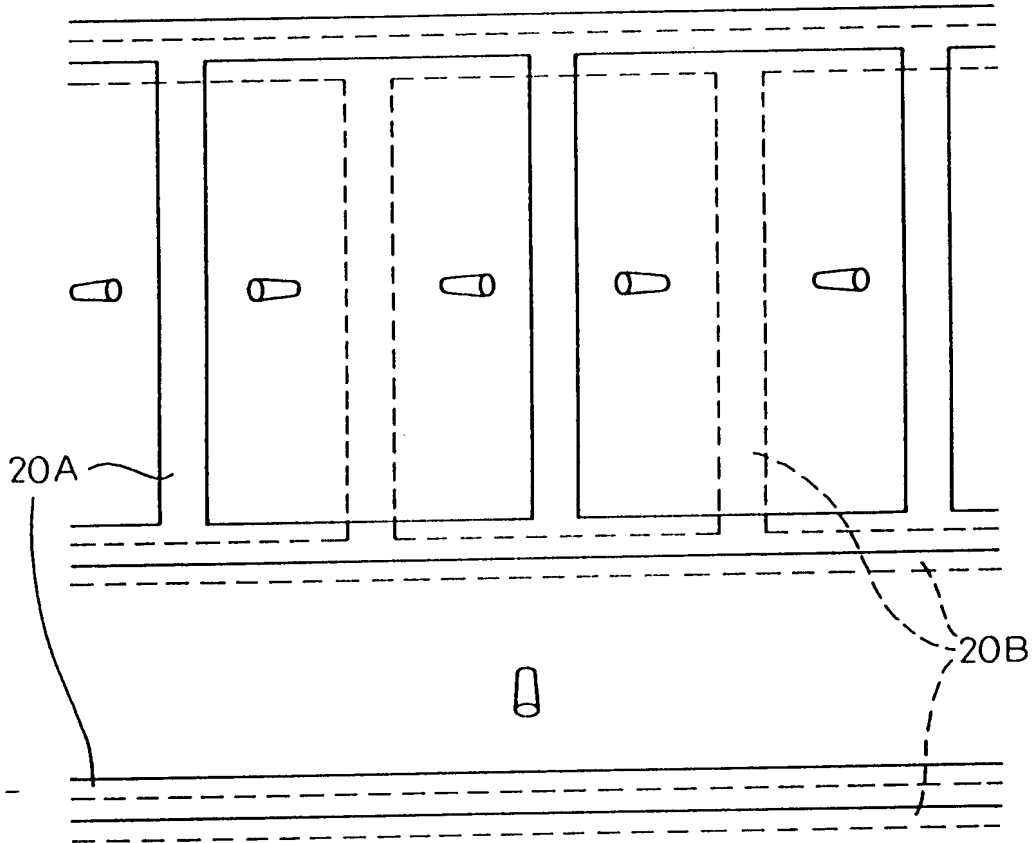
Fig.102





101/246

Fig.104



14

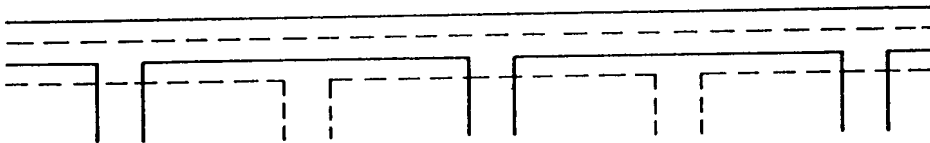


Fig.105A

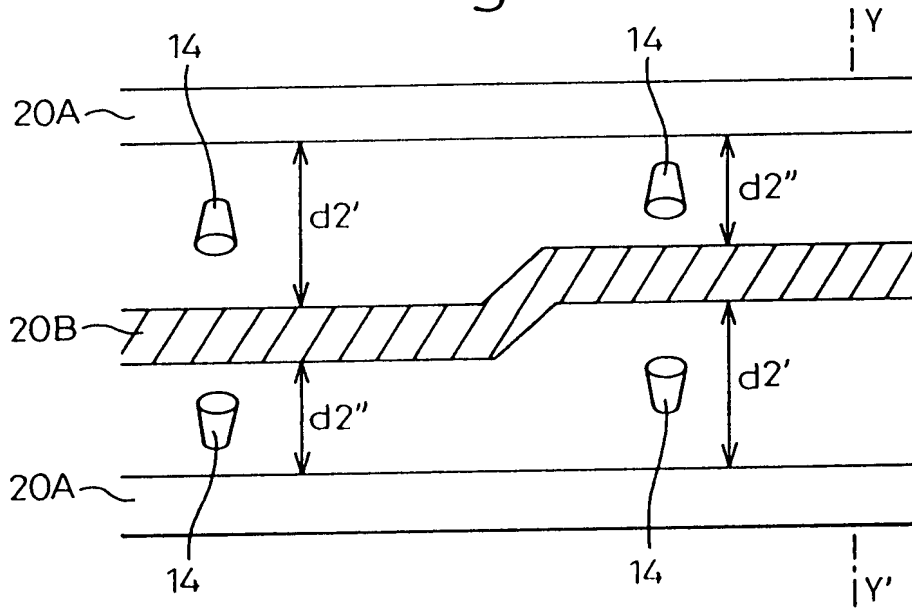
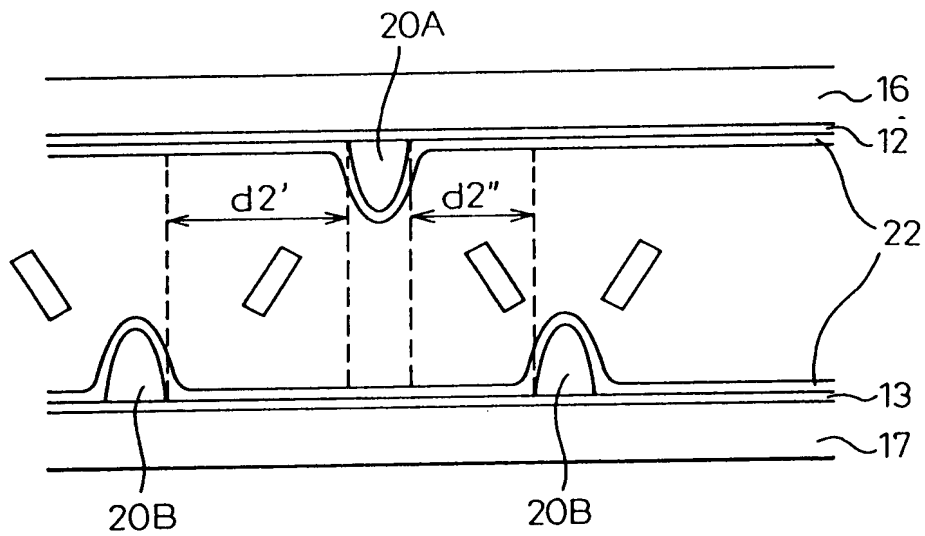


Fig.105B



103/246

Fig.106

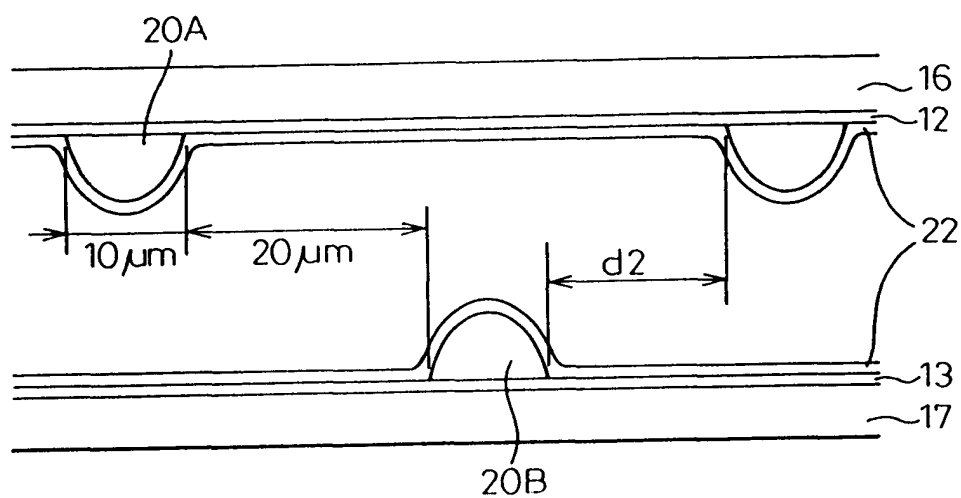
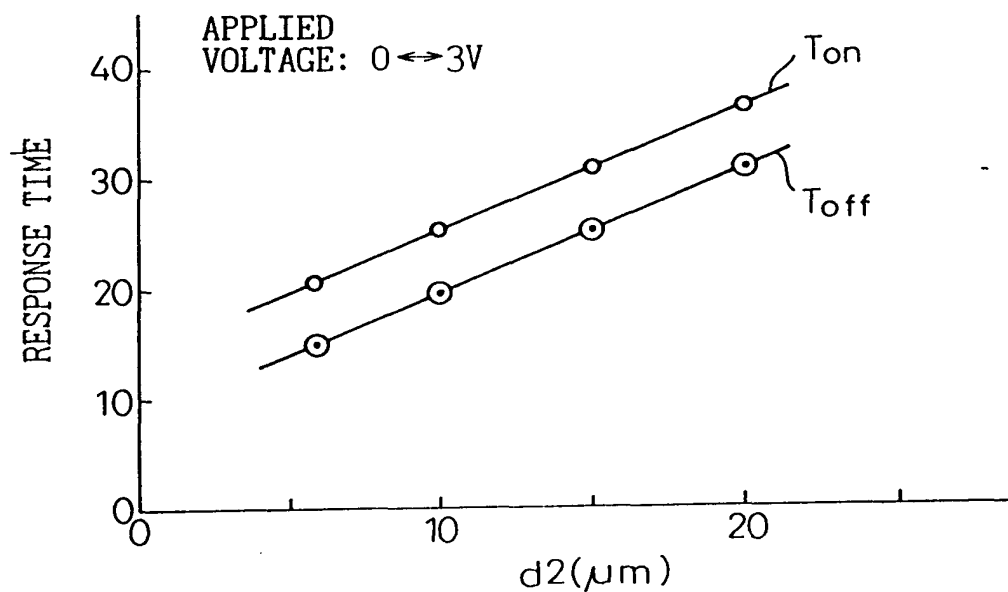


Fig.107



104/246

Fig.108A

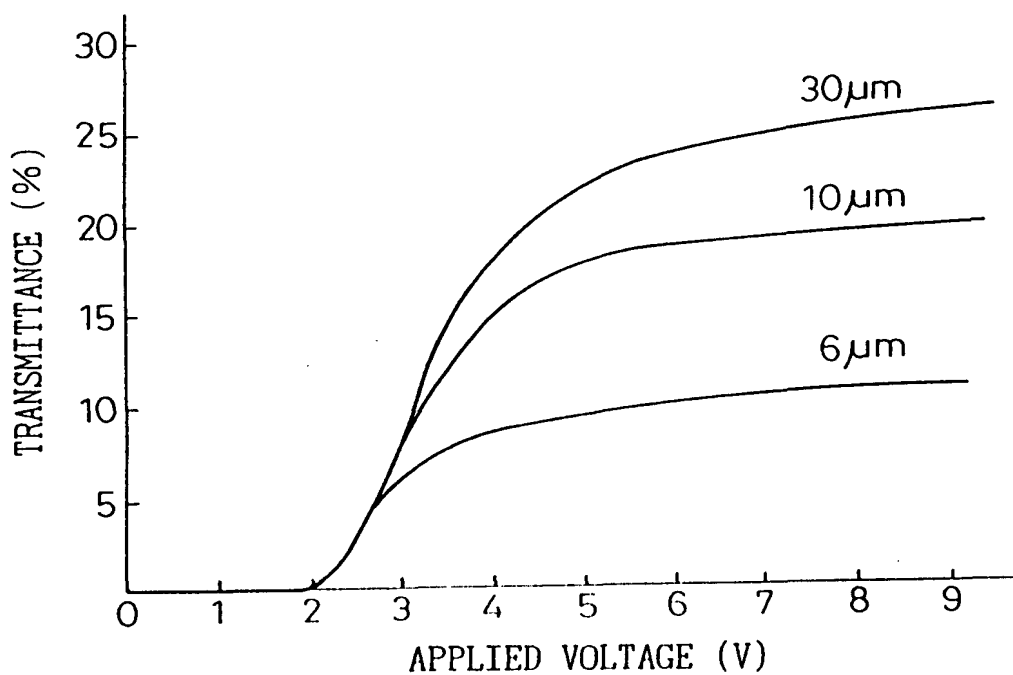
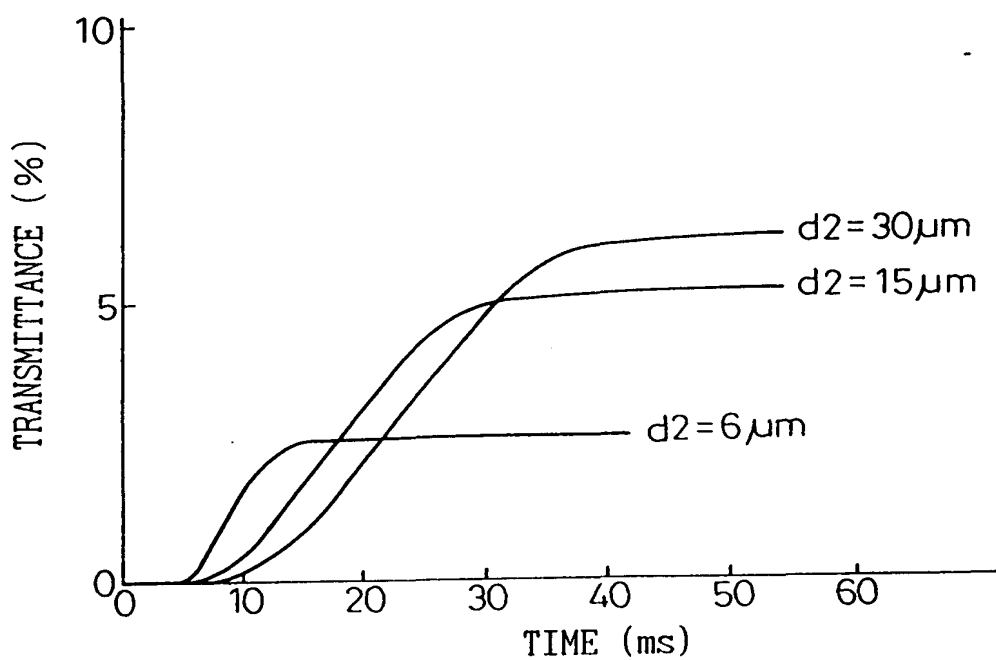


Fig.108B





105/  
246

Fig.109A

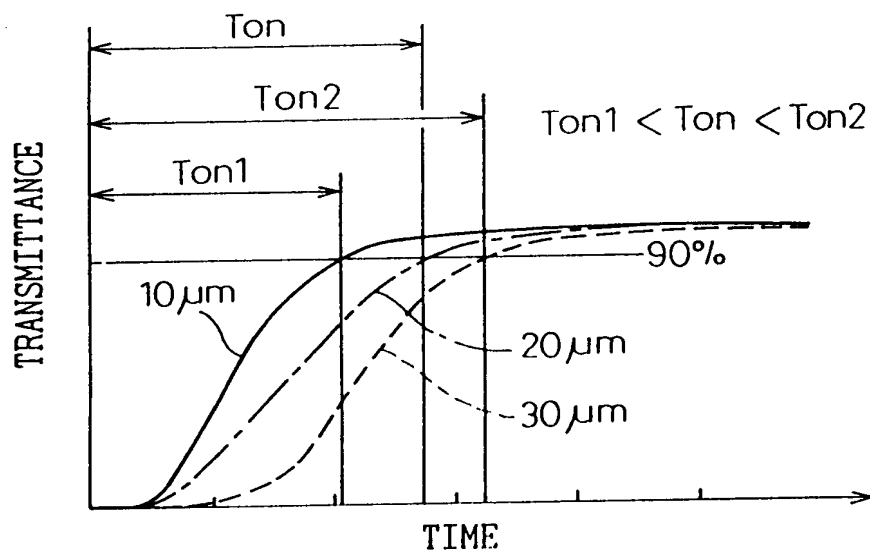
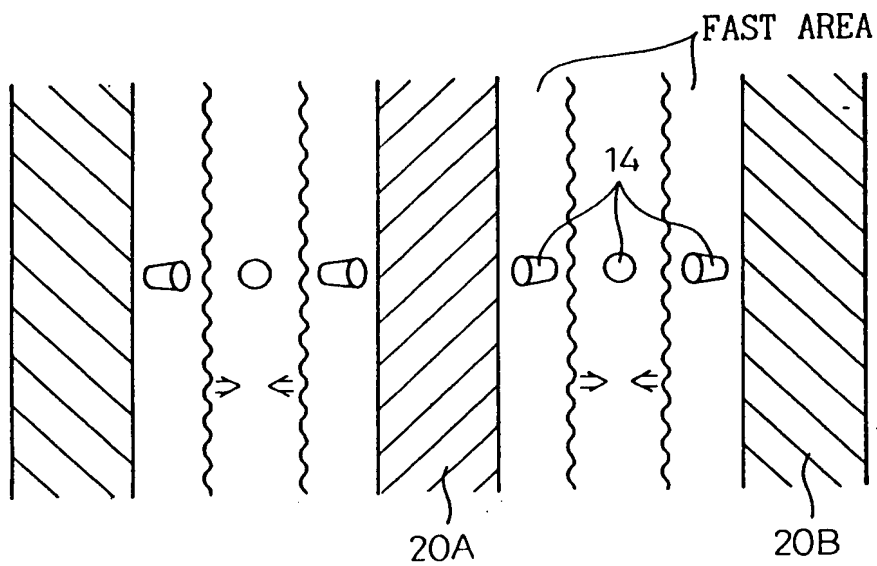
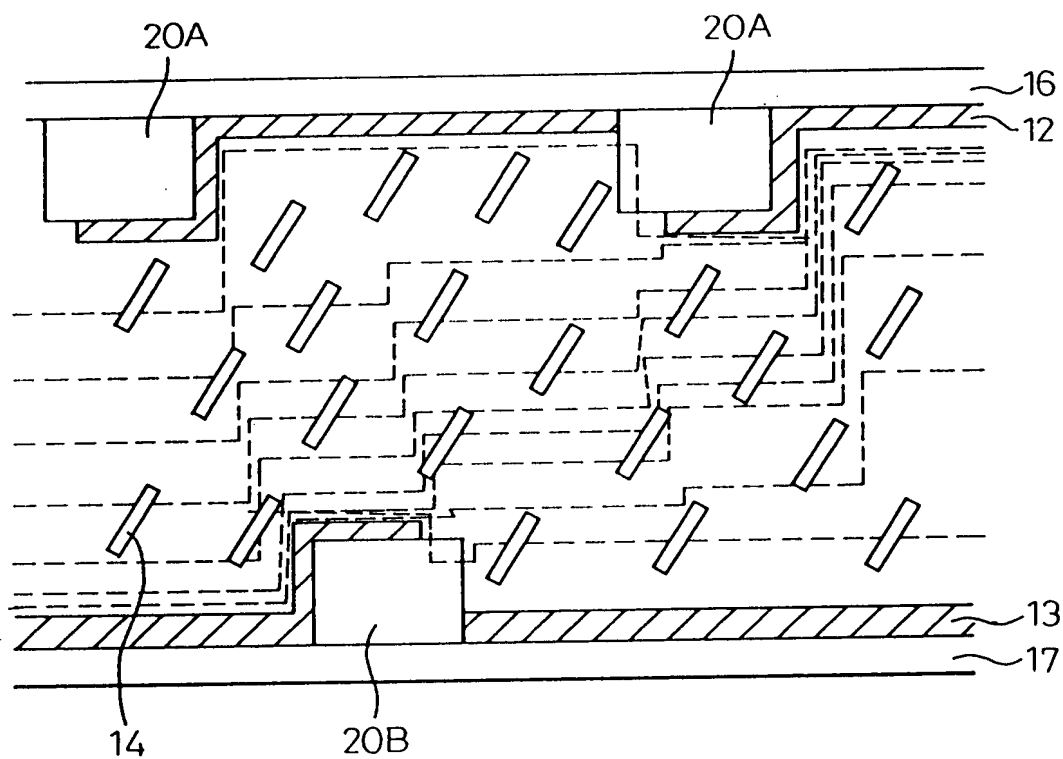


Fig.109B



106/  
246

Fig. 110



107/246

Fig. 111

CONTRAST RATIO	
—————	100.000
-----	50.000
- - - - -	20.000
- . - . -	10.000
- . . . -	5.000

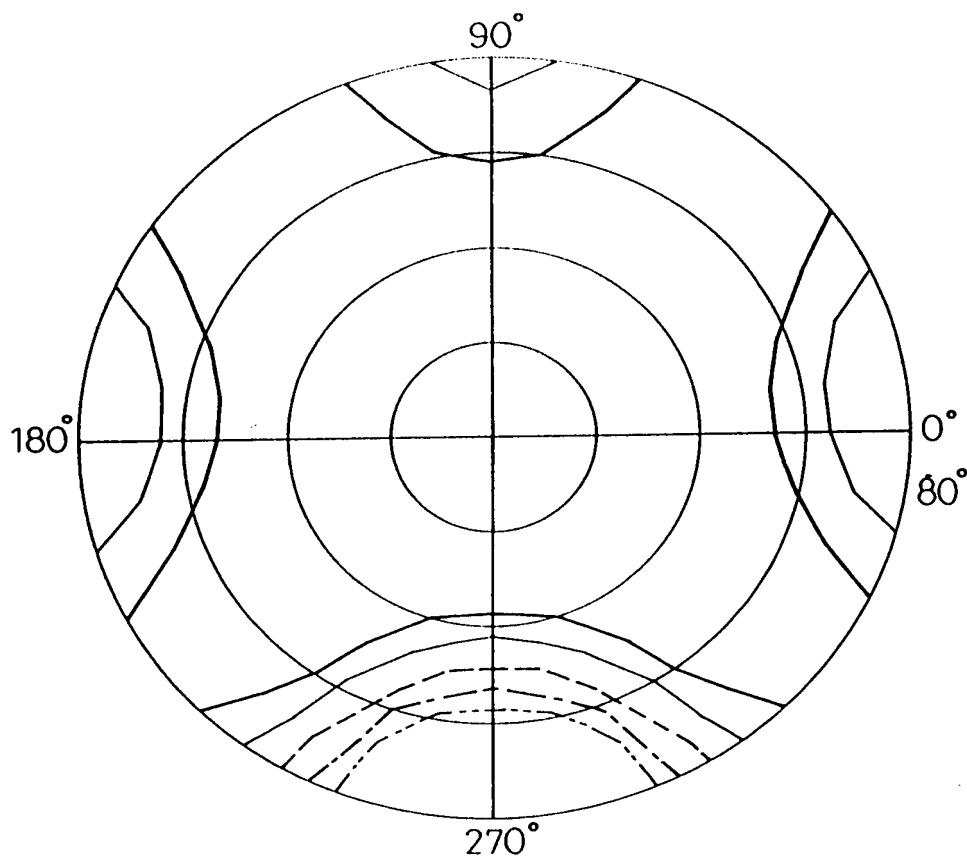
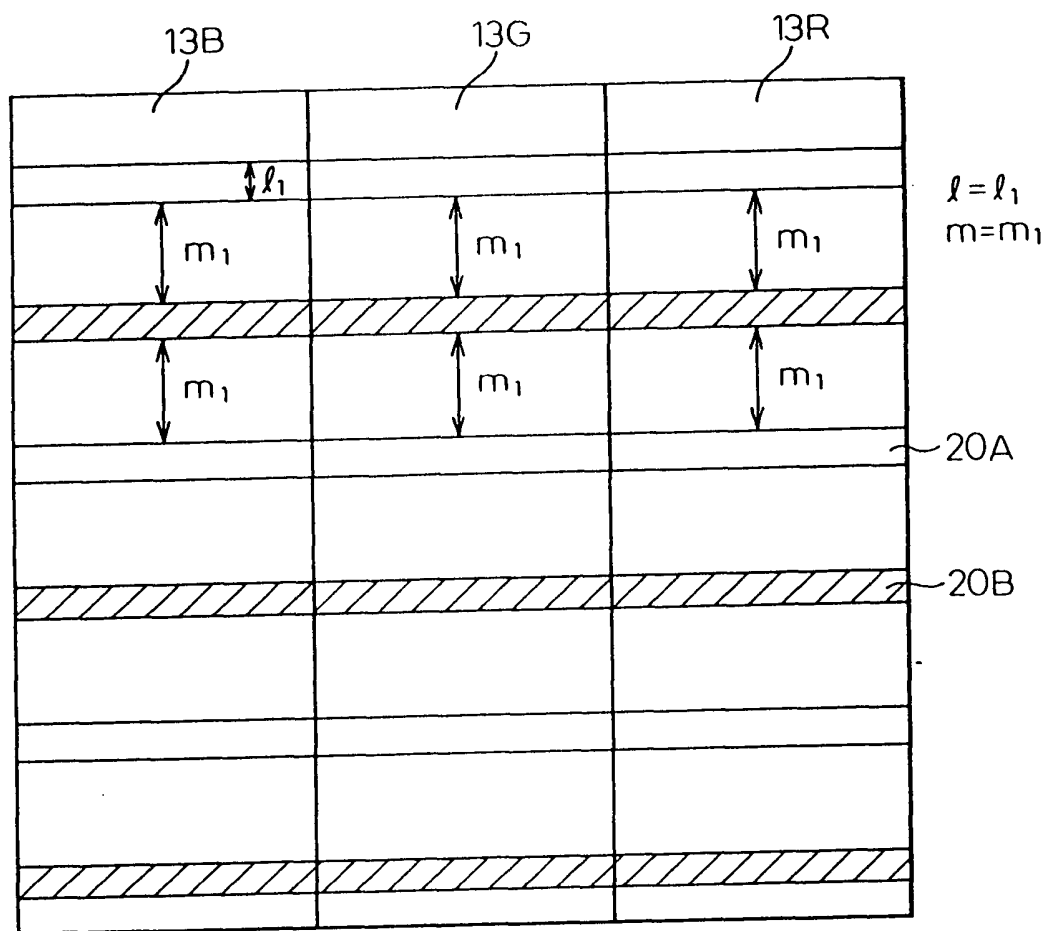


Fig.112



109/  
246

Fig.113

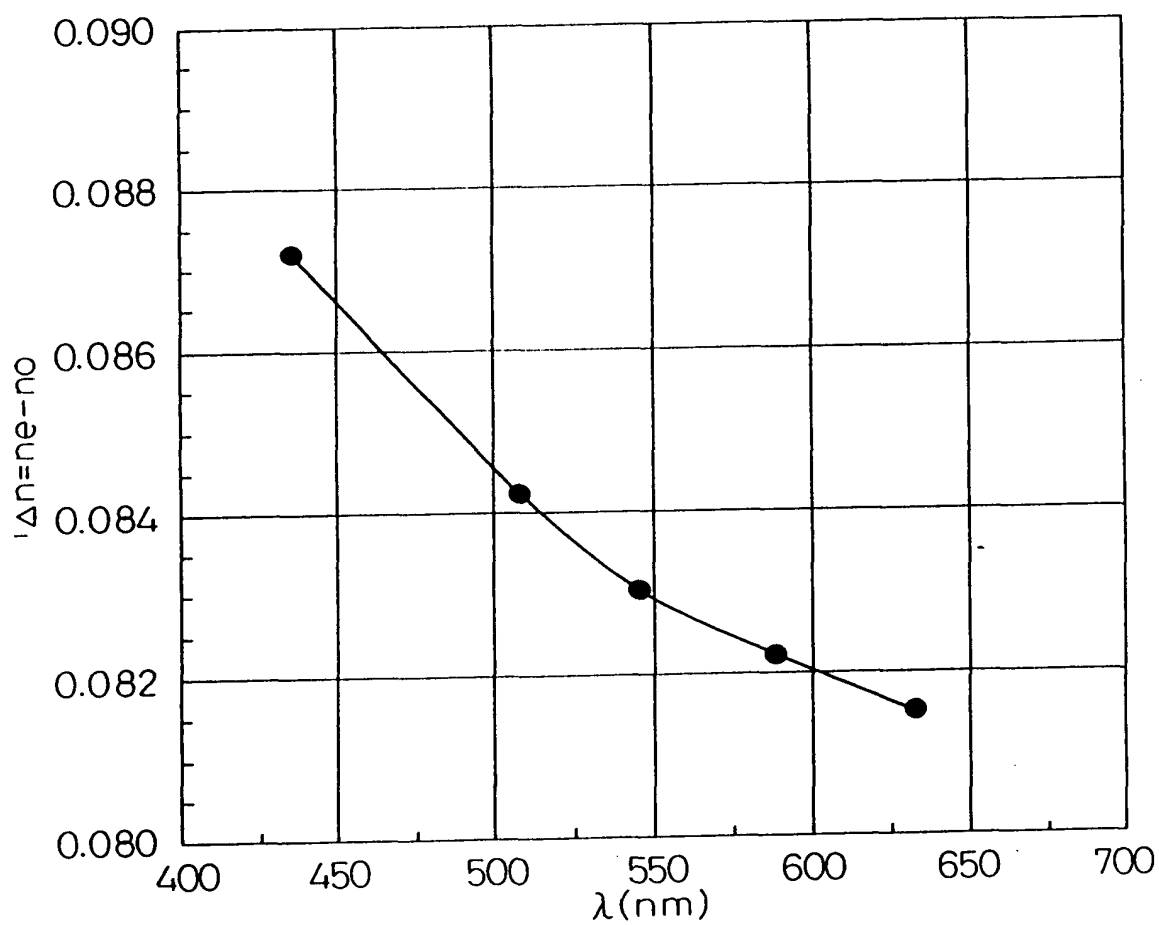
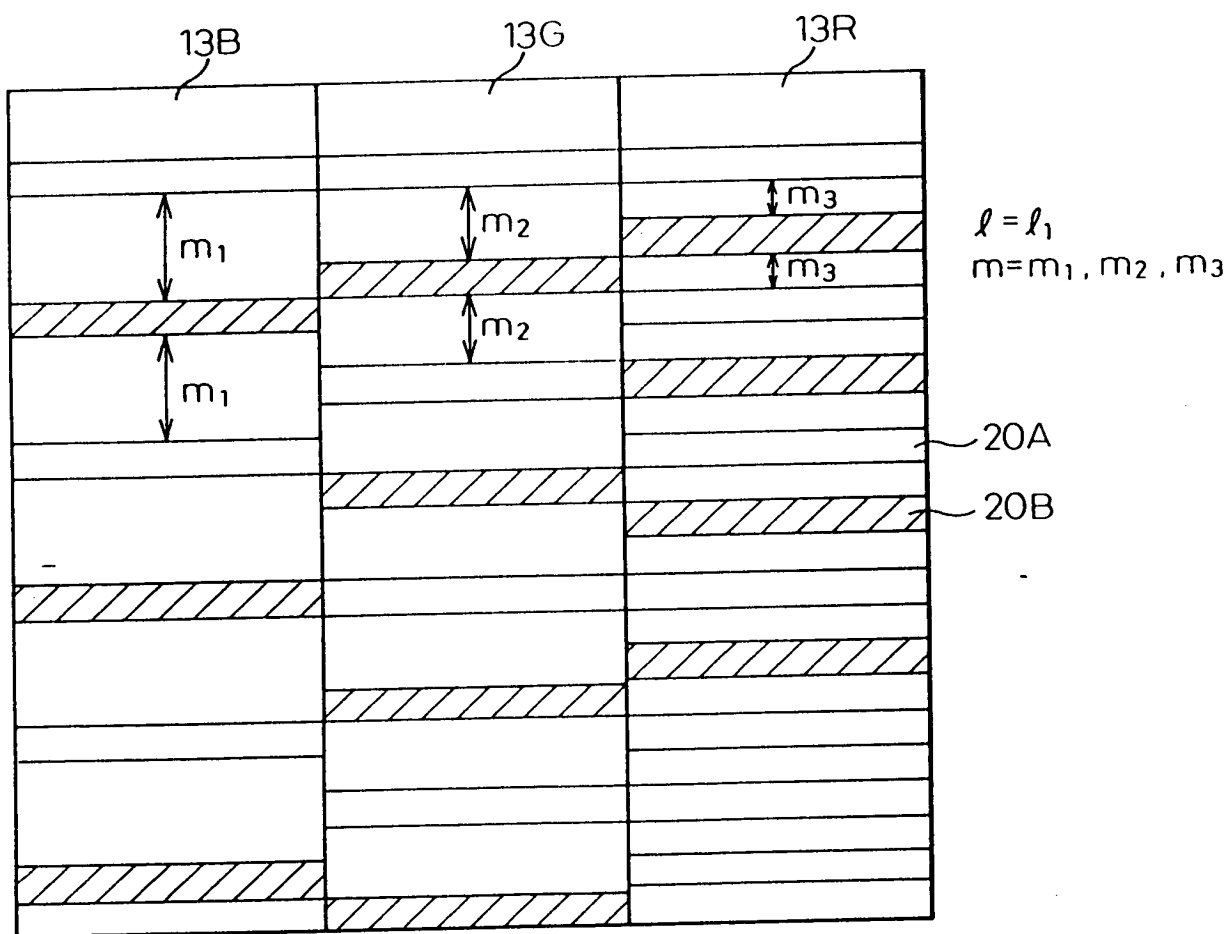
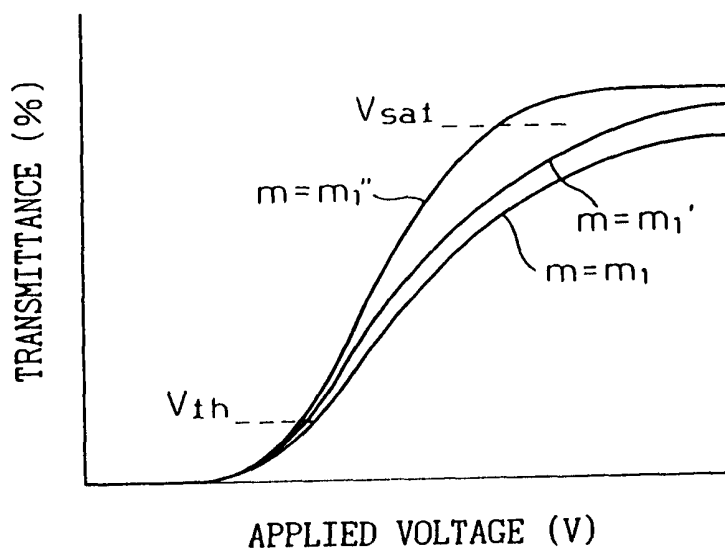


Fig.114



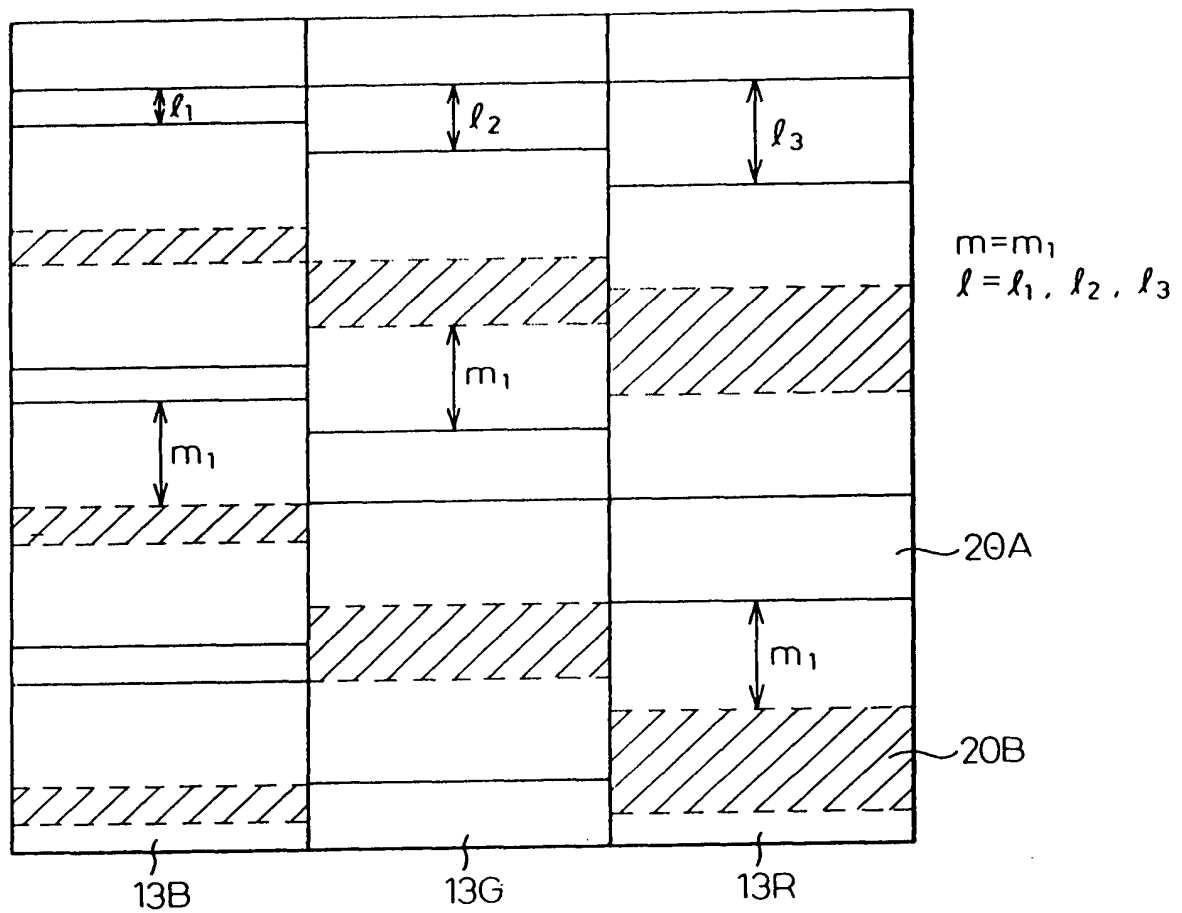
111/246

Fig.115



112/246

Fig.116





113/246

Fig. 117

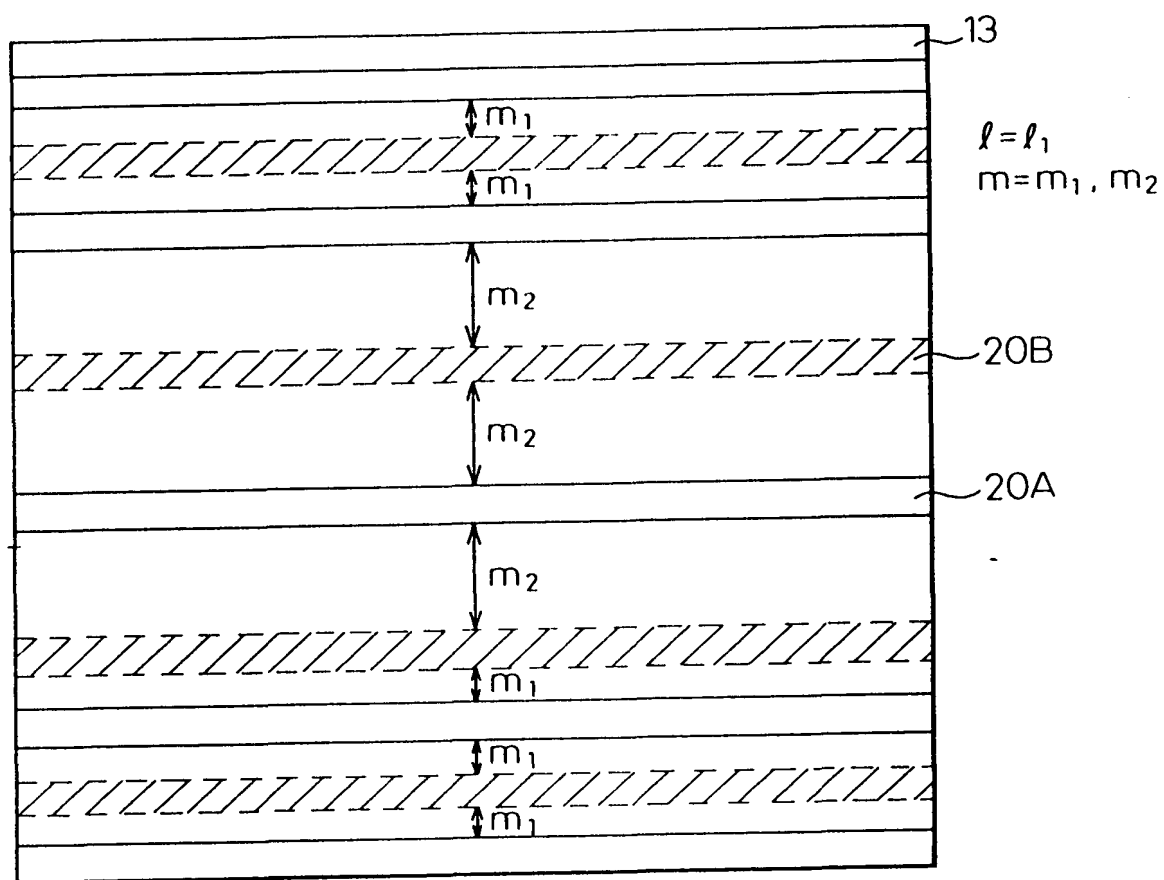


Fig. 118

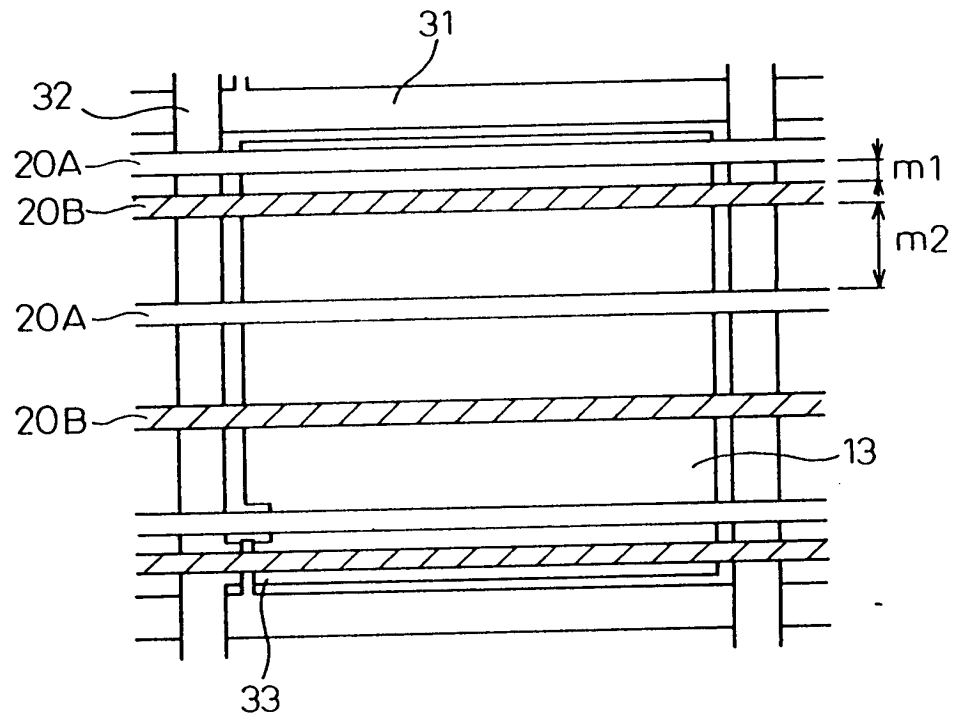


Fig. 119

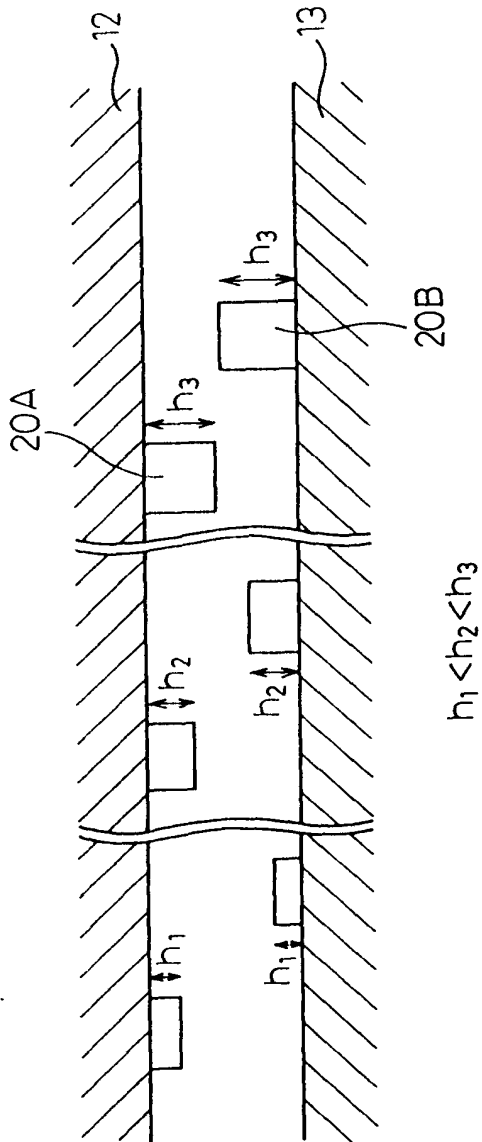


Fig.120

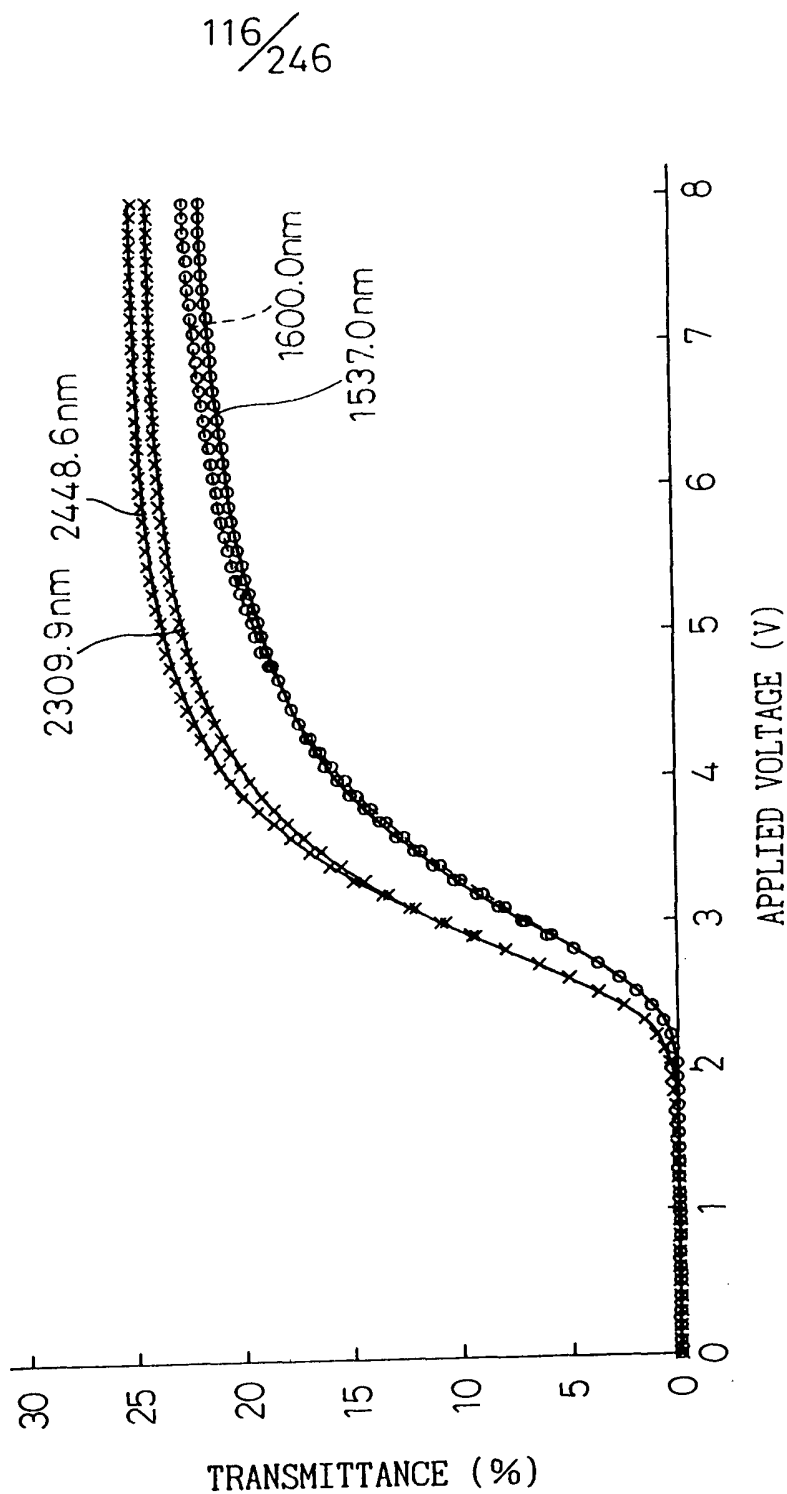
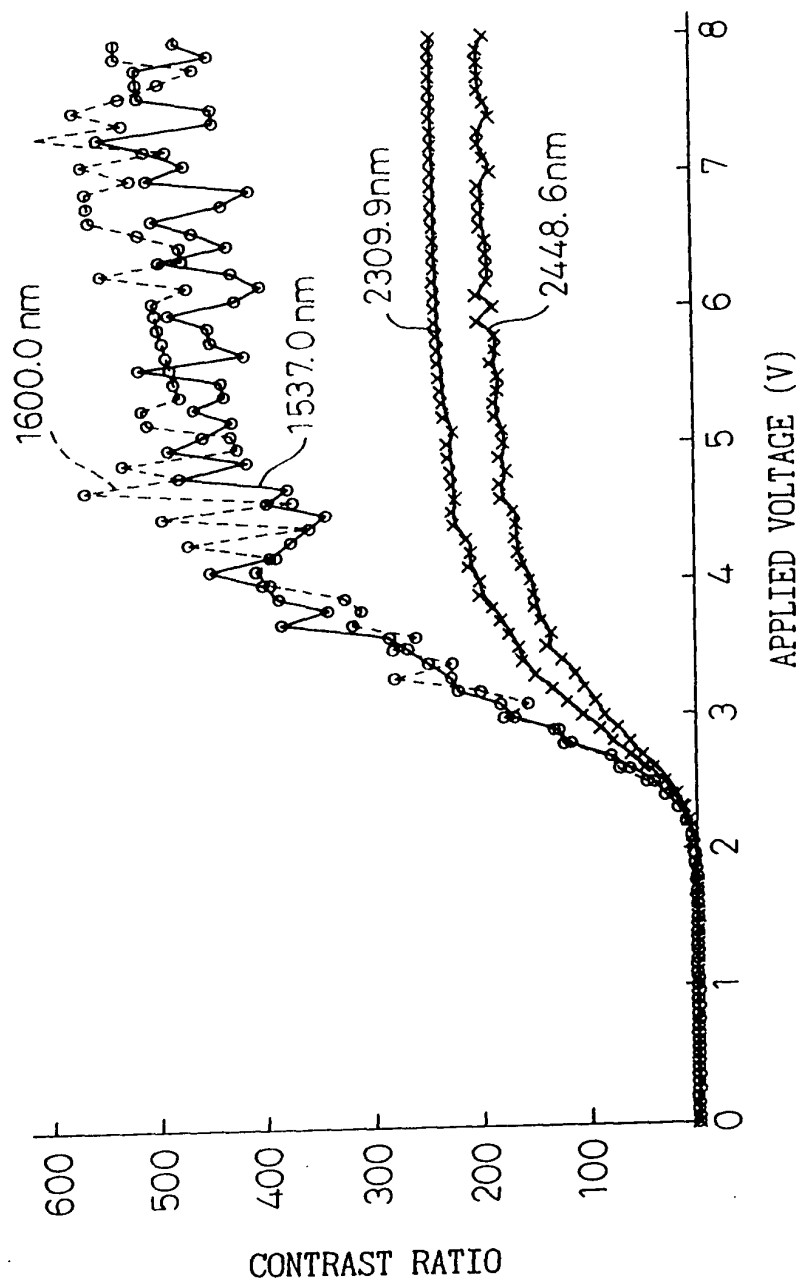


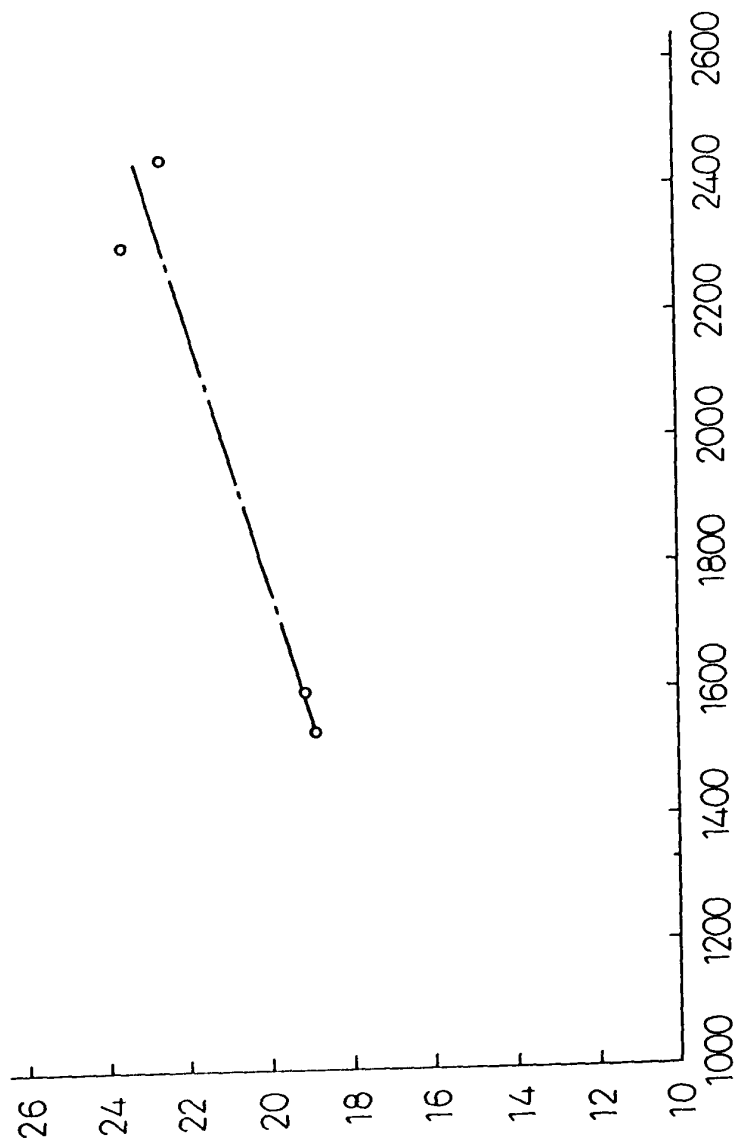
Fig. 121



WHEN 5V IS APPLIED

TRANSMITTANCE (%)

HEIGHT OF AN PROJECTION (nm)

$$\frac{118}{246}$$


[illegible]
$$\frac{119}{246}$$

Fig. 123

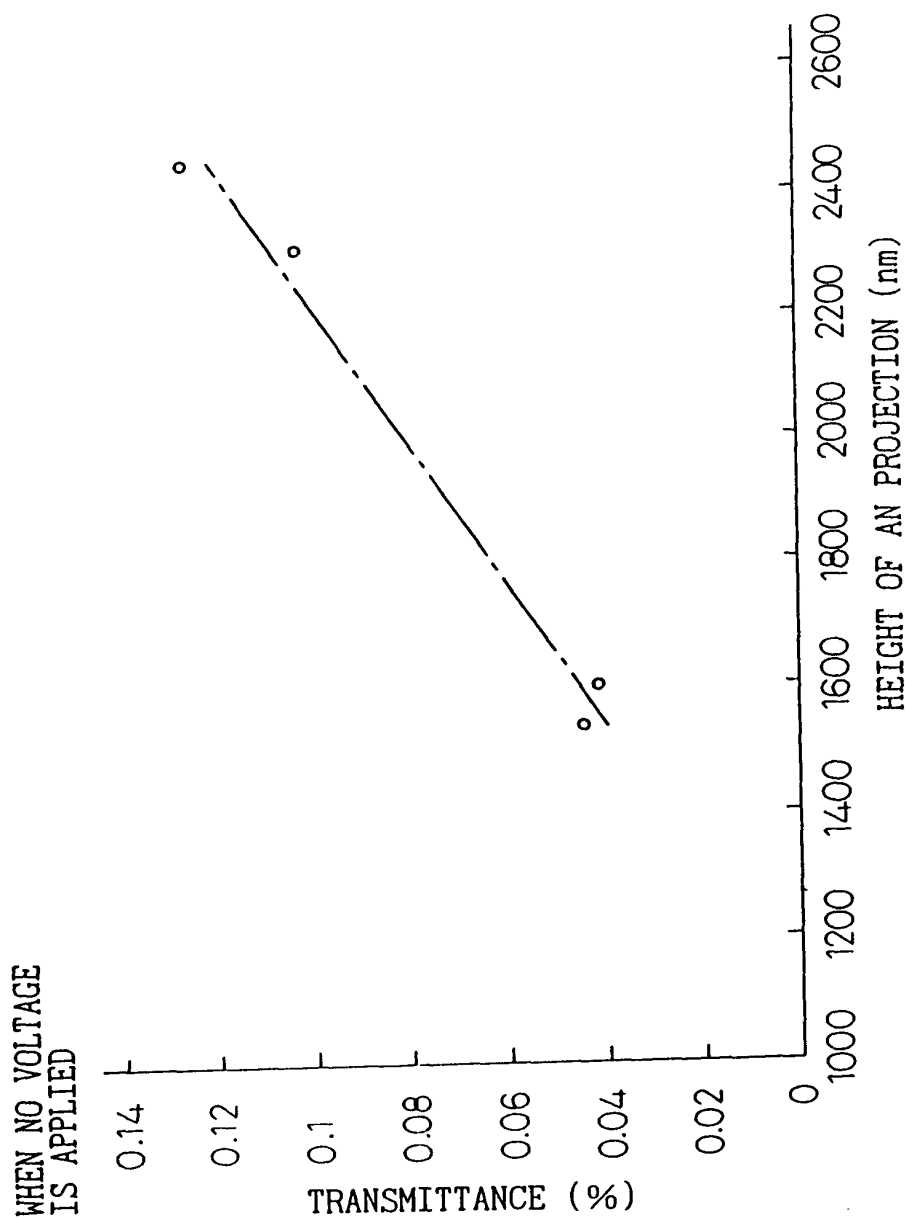


Fig. 124A

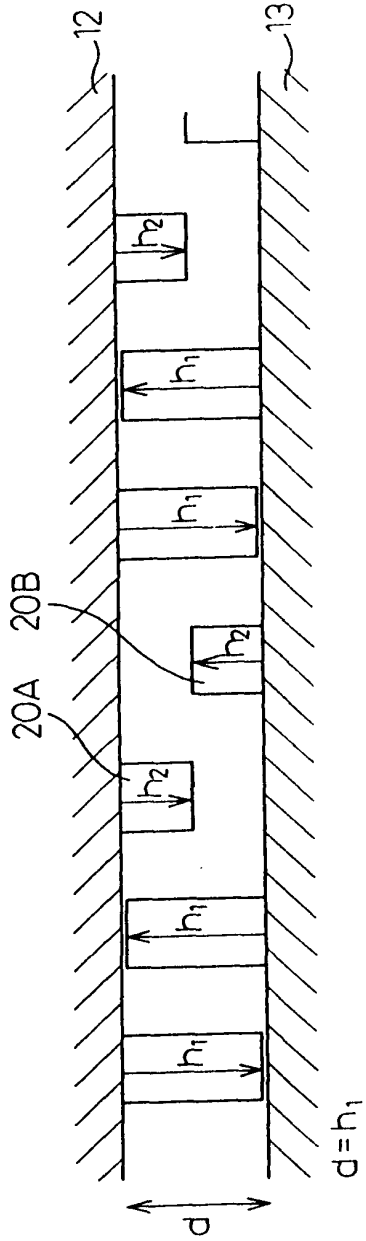


Fig. 124B

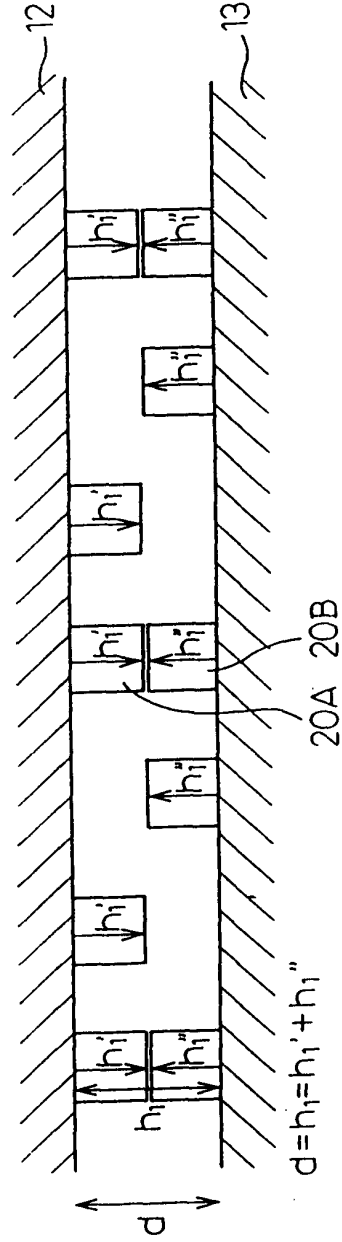




Fig. 125A

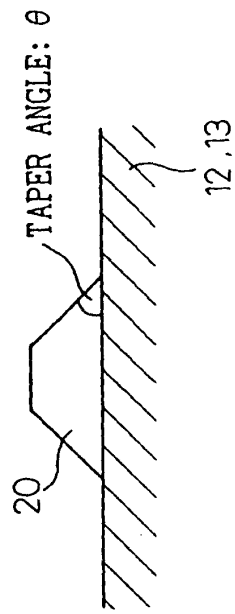


Fig. 125B

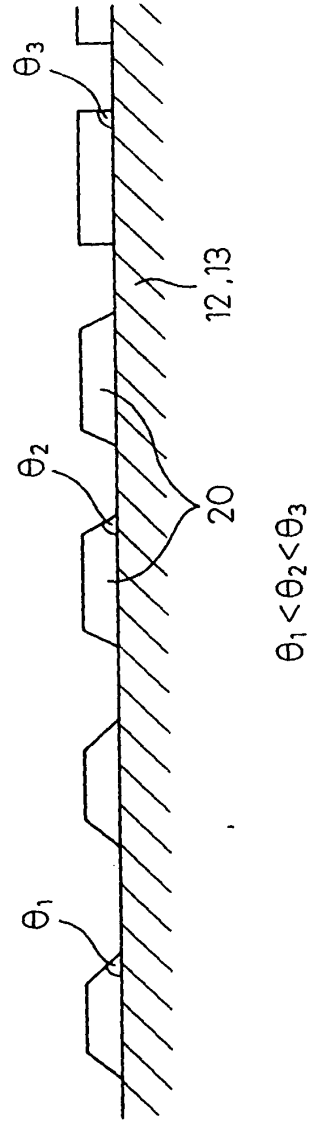
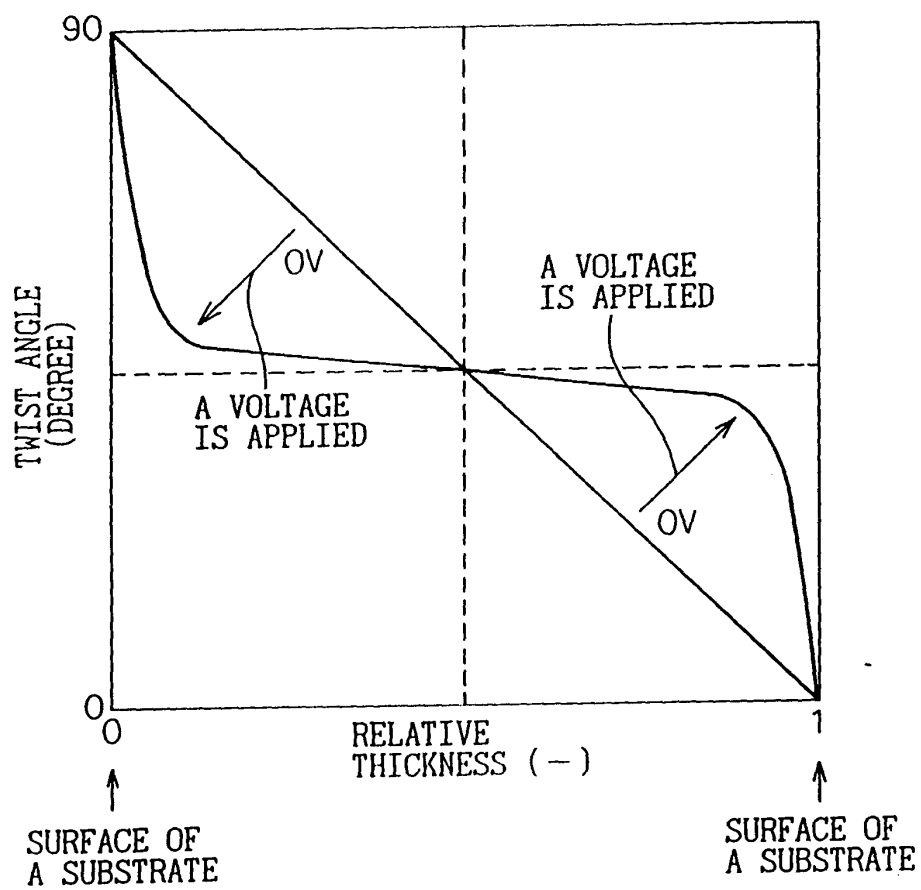
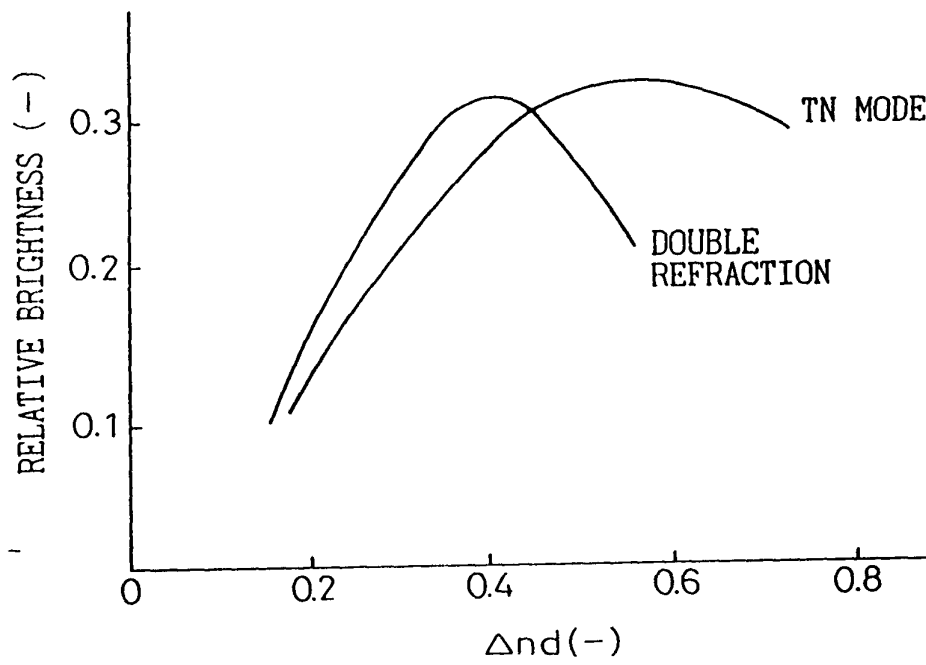


Fig .126



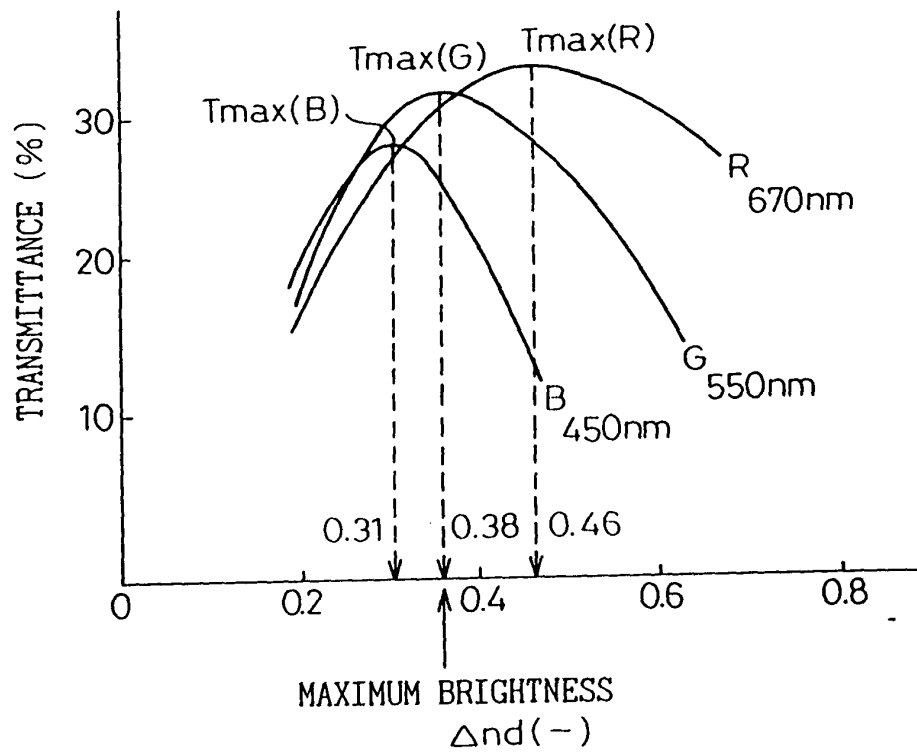
123/246

Fig. 127



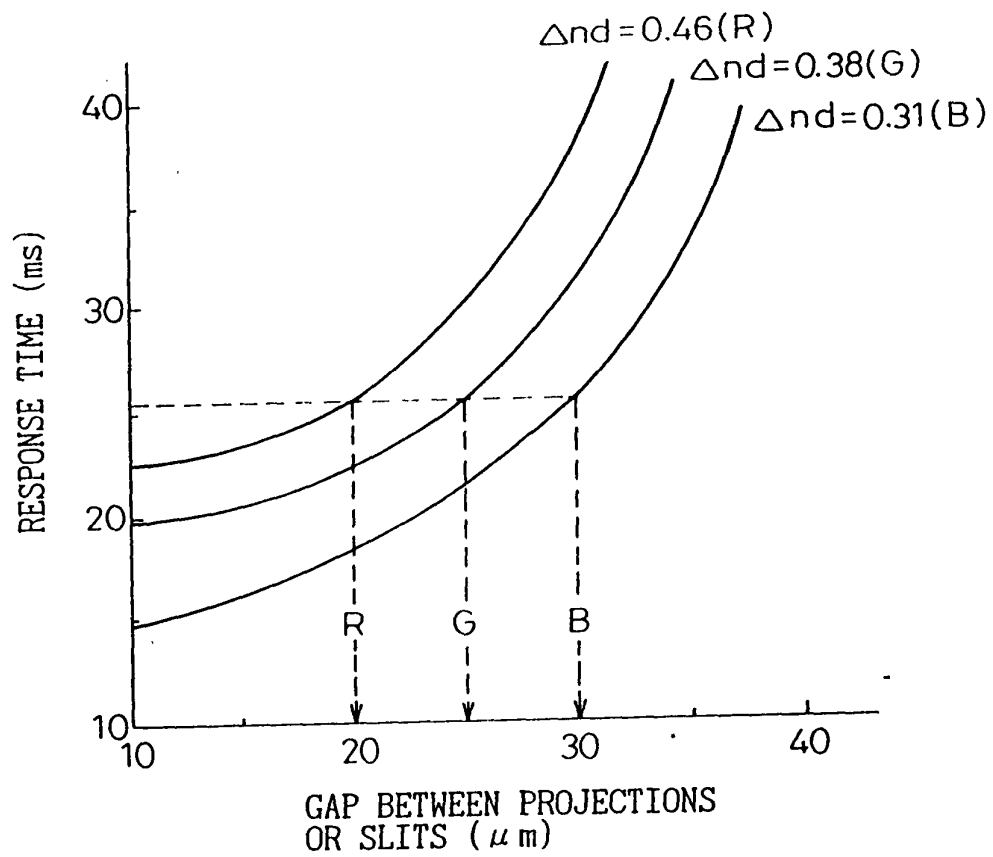
124/  
246

Fig .128



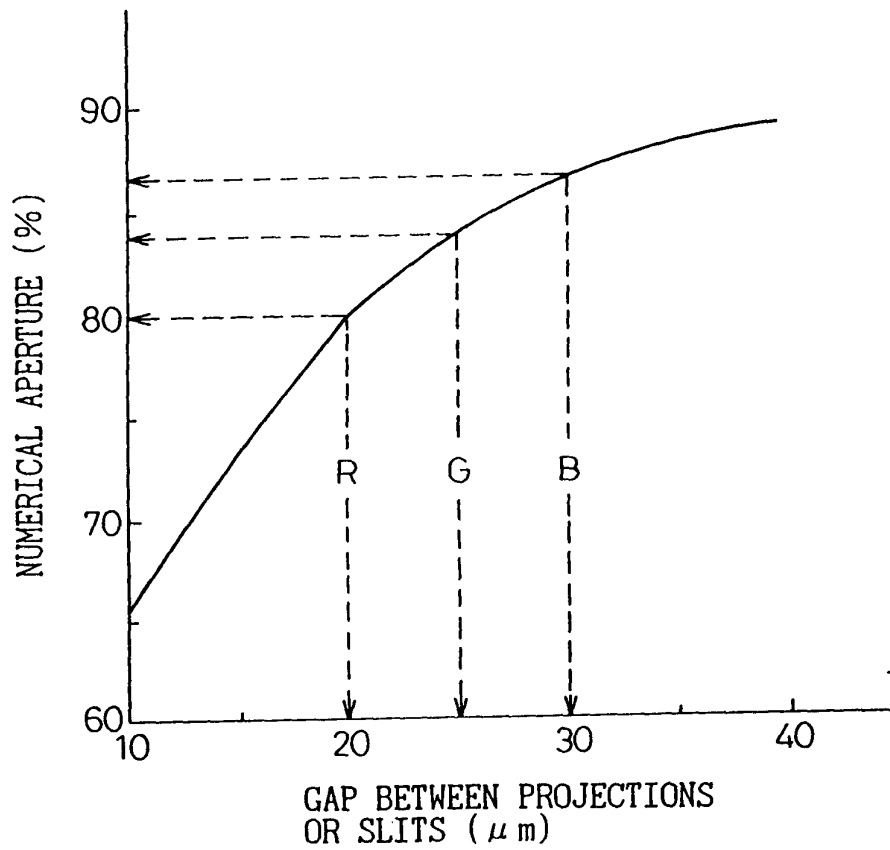
125/  
246

Fig.129



126/246

Fig.130



www.scribd.com

Fig. 131

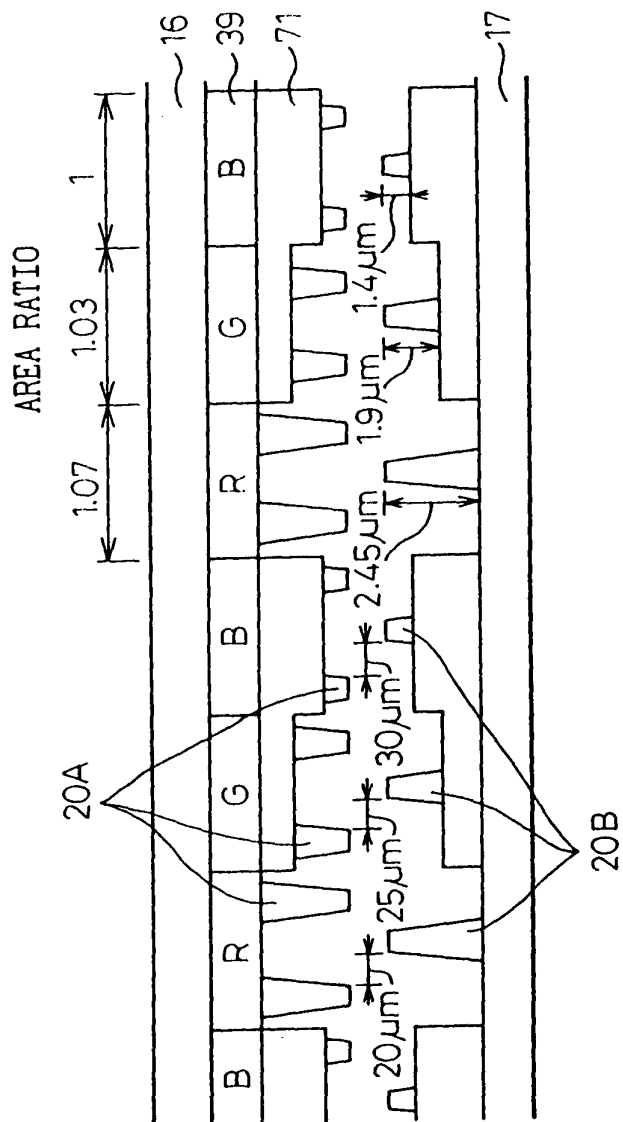


Fig. 132

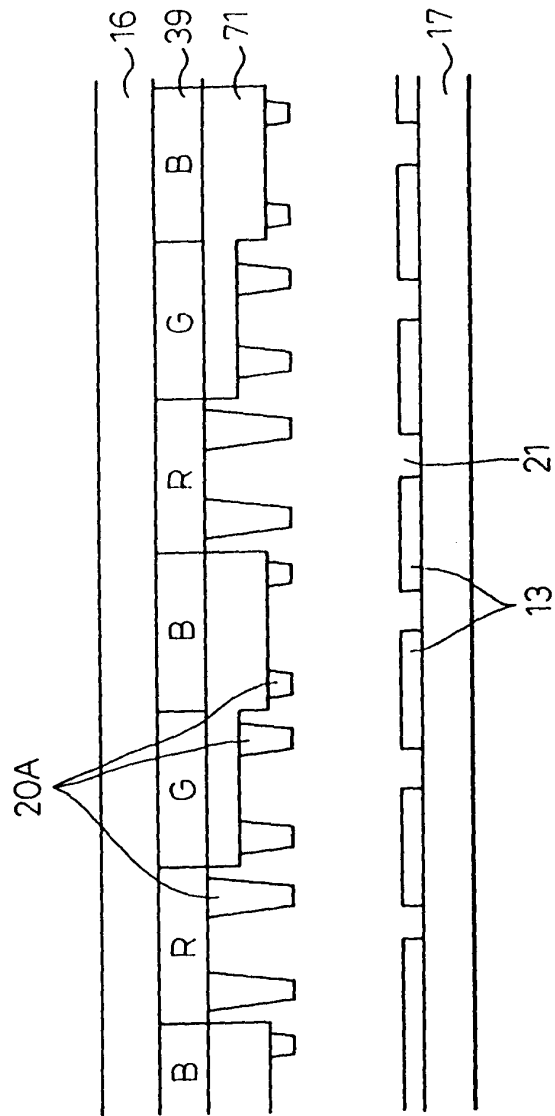




Fig. 133

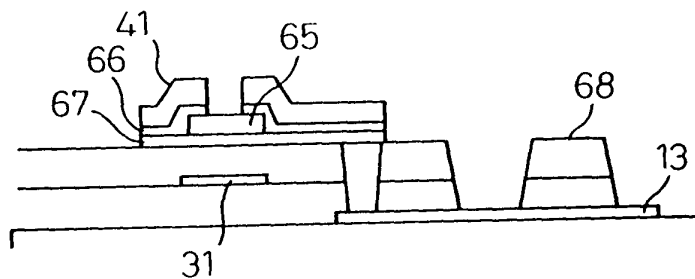


Fig. 134A

Fig. 134B

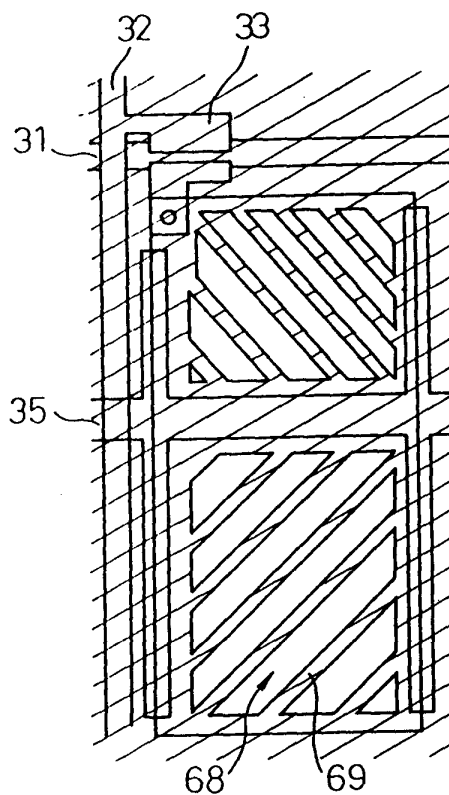
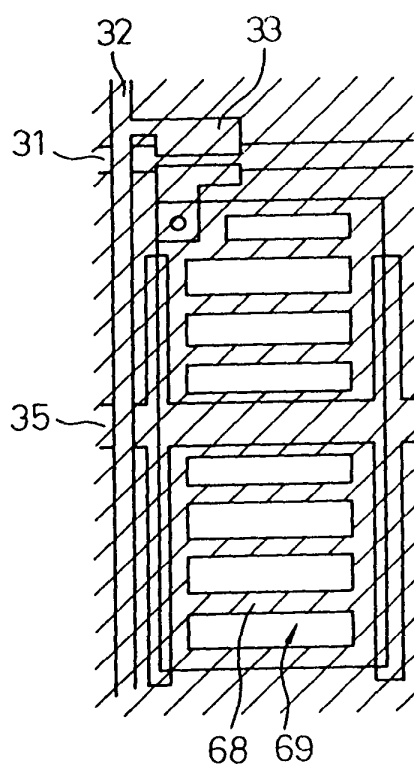


Fig. 135

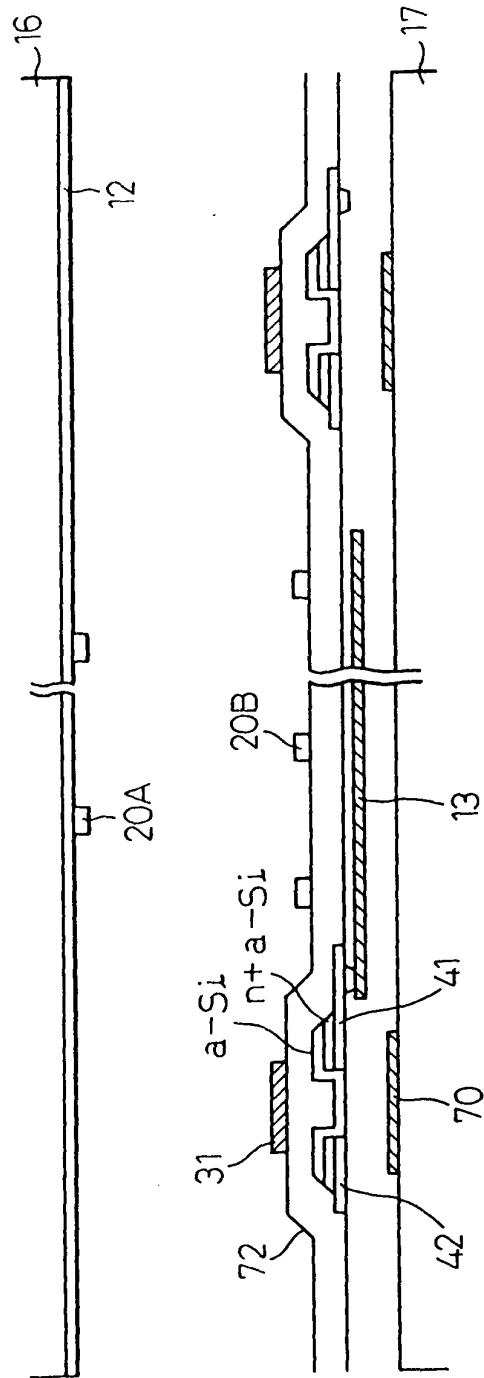
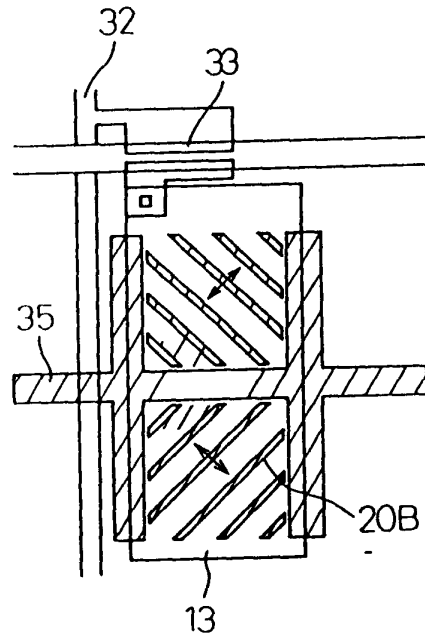
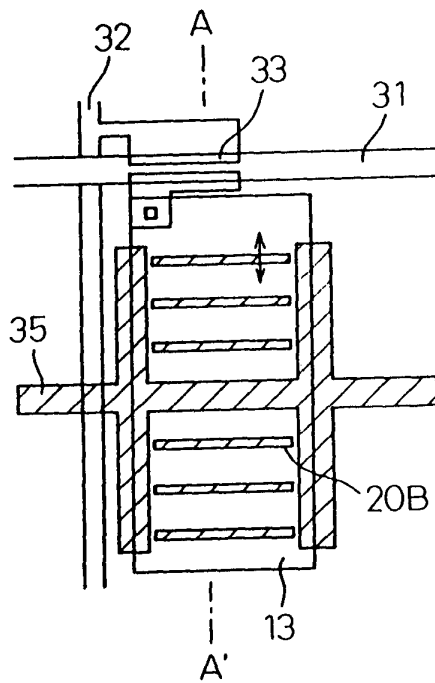


Fig.136A

Fig.136B



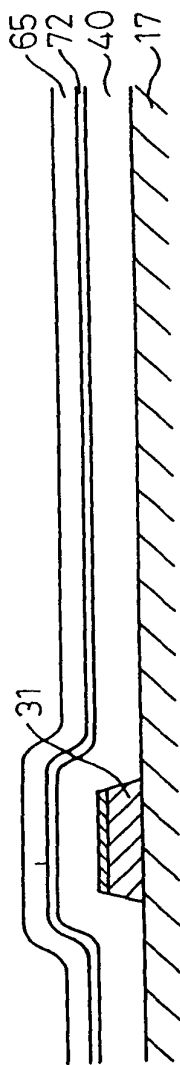


Fig. 137A

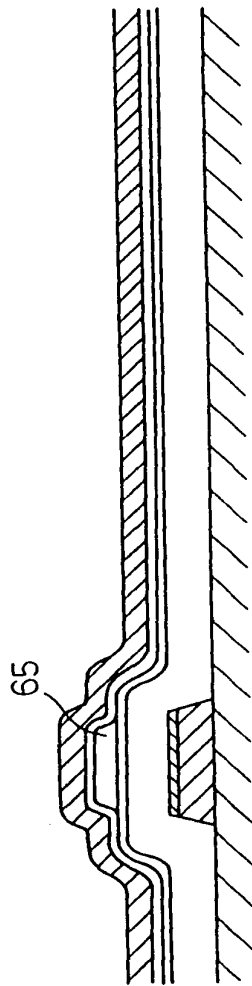


Fig. 137B

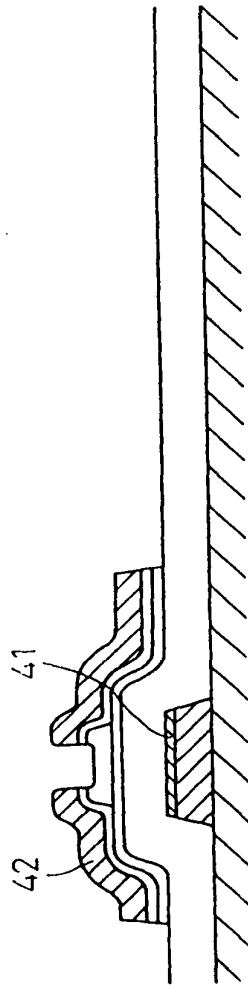


Fig. 137C

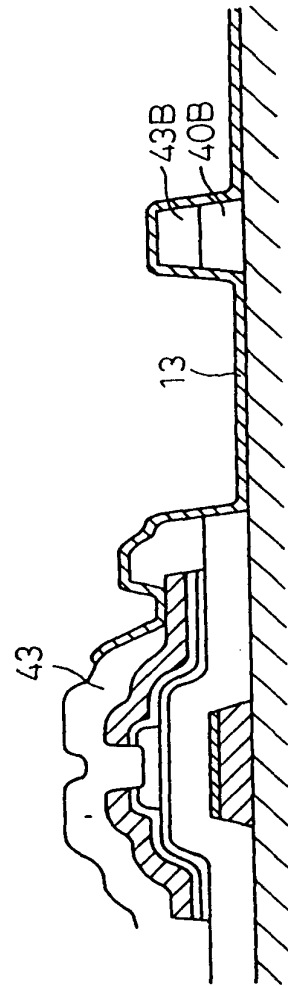


Fig. 137D

Fig. 138

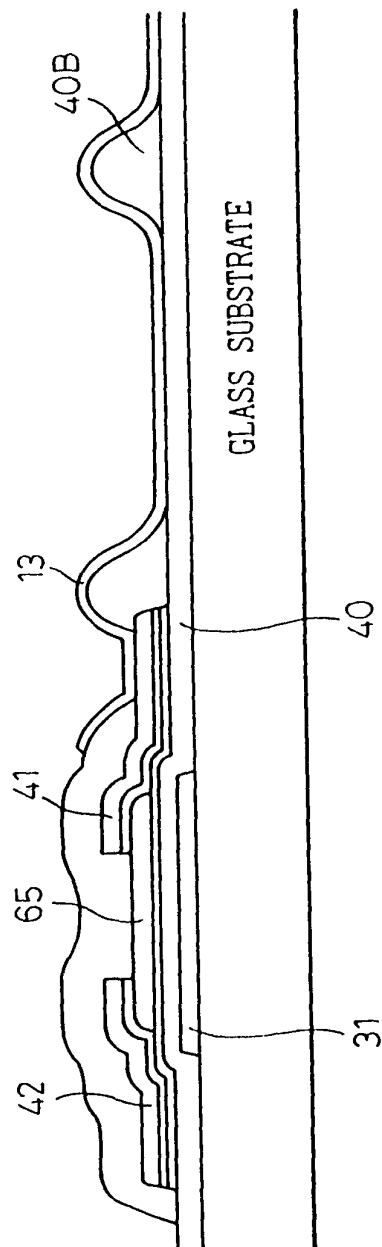


FIG. 139A

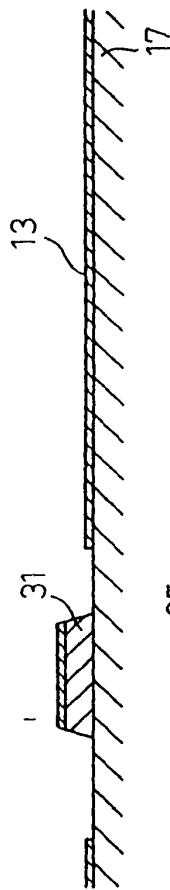


Fig. 139A

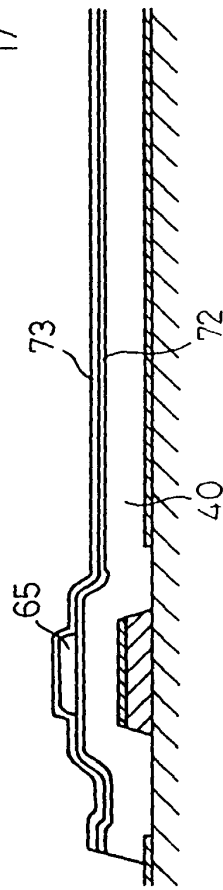


Fig. 139B

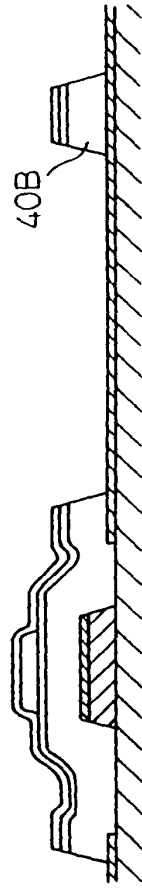


Fig. 139C

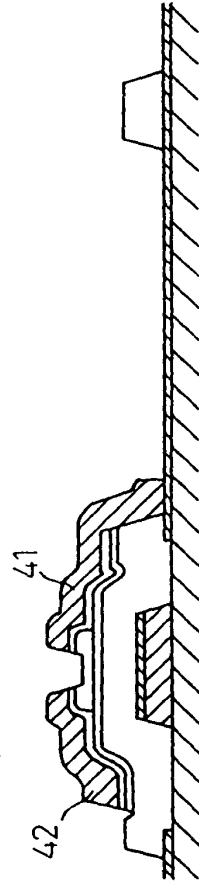


Fig. 139D

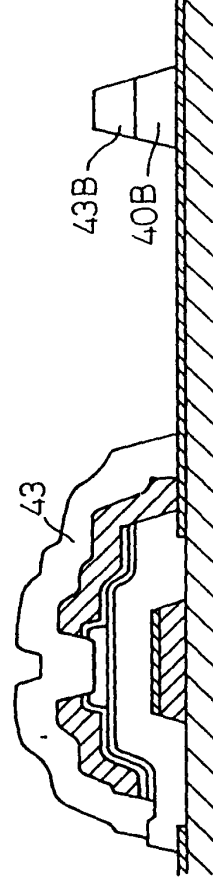


Fig. 139E

135/  
246

Fig.140A

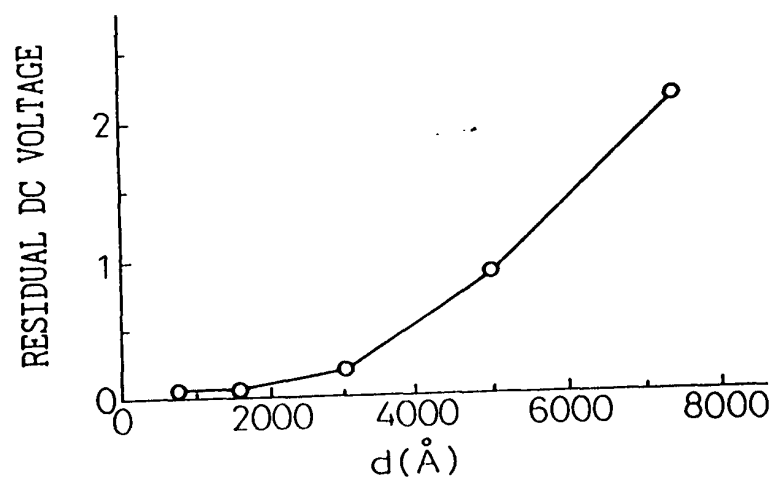
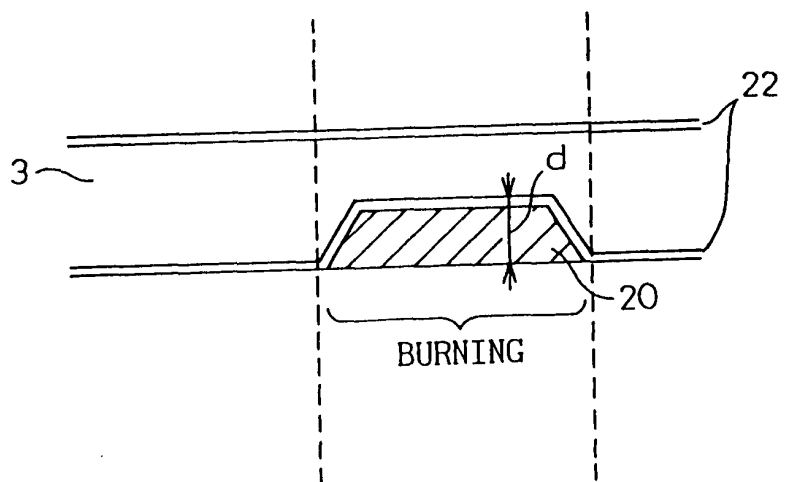


Fig.140B



136/  
246

Fig.141A

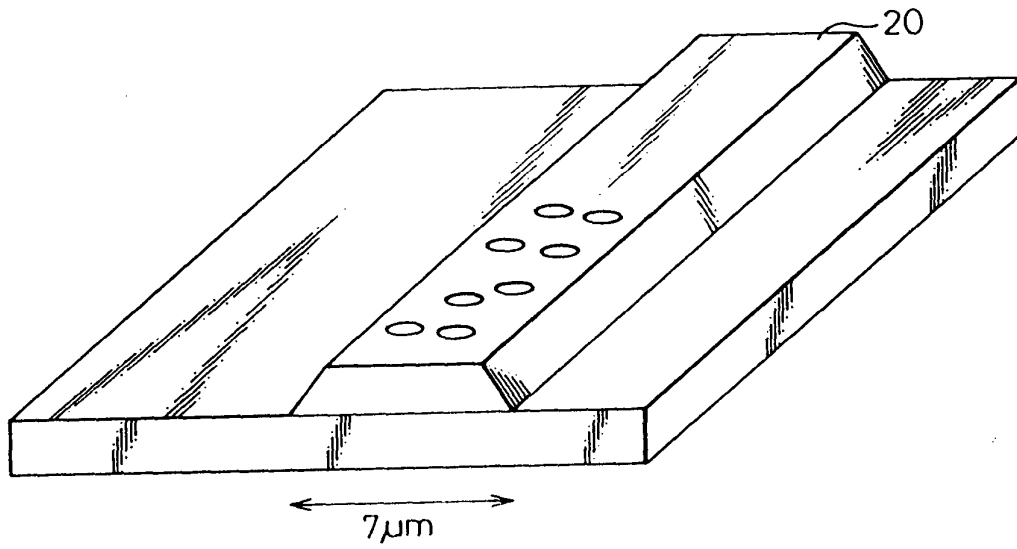
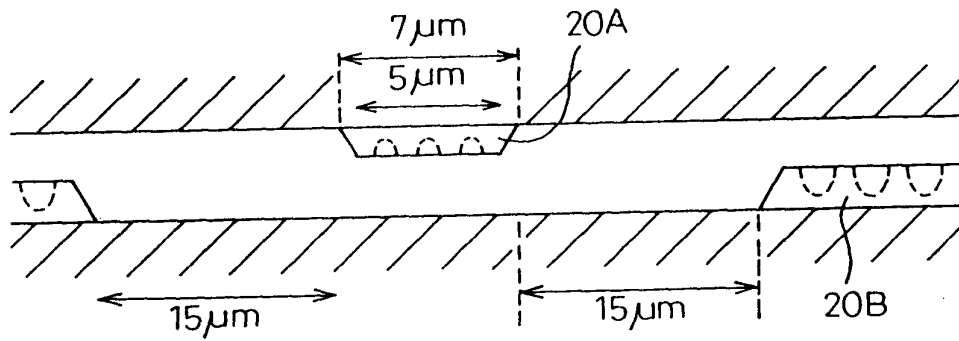


Fig.141B





137/246

Fig.142A

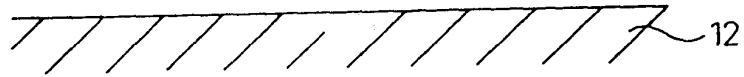


Fig.142B

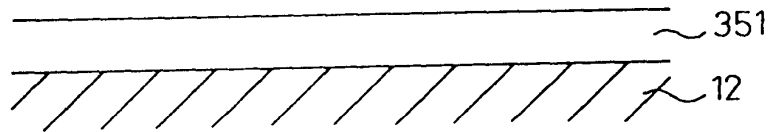


Fig.142C

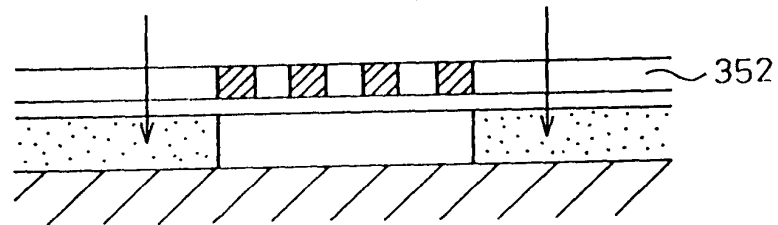


Fig.142D

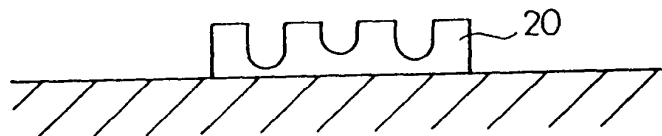
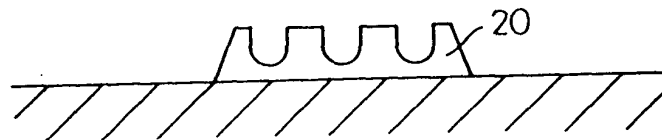
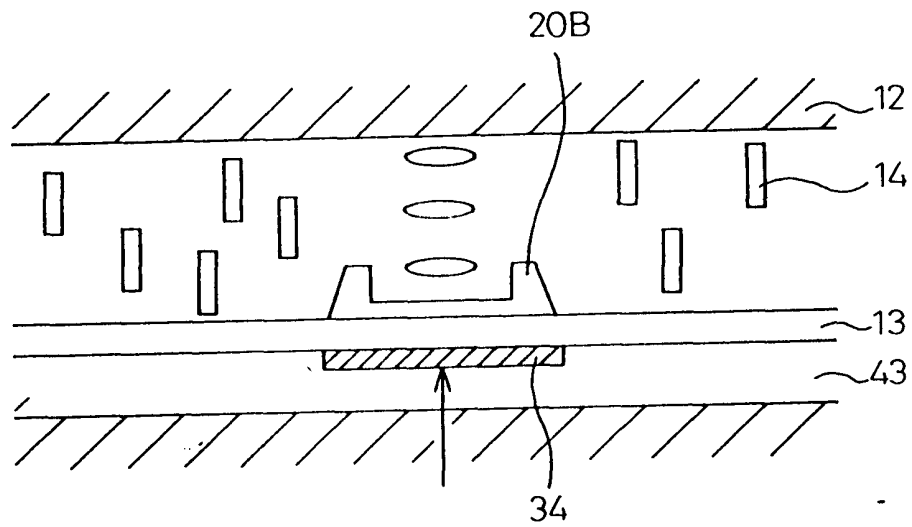


Fig.142E



138/  
246

Fig.143



139/  
246

Fig. 144A

BEFORE BAKING

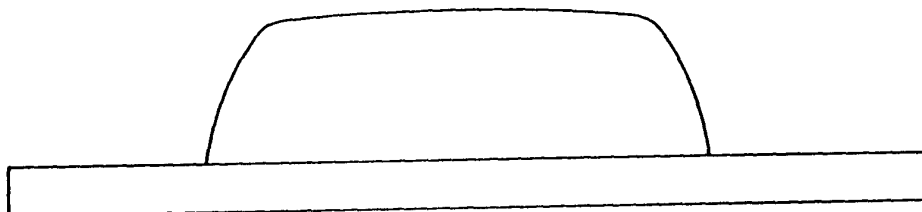


Fig. 144B

AFTER BAKING

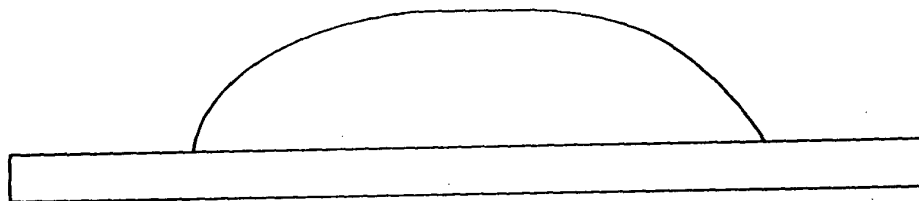


Fig.145A NO BAKING

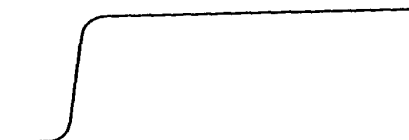


Fig.145B 120°C

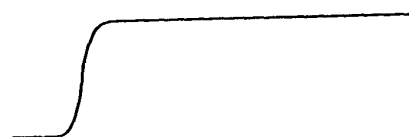


Fig.145C 130°C

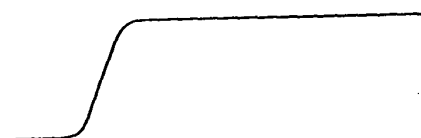


Fig.145D 140°C



Fig.145E 150°C

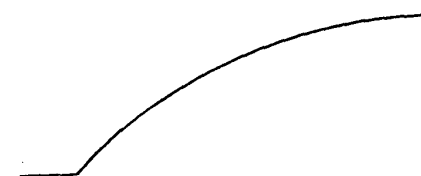


Fig. 145A : NO BAKING  
Fig. 145B : 120°C  
Fig. 145C : 130°C  
Fig. 145D : 140°C  
Fig. 145E : 150°C

141/246

Fig.146A

2  $\mu$ m WIDTH

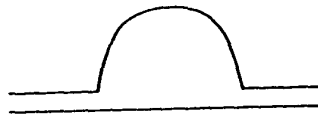


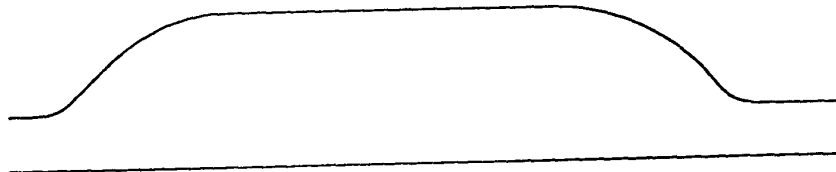
Fig.146B

5  $\mu$ m WIDTH



Fig.146C

10  $\mu$ m WIDTH



142/246

Fig.147A

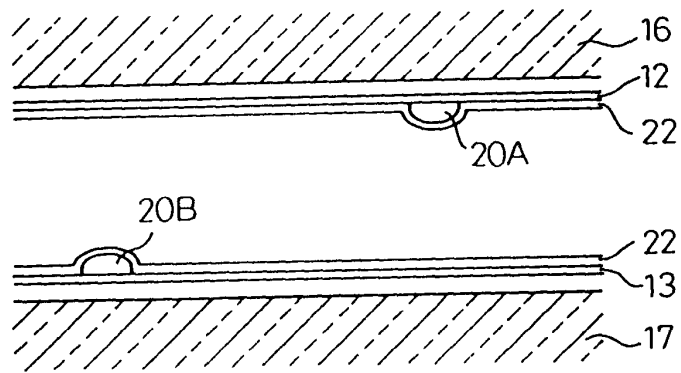
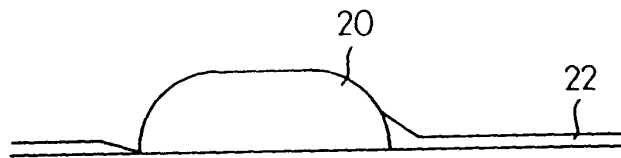


Fig.147B



143/  
246

Fig.148A

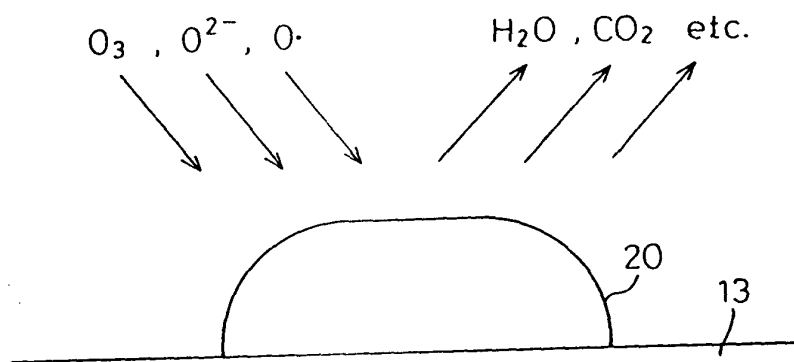


Fig.148B

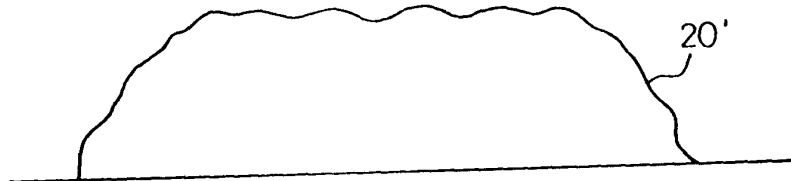
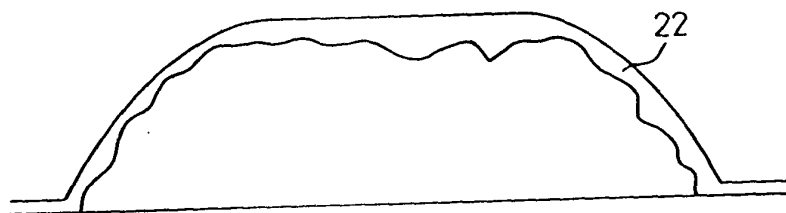


Fig.148C



144/246

Fig.149A

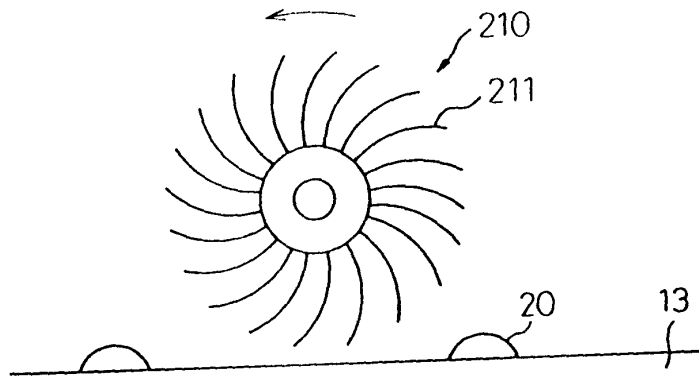
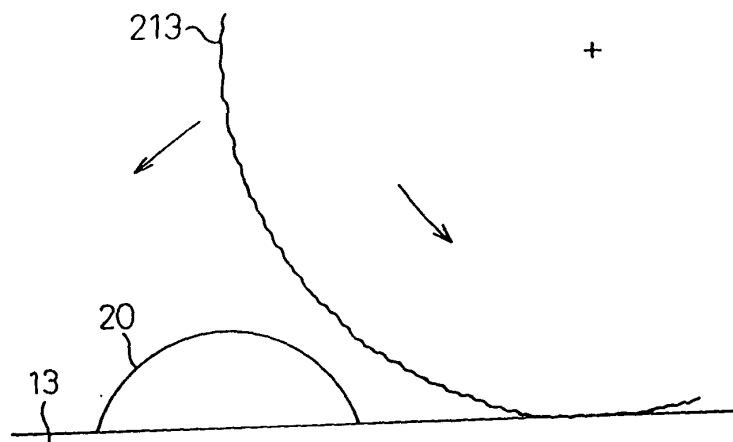


Fig.149B

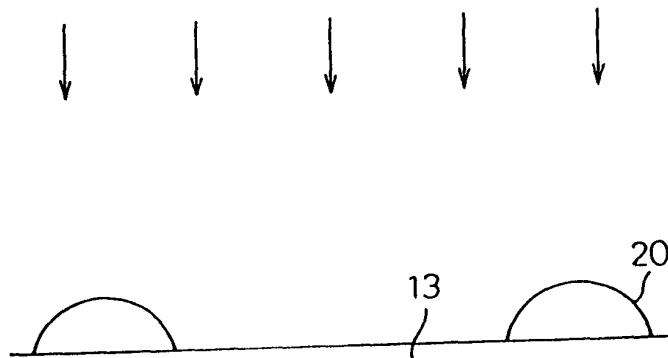




145/  
246

Fig. 150

ULTRA-VIOLET LIGHT



146/246

Fig.151A

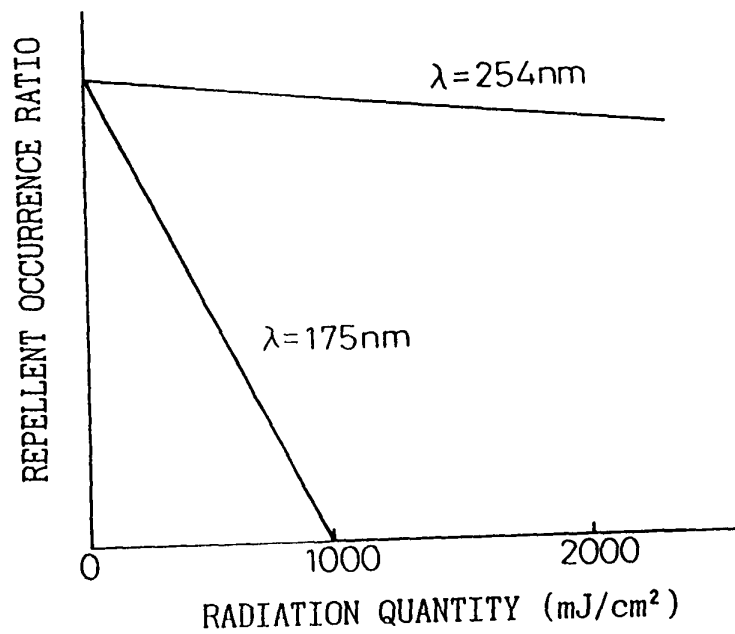
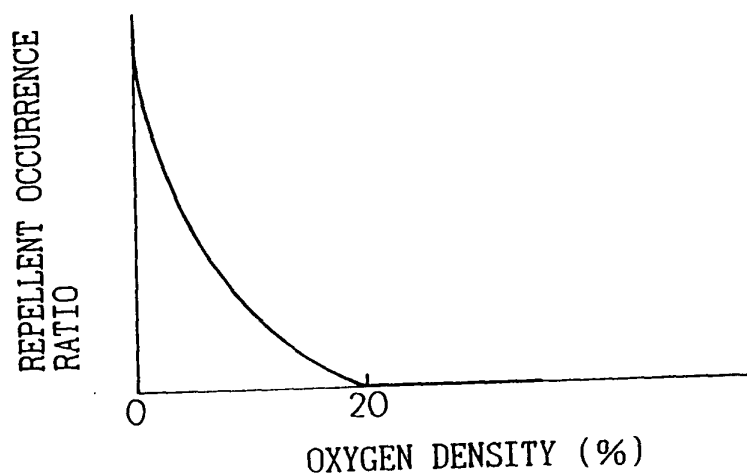


Fig.151B



147/246

Fig.152A

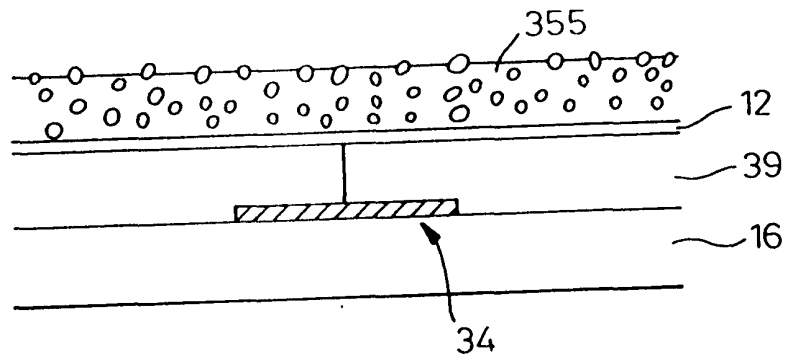


Fig.152B

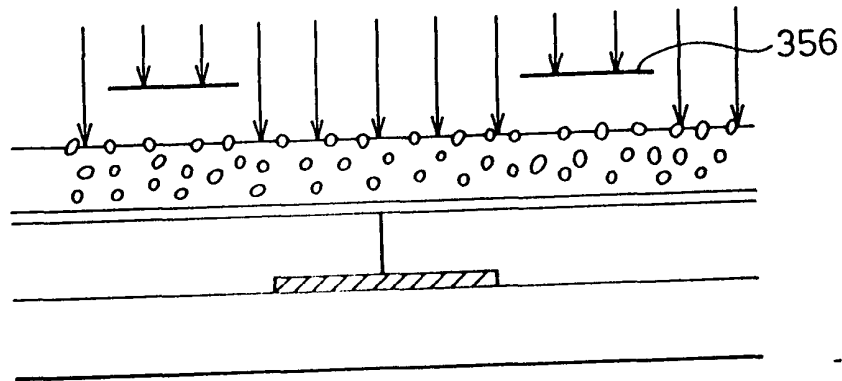
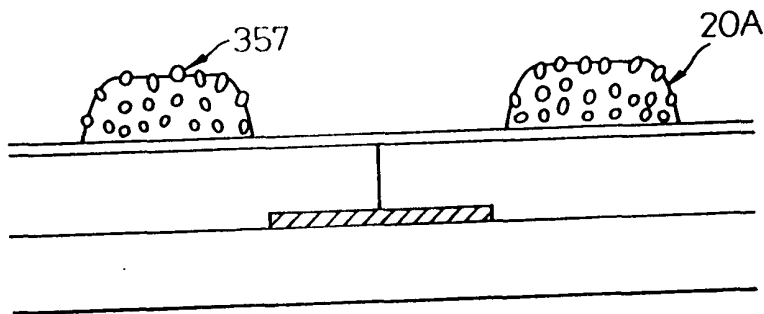


Fig.152C



148/246

Fig.153A

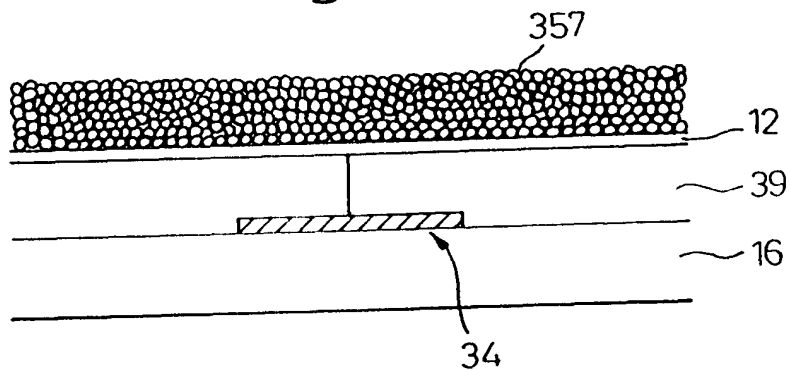


Fig.153B

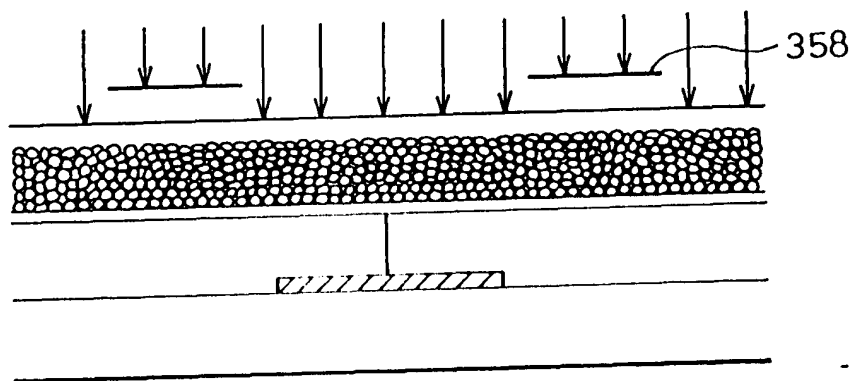
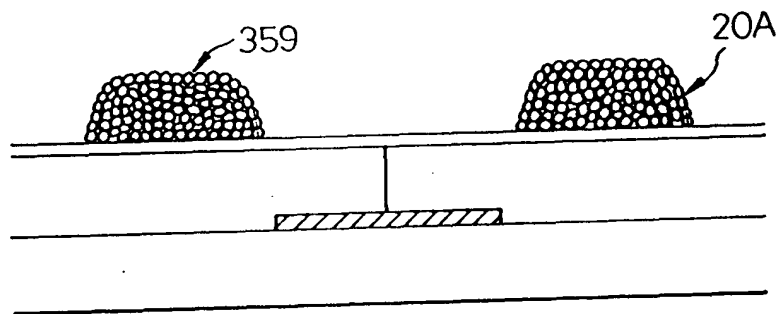


Fig.153C



149/  
246

Fig.154A

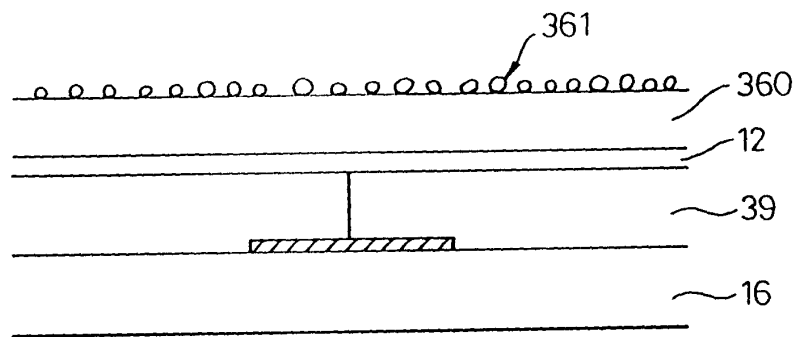
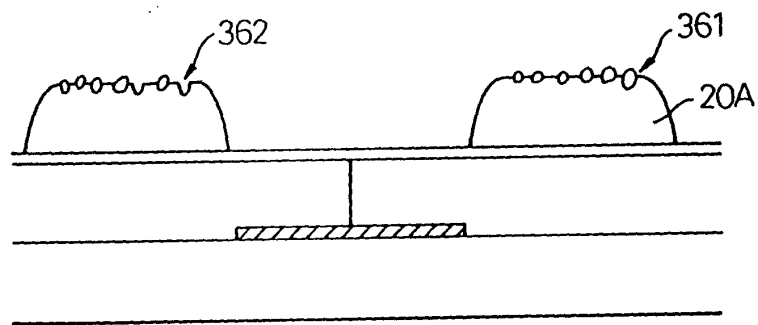


Fig.154B



150/  
246

Fig.155A

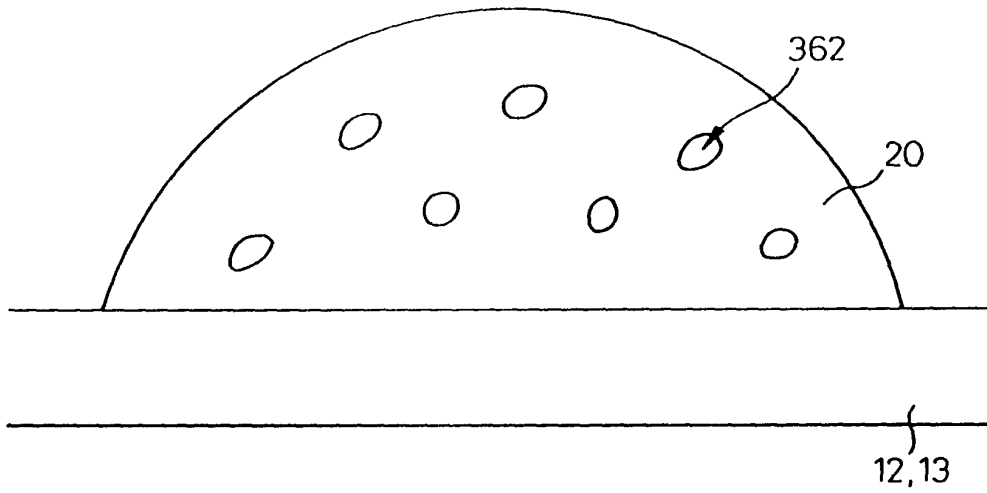


Fig.155B

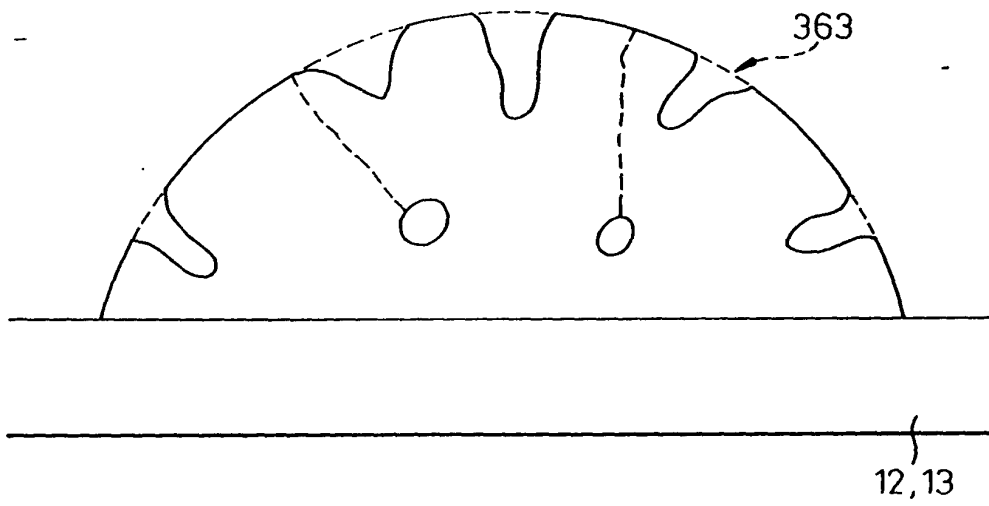
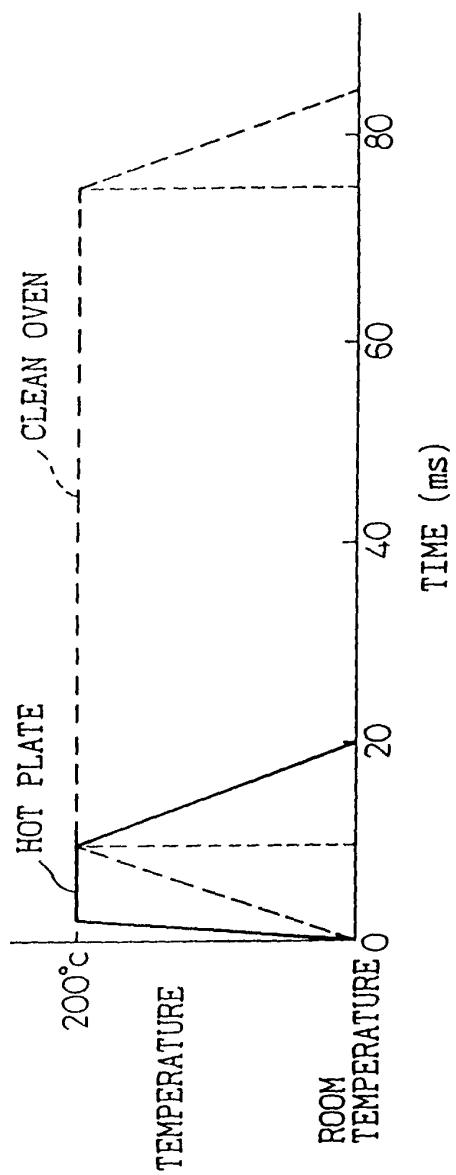


Fig.156



152/246

Fig.157A

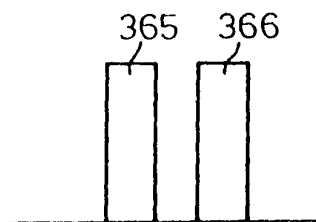


Fig.157B



Fig.157C

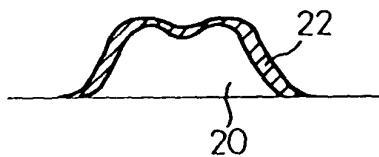
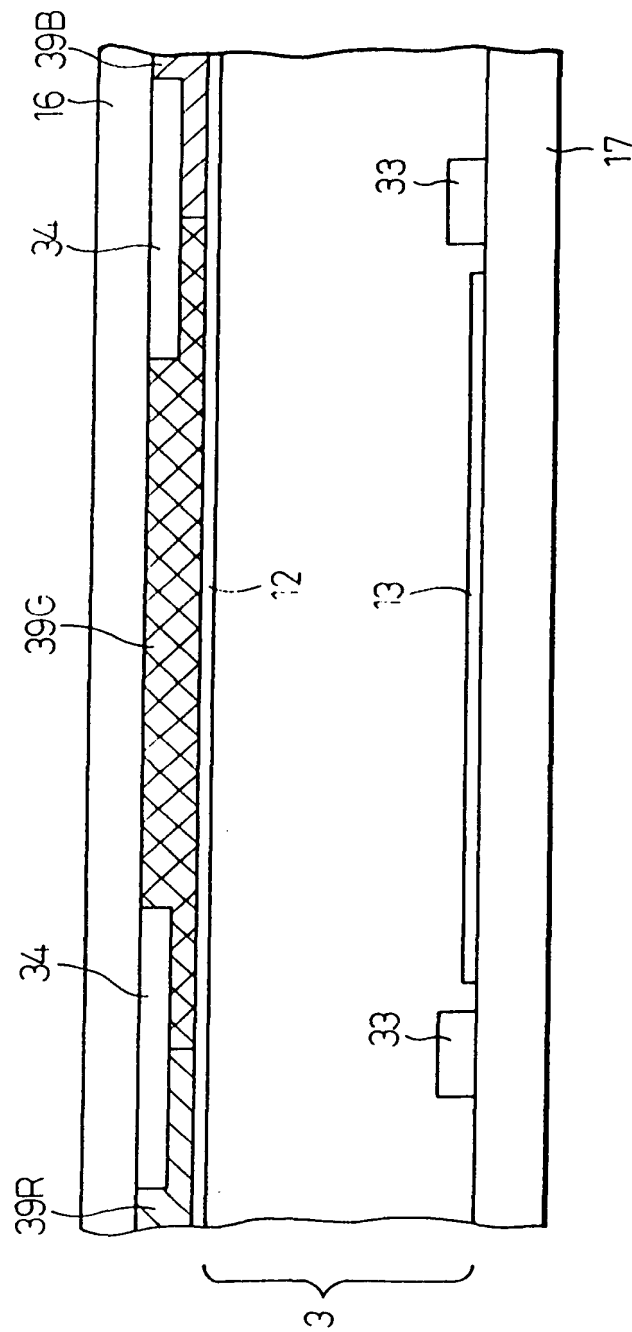


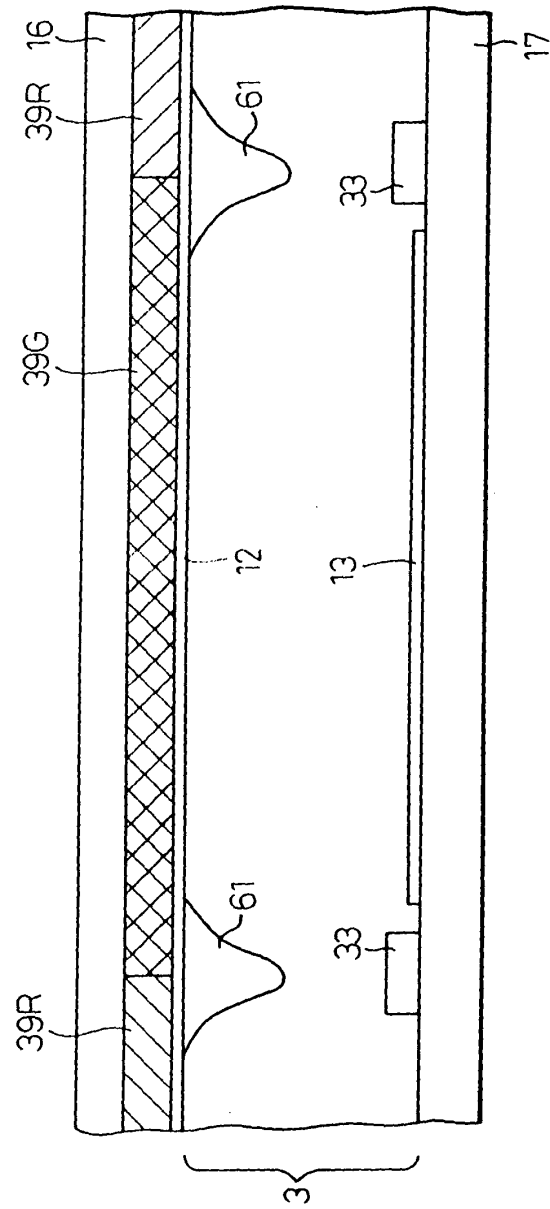


Fig.158



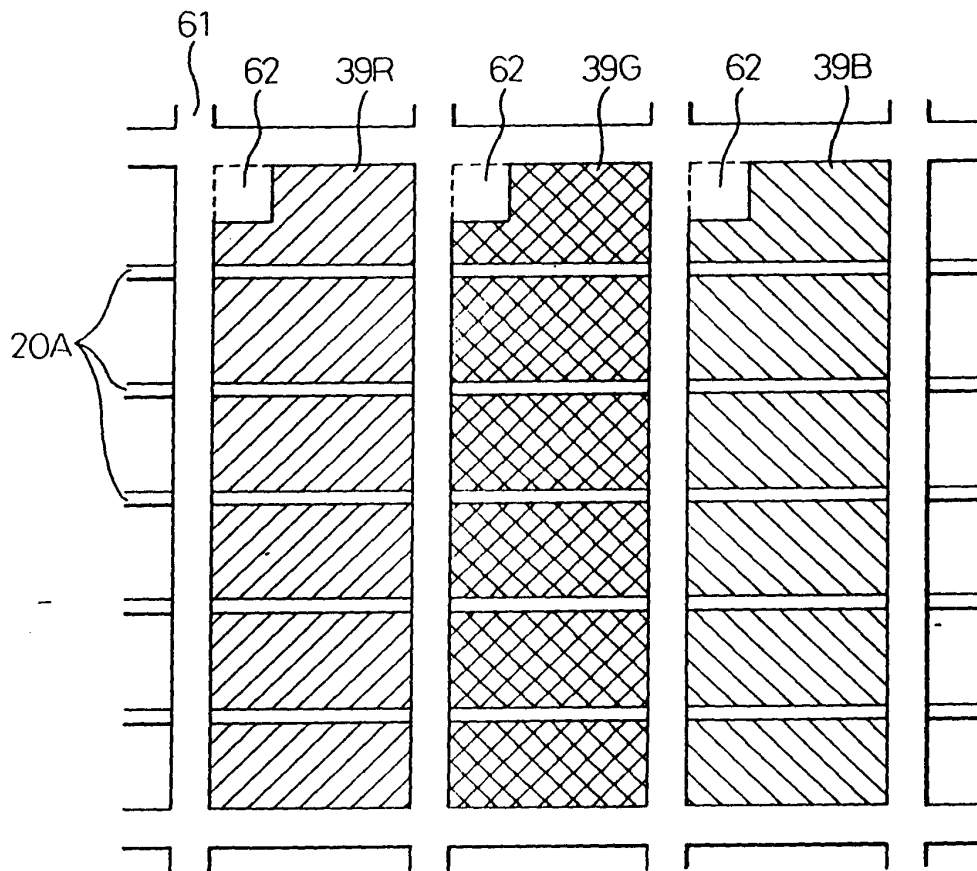
153/246

Fig. 159



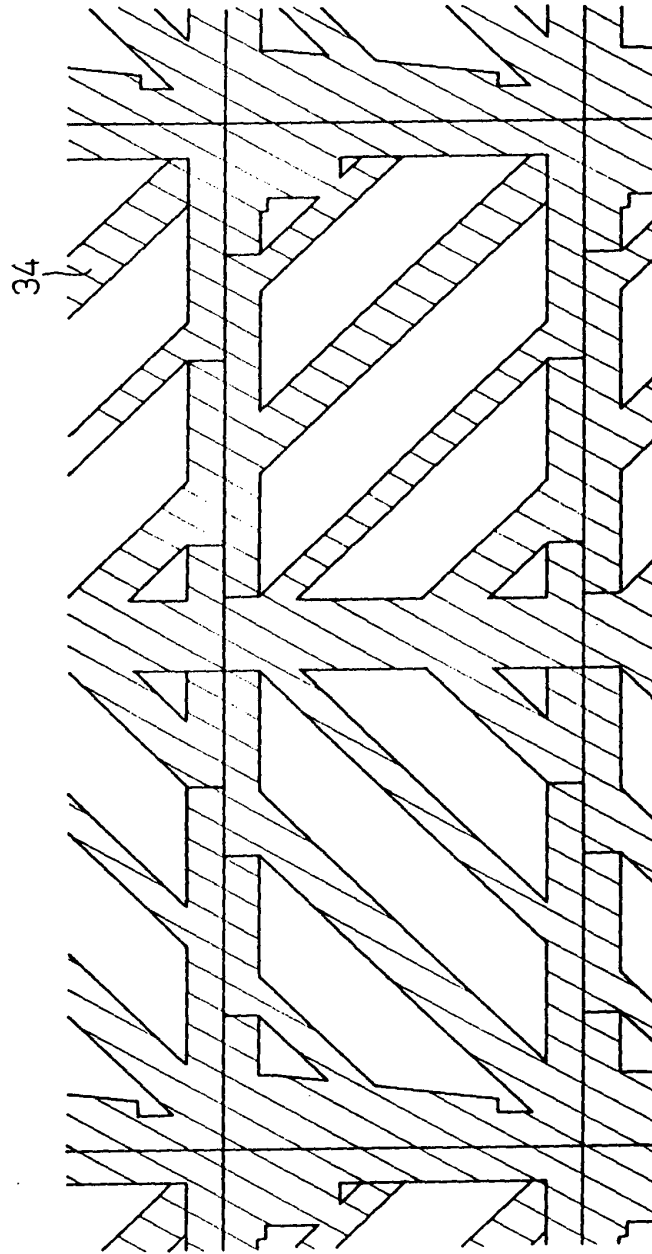
154/246

Fig.160



2025 RELEASE UNDER E.O. 14176

Fig.161



156/246

Fig.162

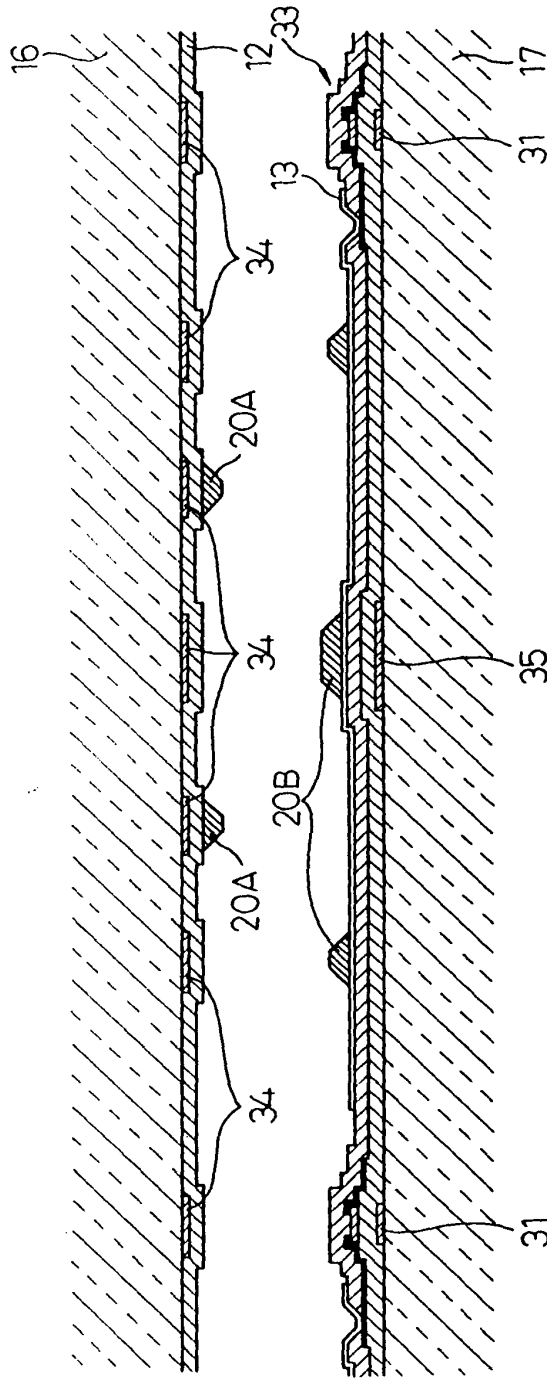


Fig.163

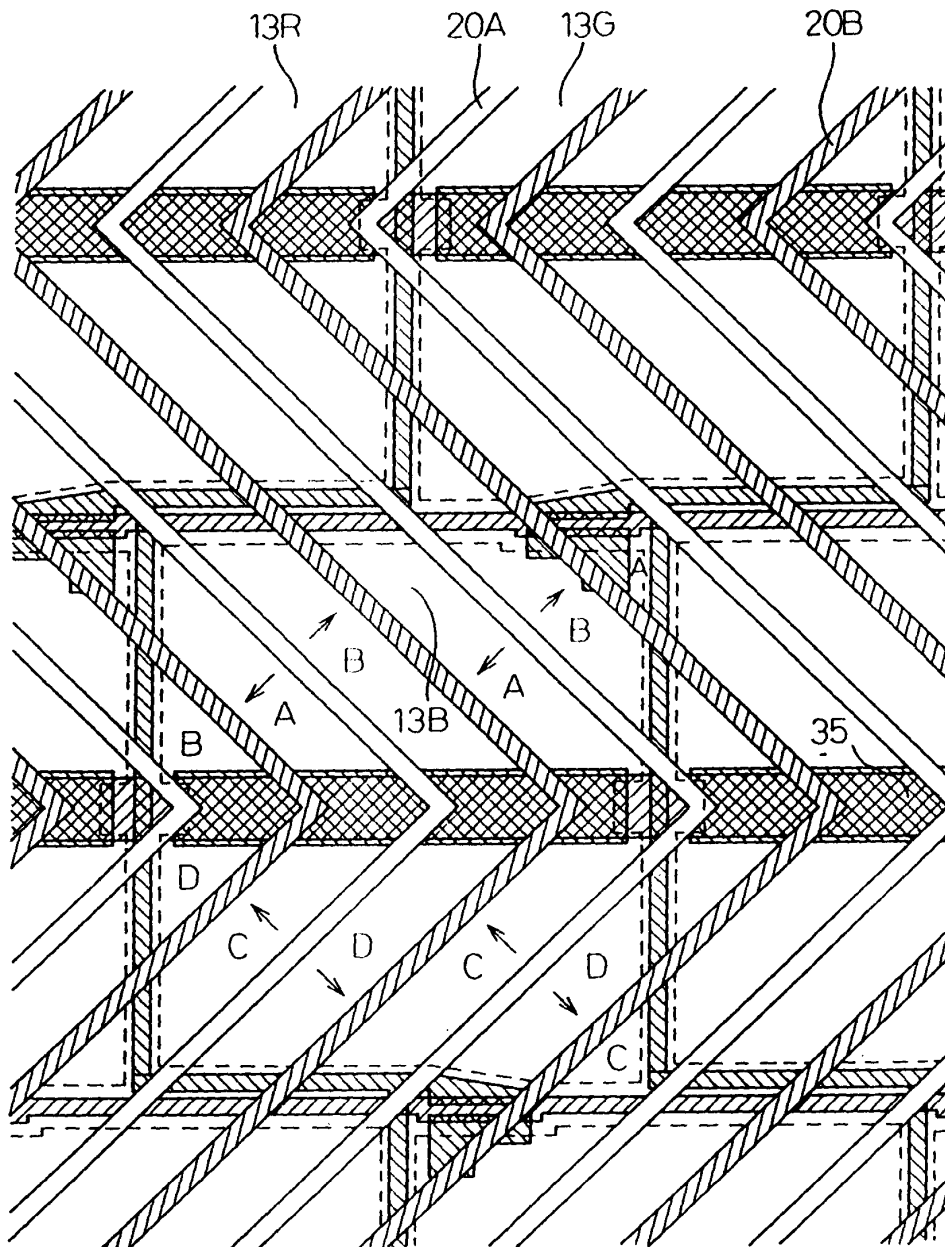


Fig. 164

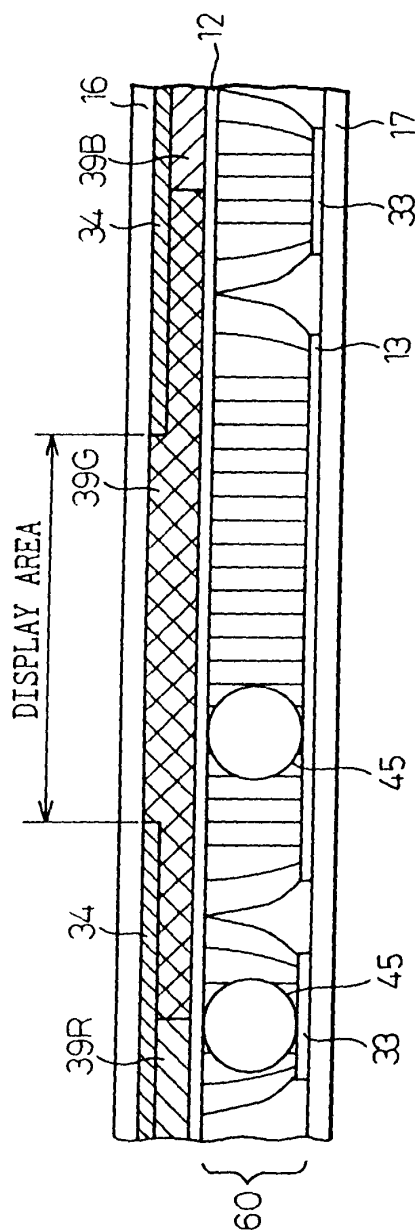


Fig.165A

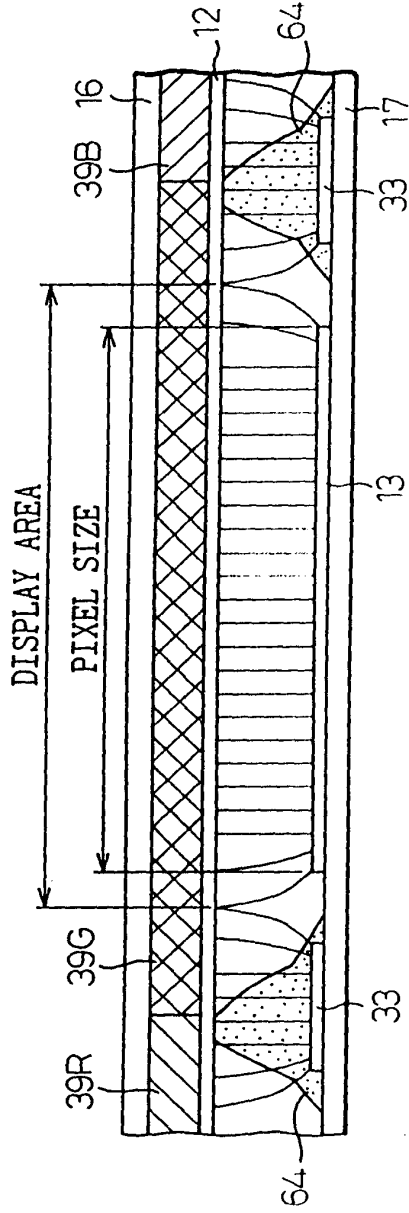


Fig.165B

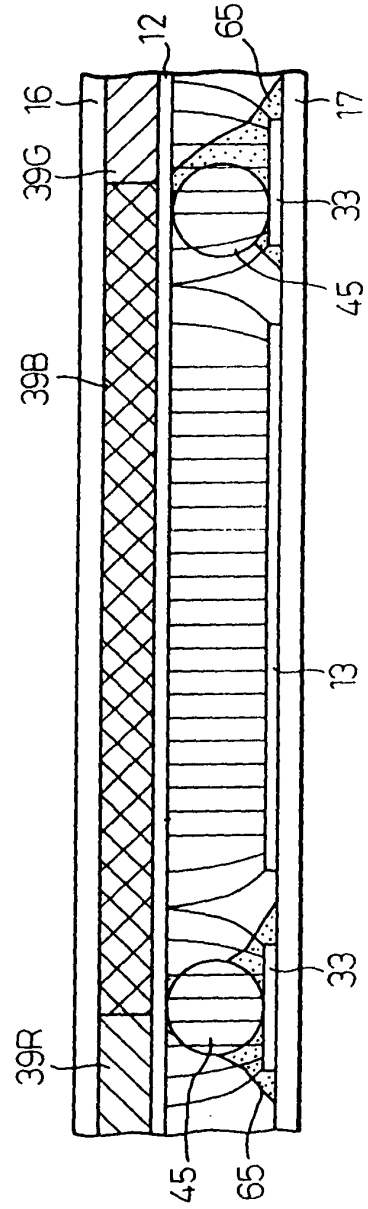
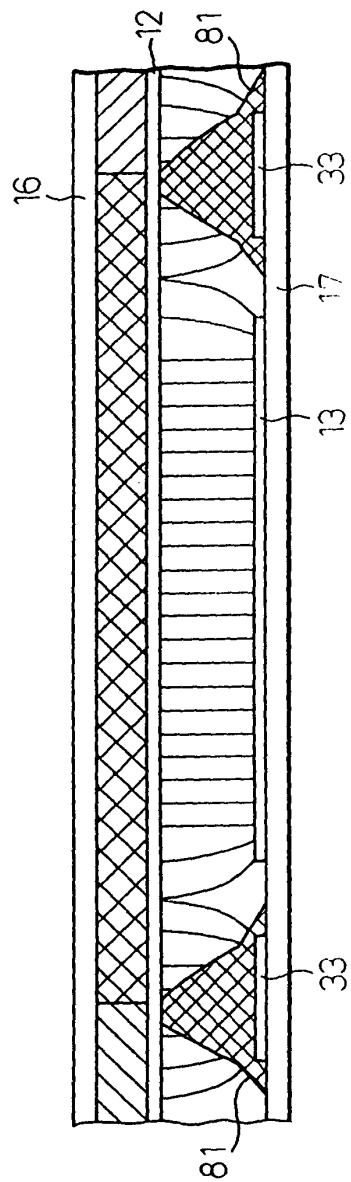




Fig.166A



161/246

Fig.166B

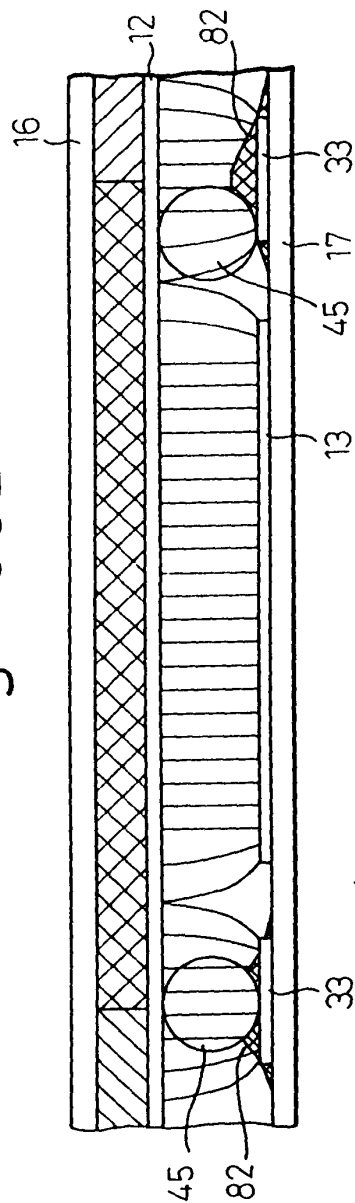
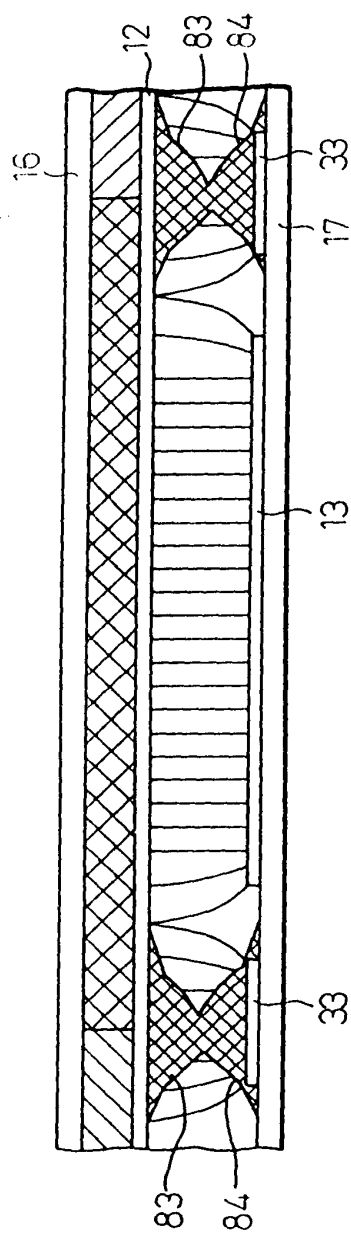


Fig. 167



163/246

Fig.168A

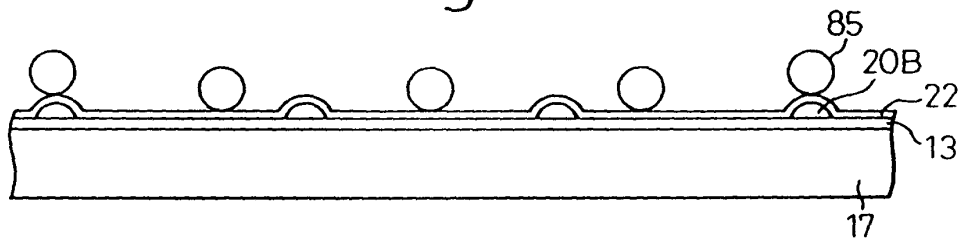


Fig.168B

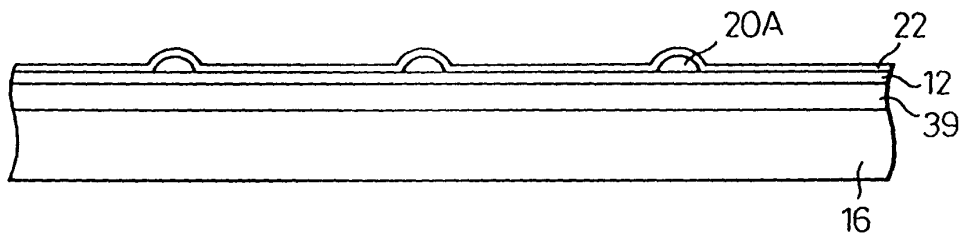
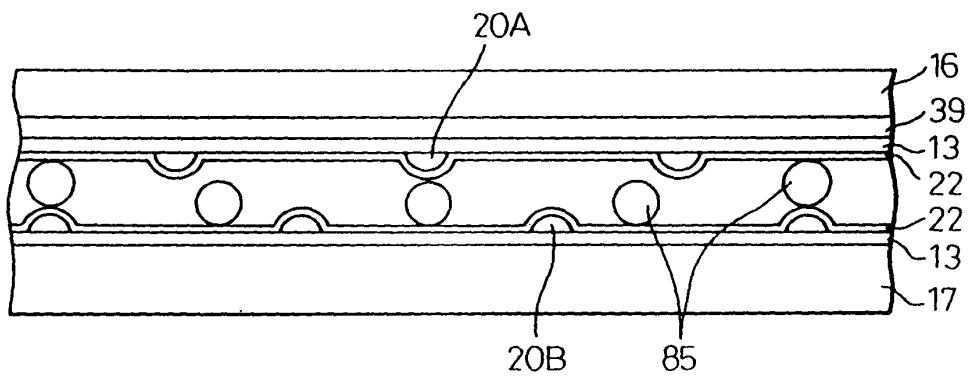


Fig.168C



[illegible]

Fig. 169

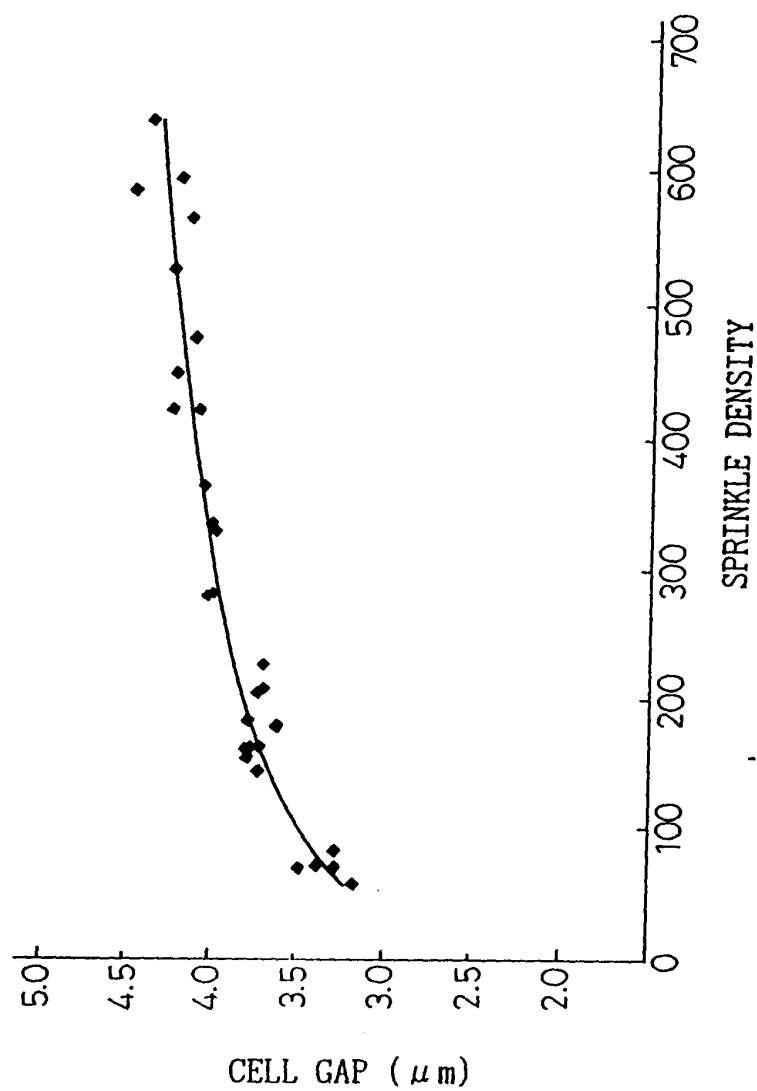
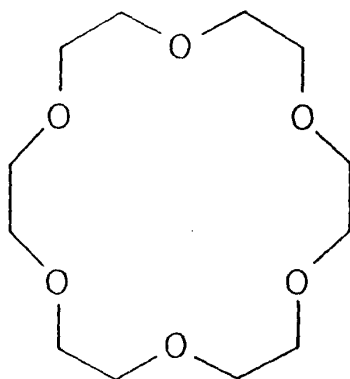

$$\begin{array}{r} 164 \\ \times 15 \\ \hline 820 \\ 1640 \\ \hline 2460 \end{array}$$

Fig.170

SPRINKLE DENSITY OF SPACERS (NUMBERS/mm <sup>2</sup> )	50	100	150	200	250	300	350	400	450	500	550
BLEMISH OCCURRENCE DUE TO PUSHING	YES	YES	NO	NO	NO	NO	NO	NO	NO	NO	NO
BLEMISH OCCURRENCE DUE TO PULLING	NO	NO	NO	NO	NO	NO	YES	YES	YES	YES	YES

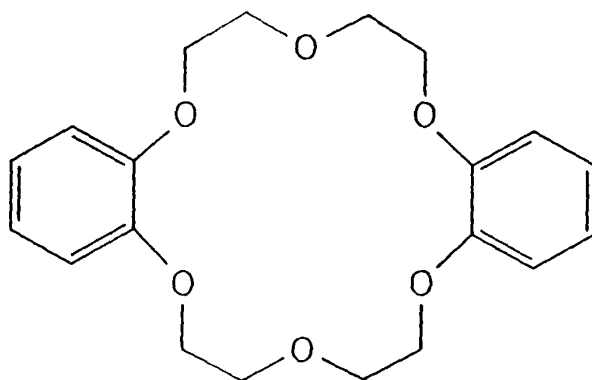
166/  
246

Fig.171A



18-CROWN-6

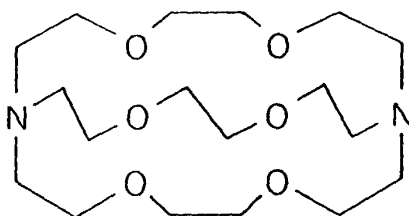
Fig.171B



DIBENZOYL-18-CROWN-6

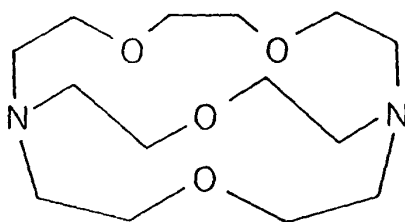
167/  
246

Fig.172A



CRYPTAND [2.2.2]

Fig.172B



CRYPTAND [2.1.1]

168/  
246

Fig.173A

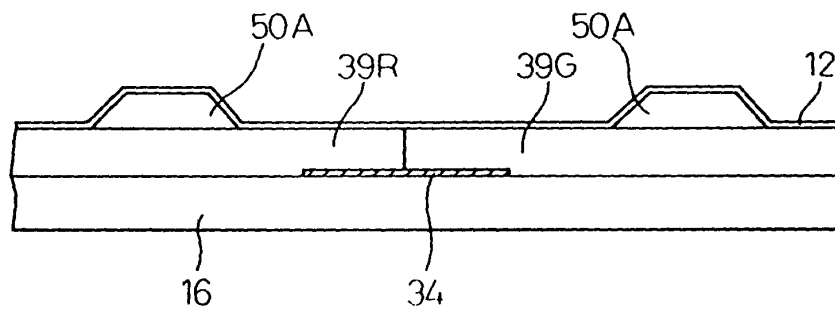
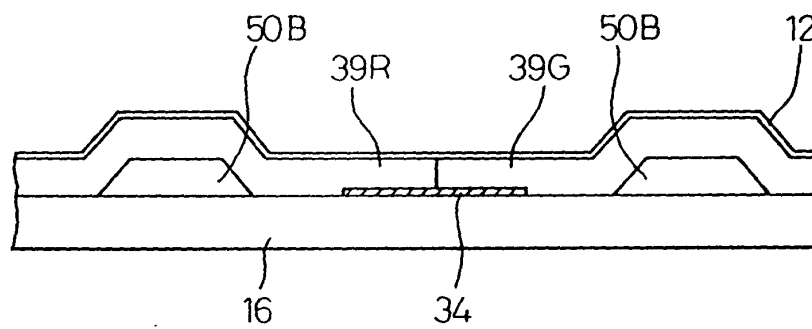


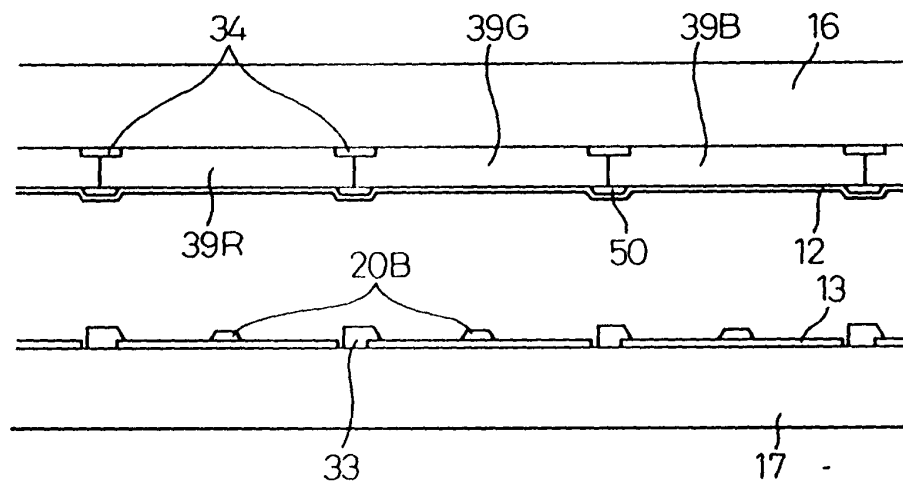
Fig.173B





169/  
246

Fig.174



170/246

Fig.175A

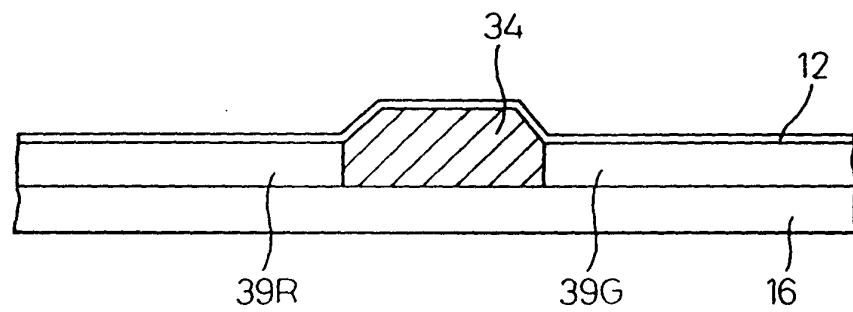
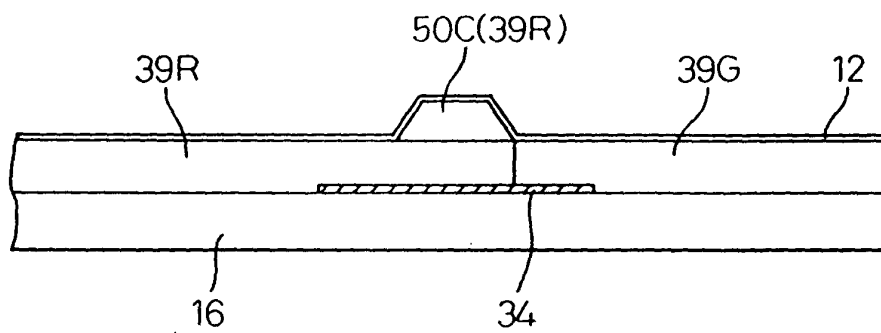


Fig.175B



171/246

Fig.176A

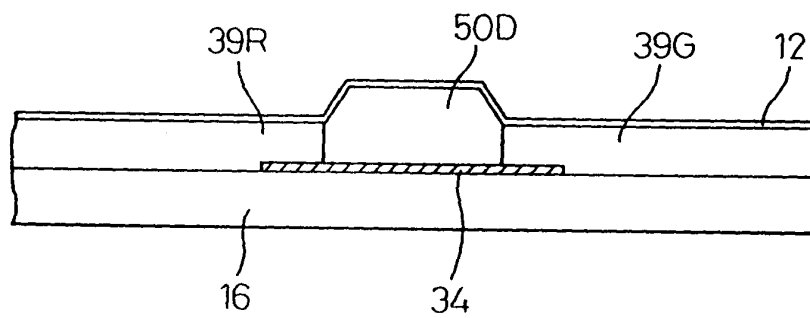
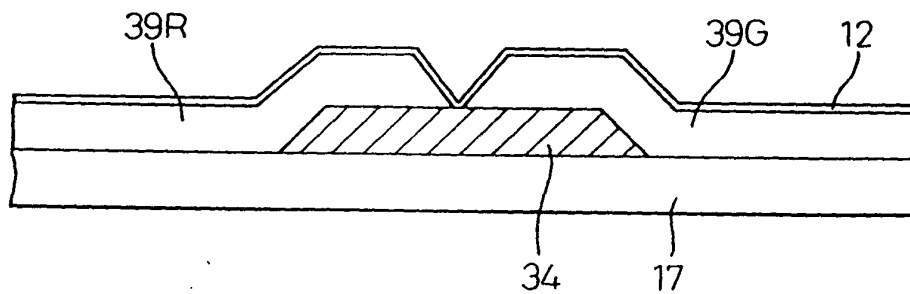


Fig.176B



172/  
246

Fig.177A

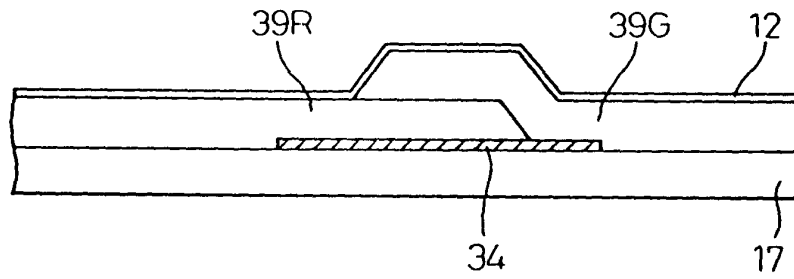


Fig.177B

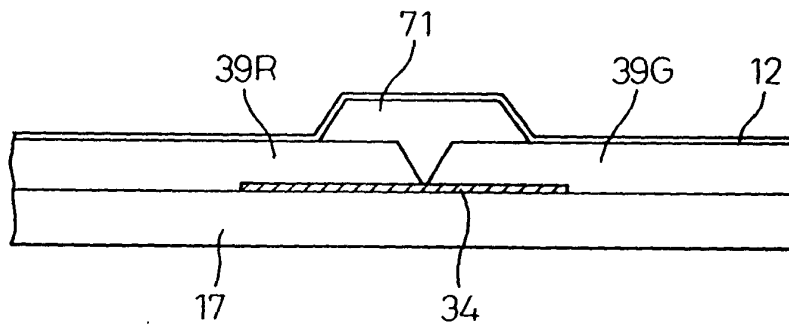
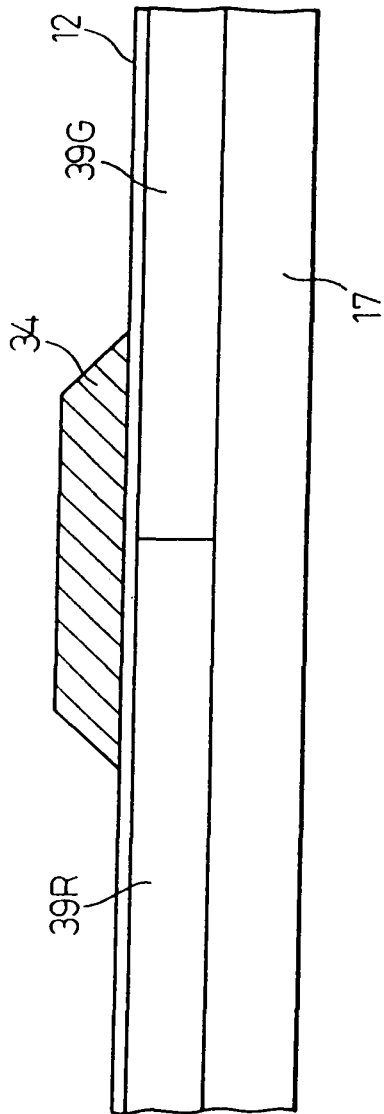


Fig.178



174/246

Fig.179A

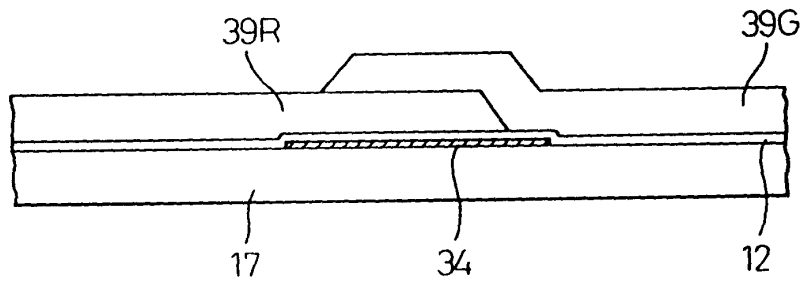


Fig.179B

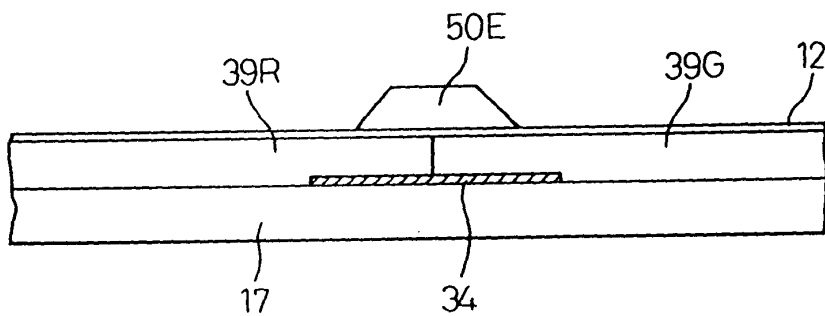


Fig.180A

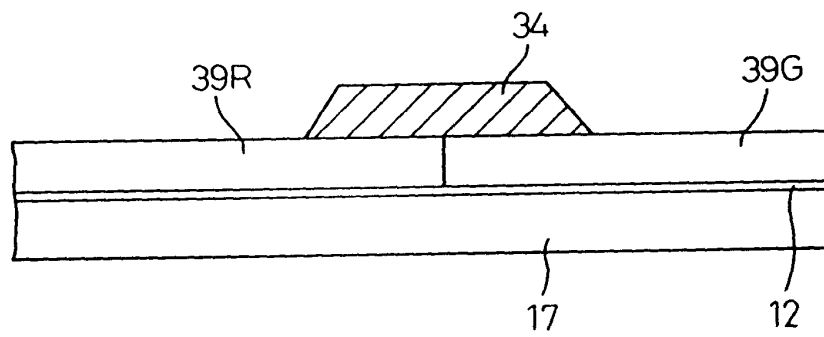


Fig.180B

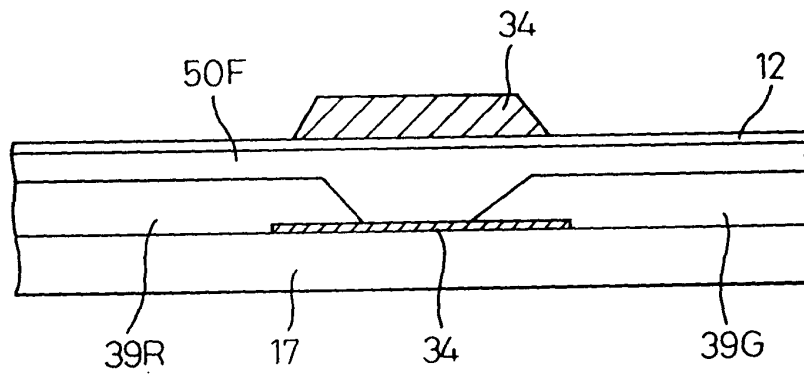


Fig.181A

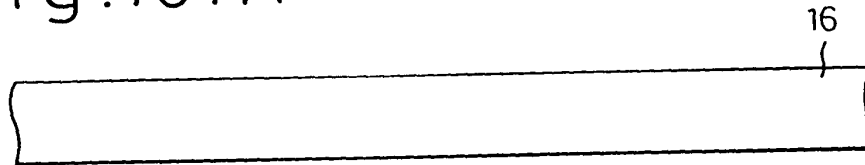


Fig.181B

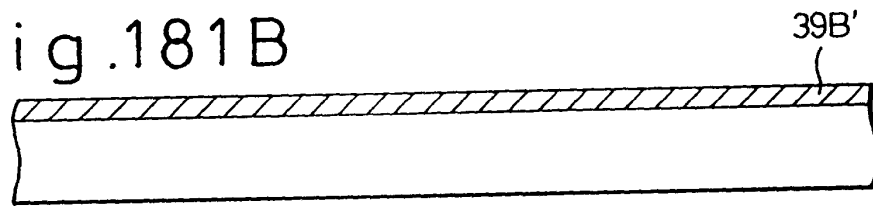


Fig.181C

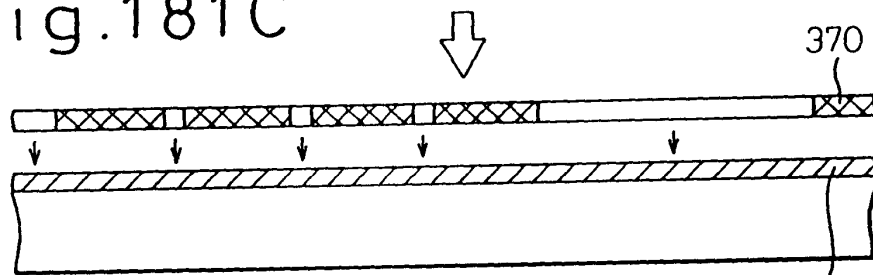
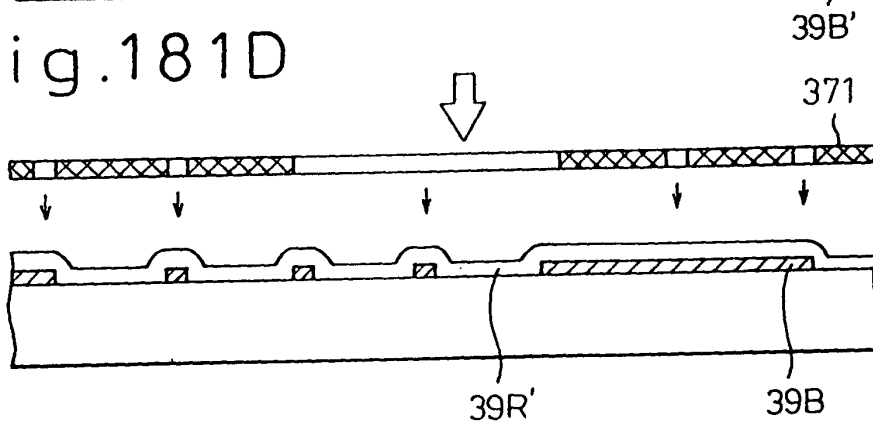


Fig.181D





177/246

Fig.181E

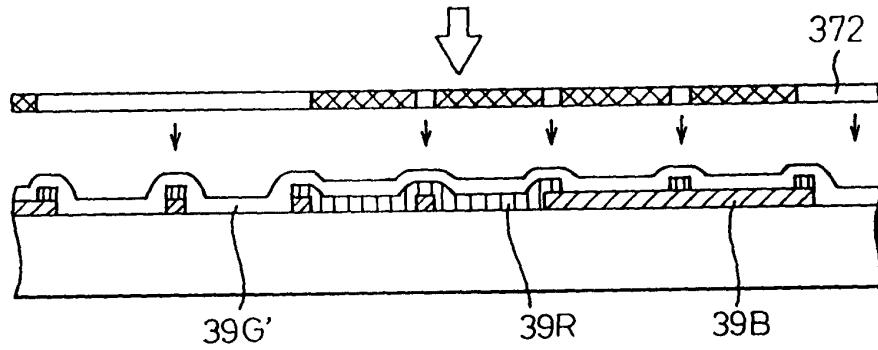


Fig.181F

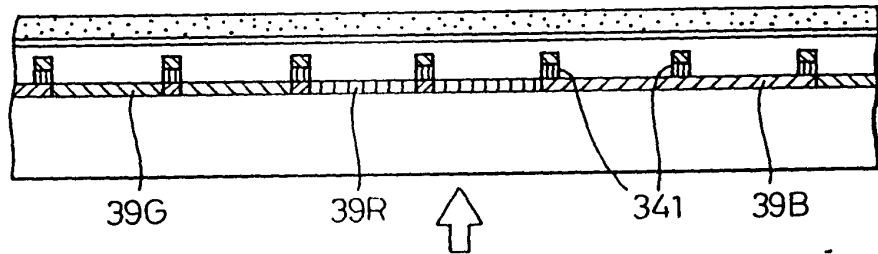
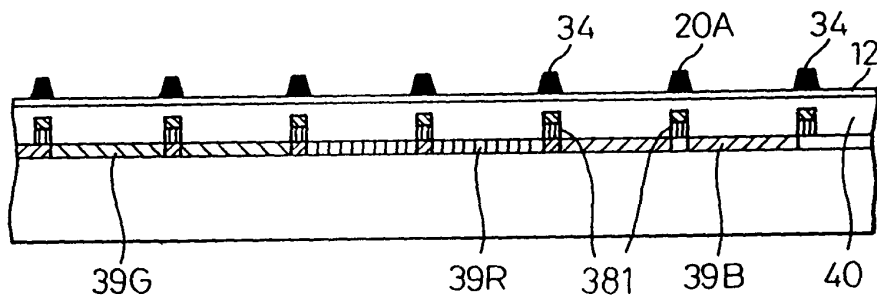


Fig.181G



$$\frac{178}{246}$$

Fig .182

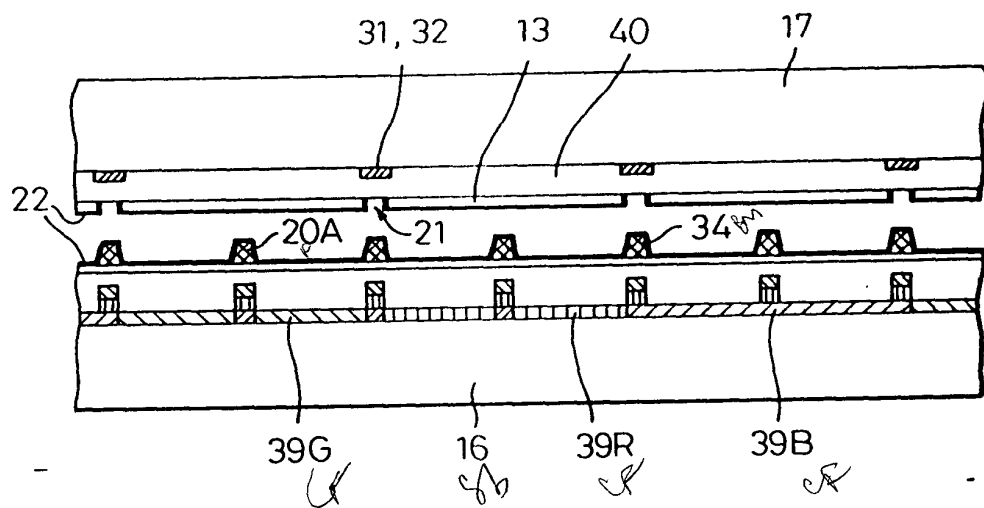


Fig.183A

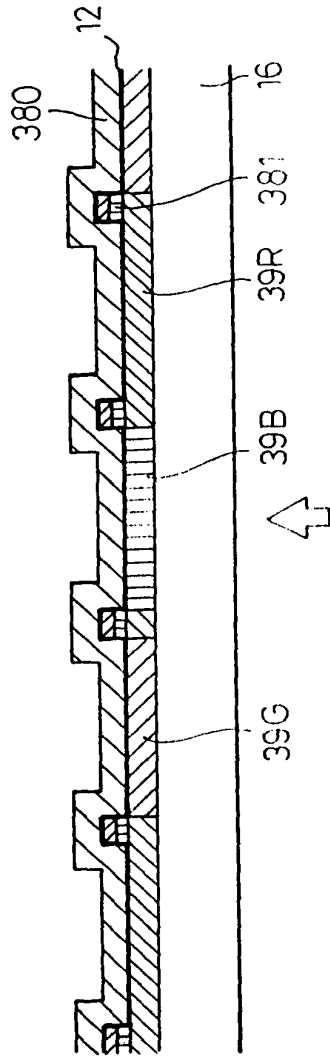


Fig.183B

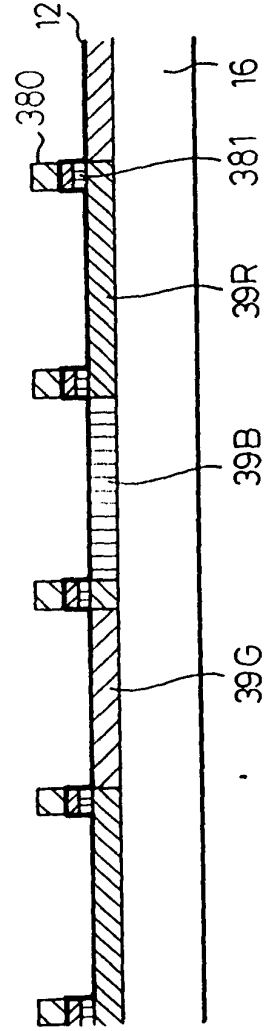


Fig.184A

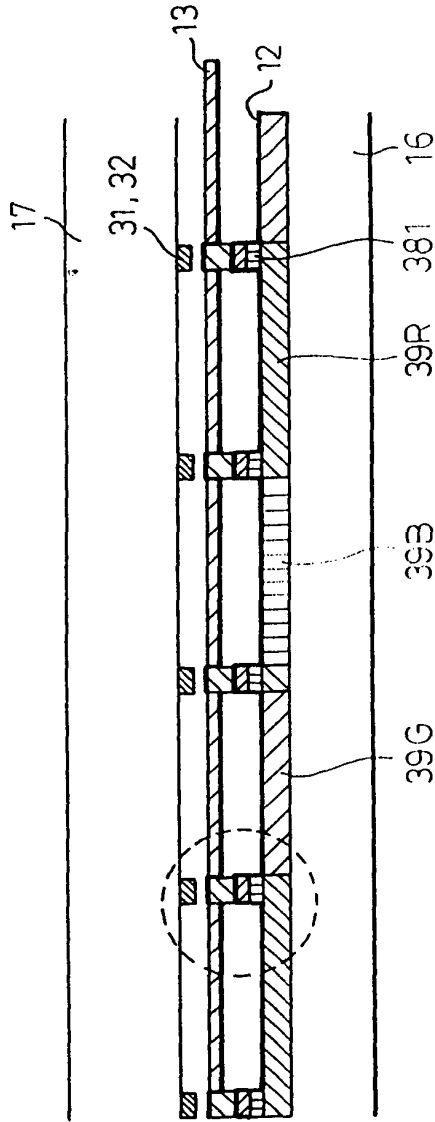
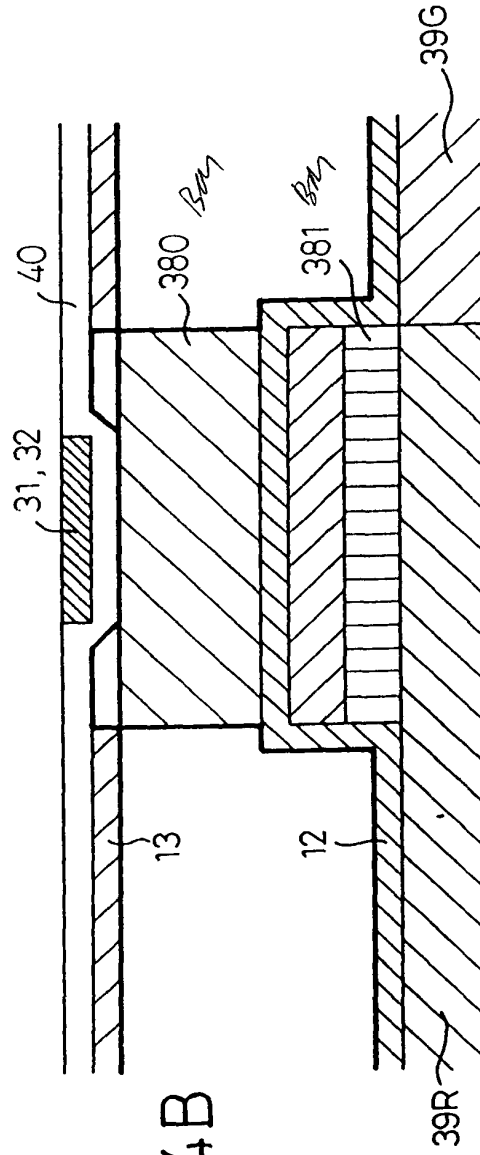


Fig.184B



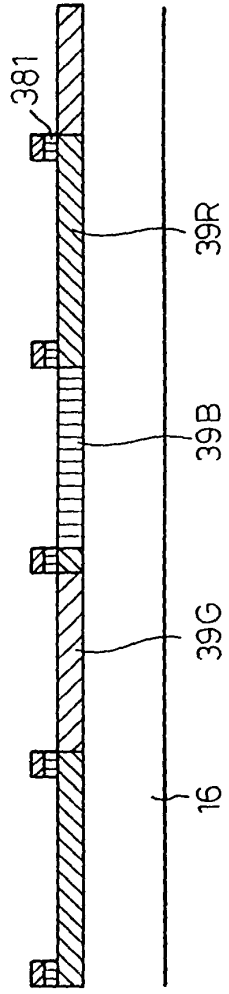


Fig.185A

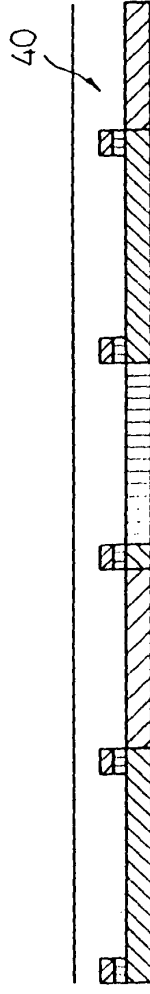


Fig.185B

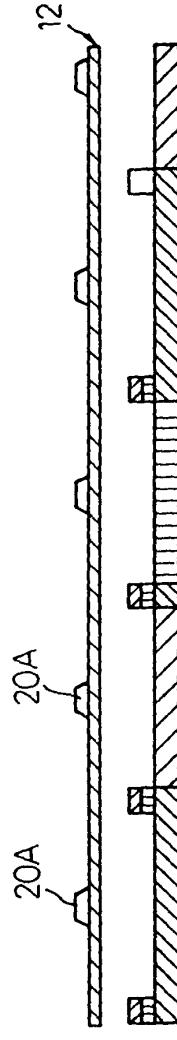
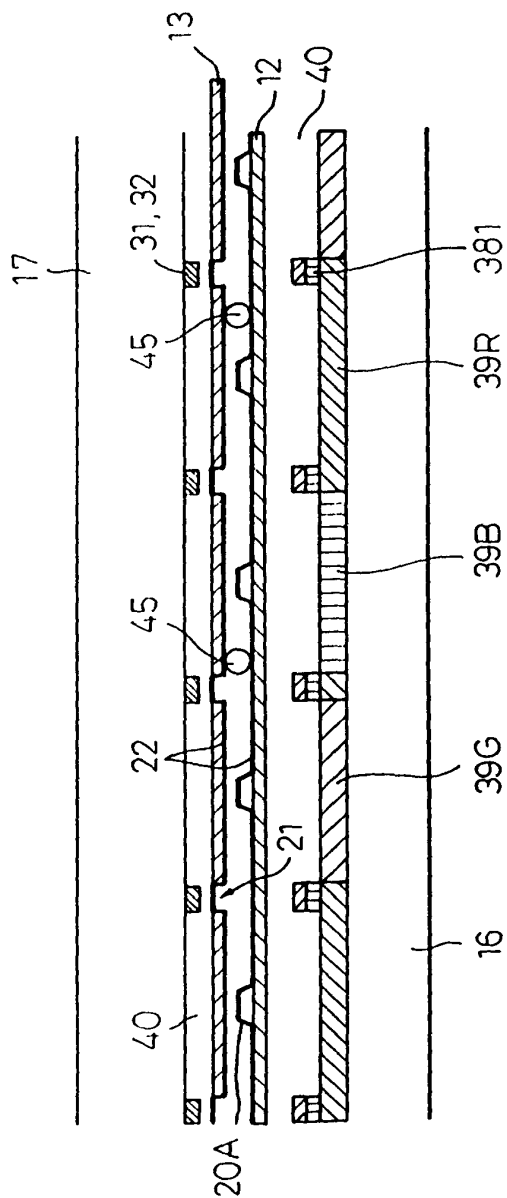


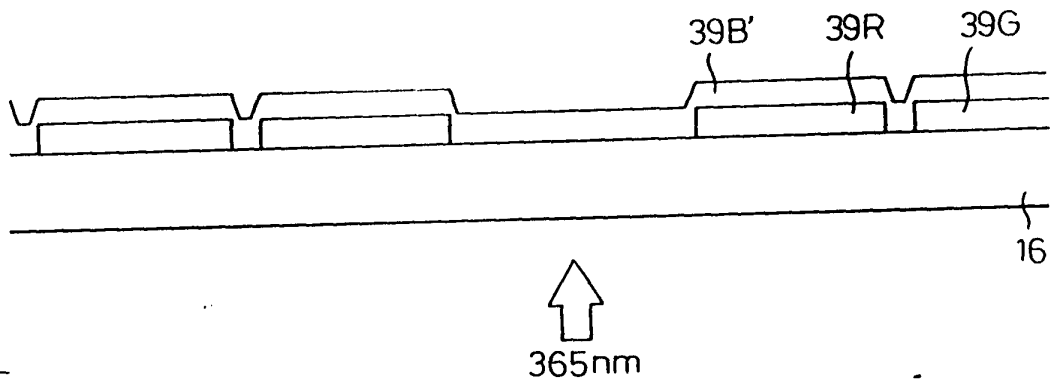
Fig.185C

Fig. 186



183/246

Fig.187



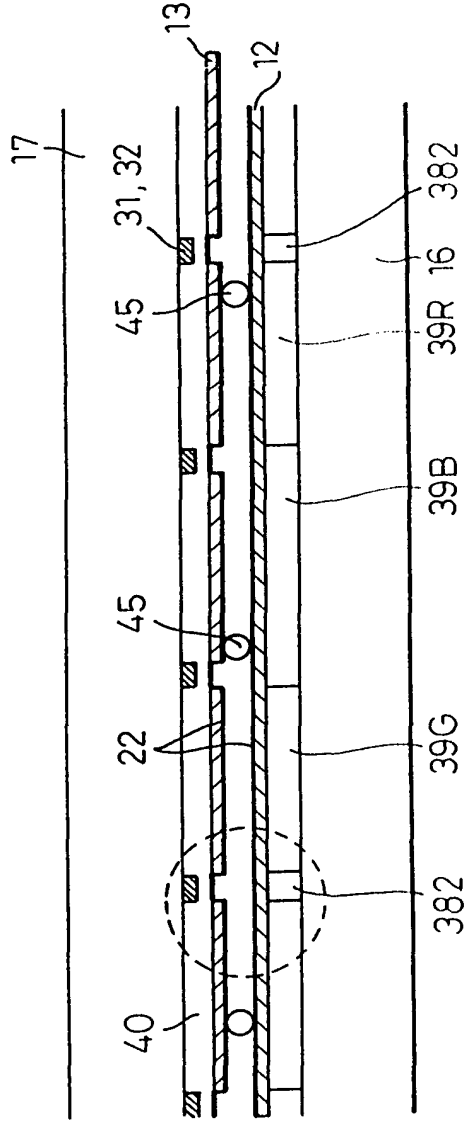


Fig. 188A

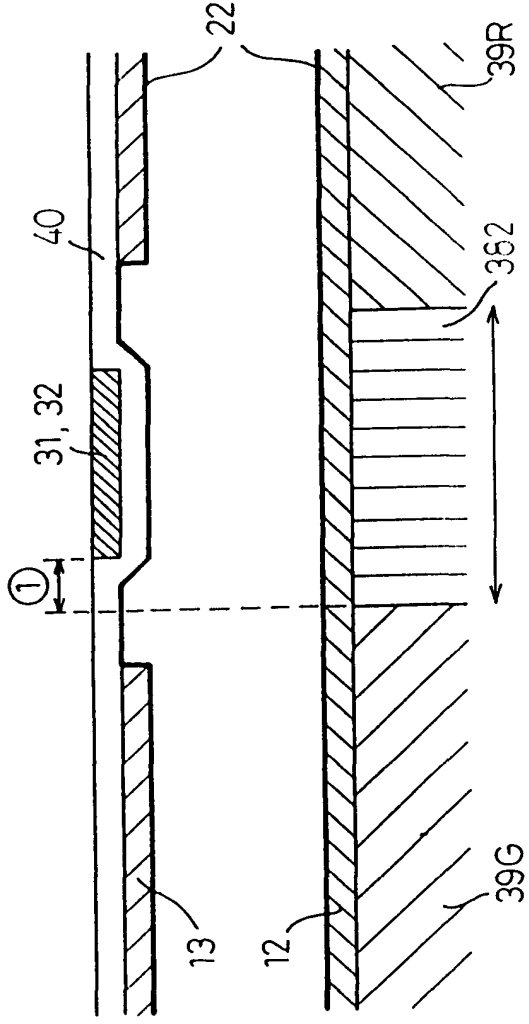


Fig. 188B



185/  
246

Fig.189

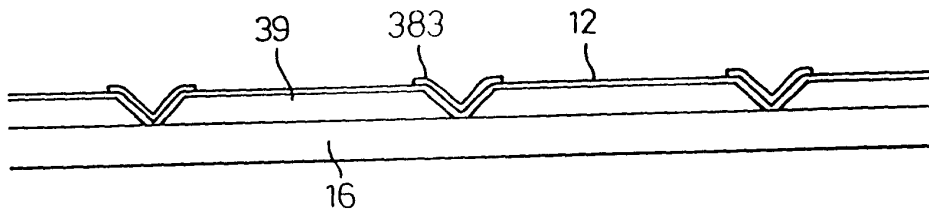


Fig.190A

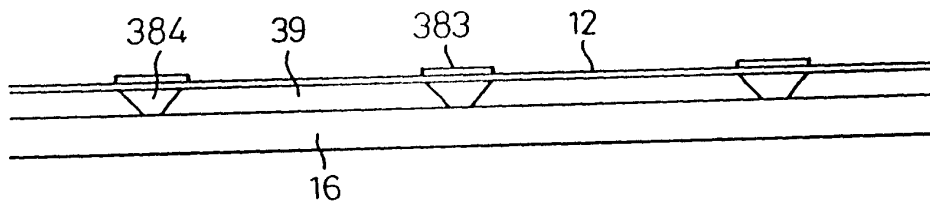
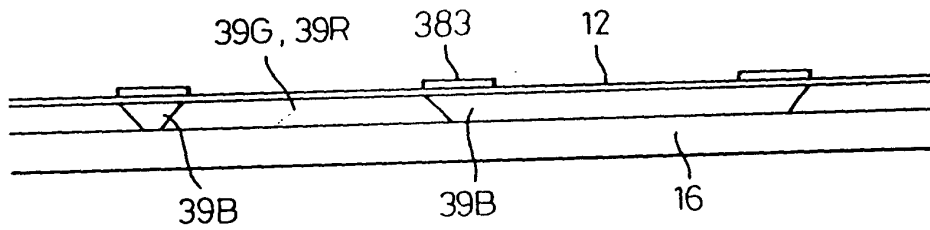


Fig.190B



186/246

Fig.191

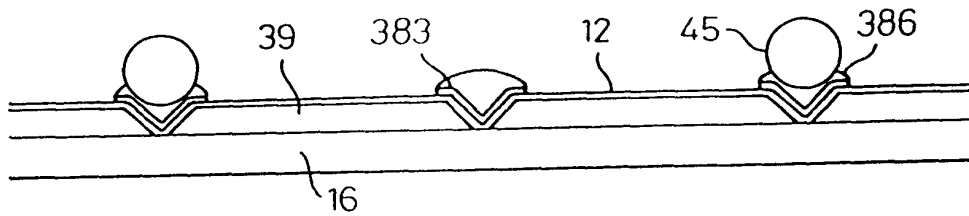


Fig.192

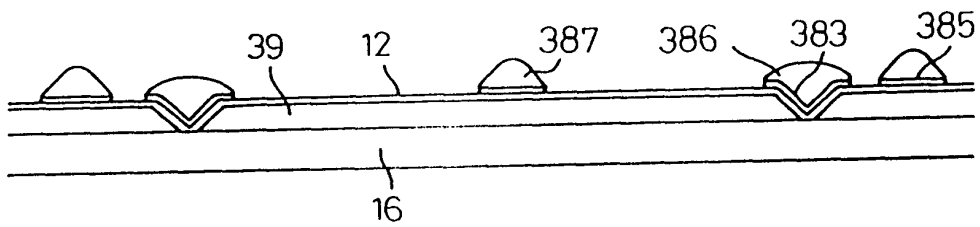
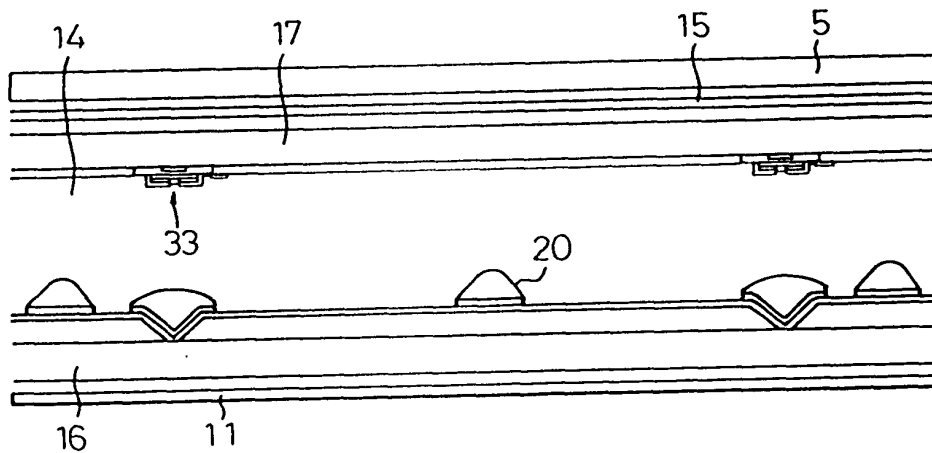


Fig.193



187/246

Fig.194

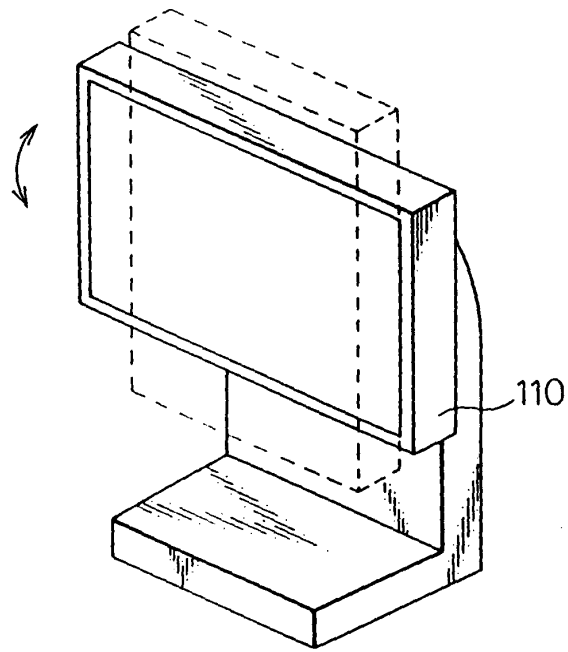
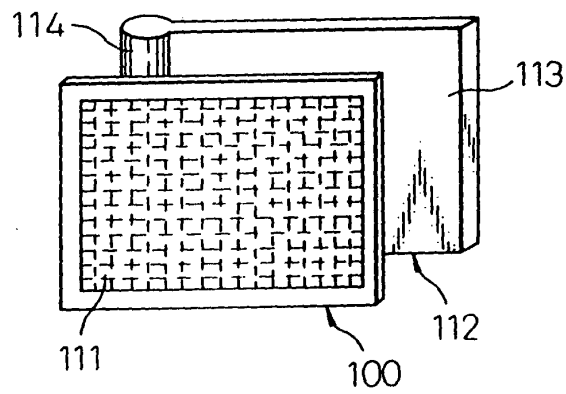


Fig.195



188/  
246

Fig.196A

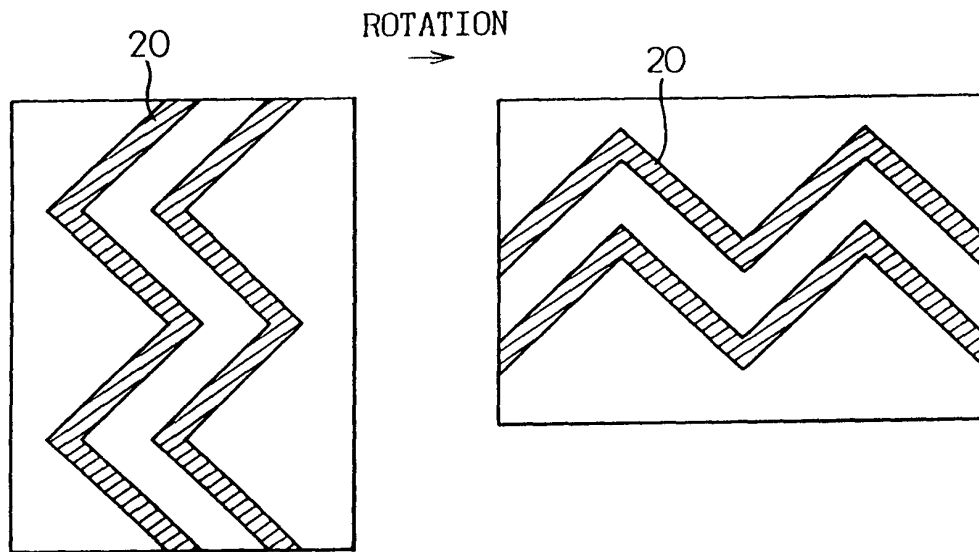


Fig.196B

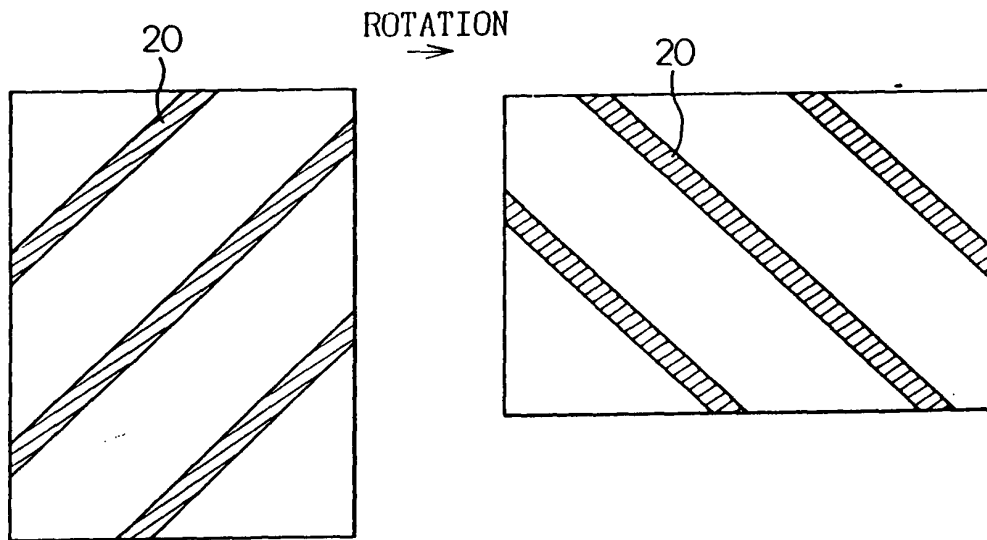


Fig.197

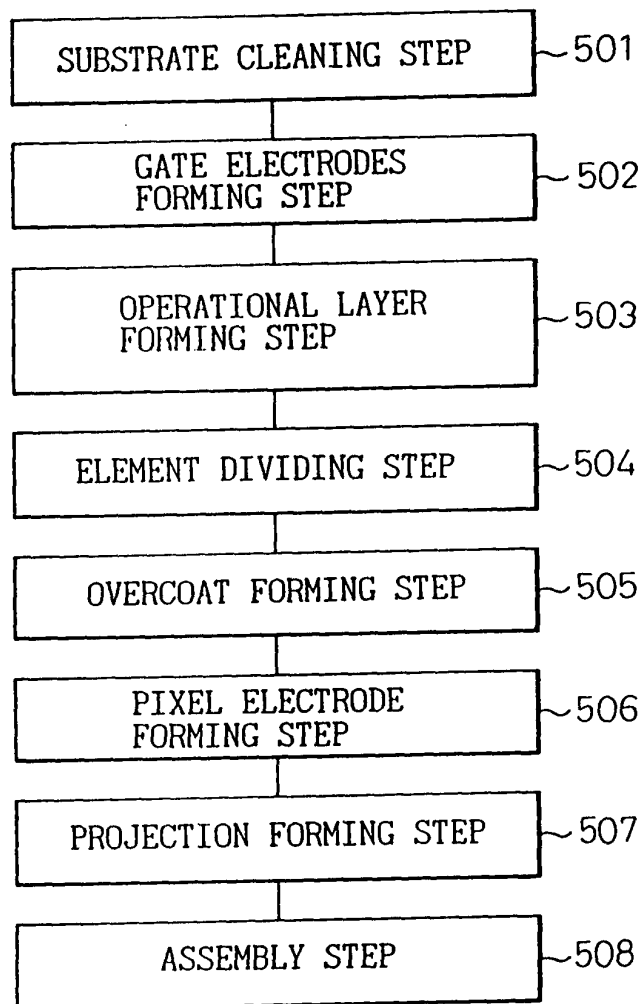


Fig.198

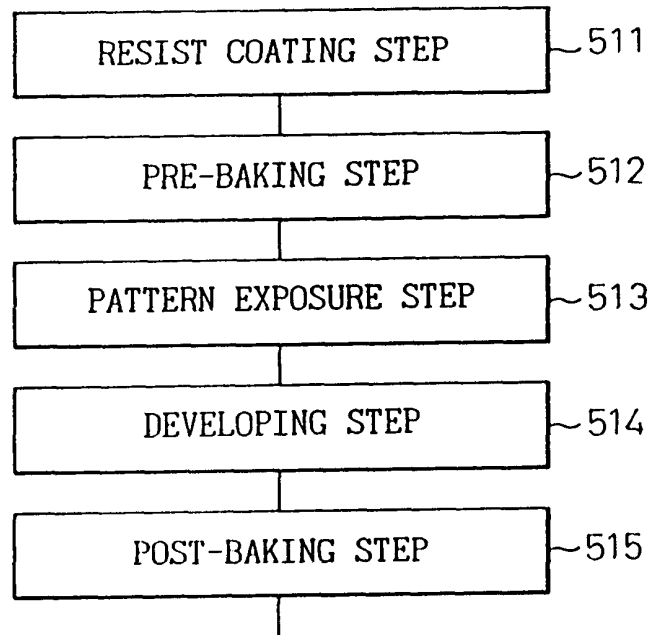


Fig.199

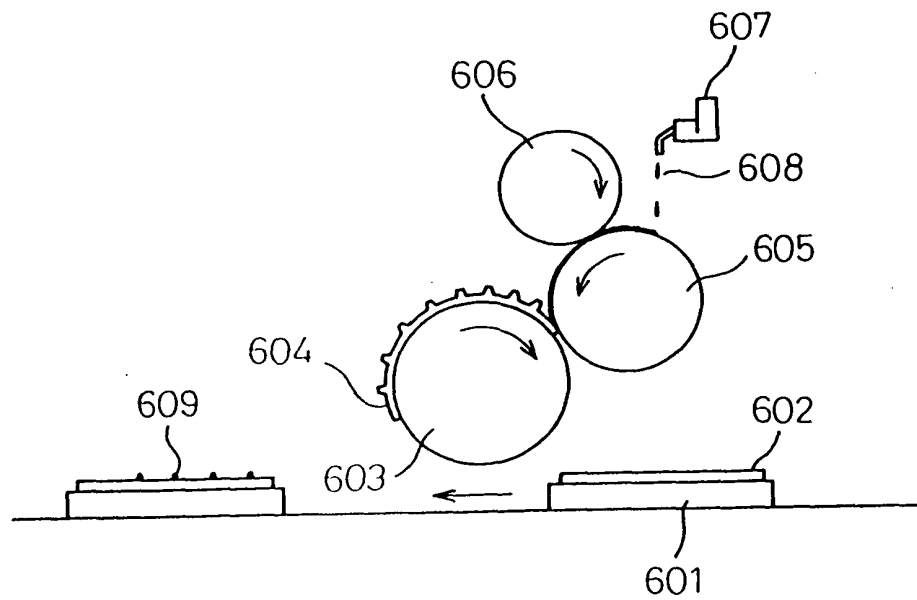


Fig. 200

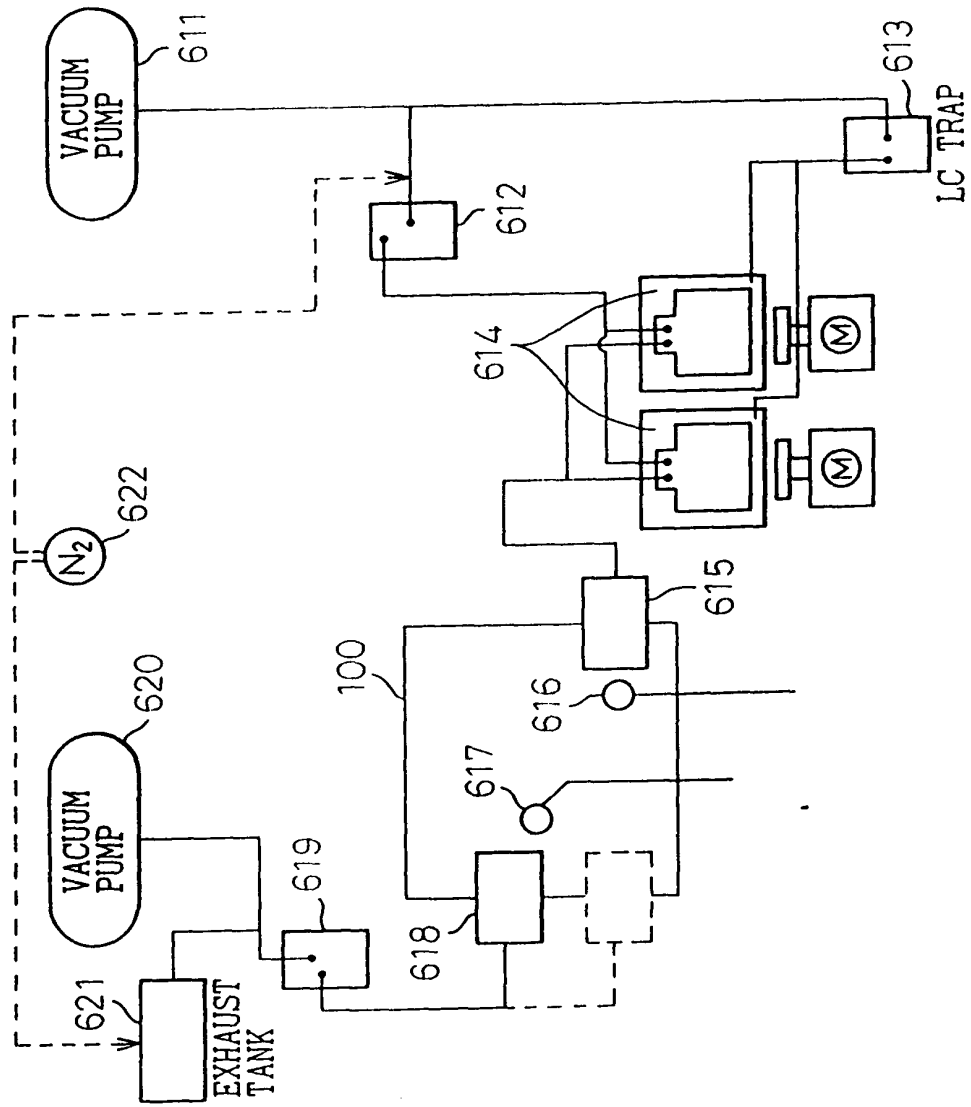


Fig. 201A

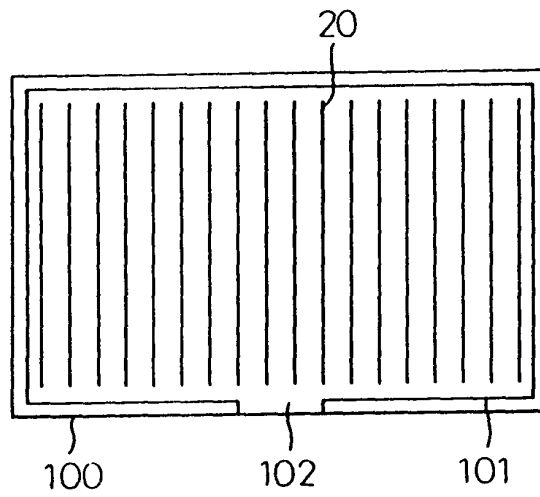


Fig. 201B

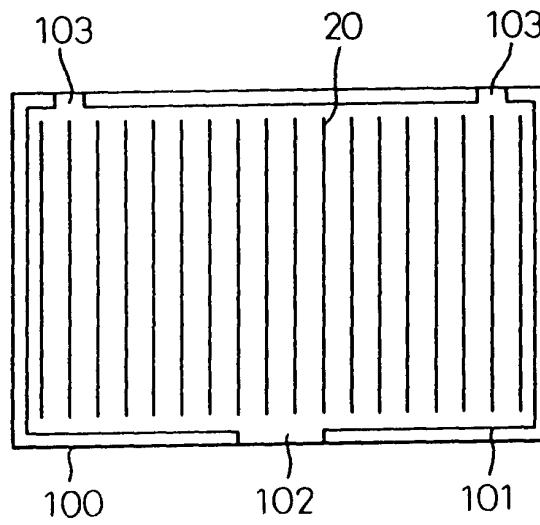




Fig. 202A

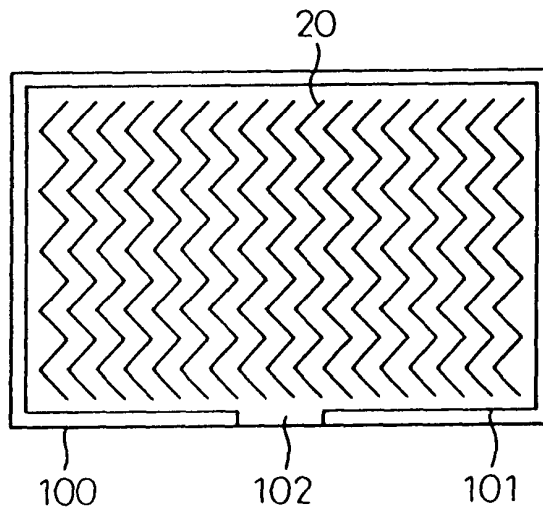


Fig. 202B

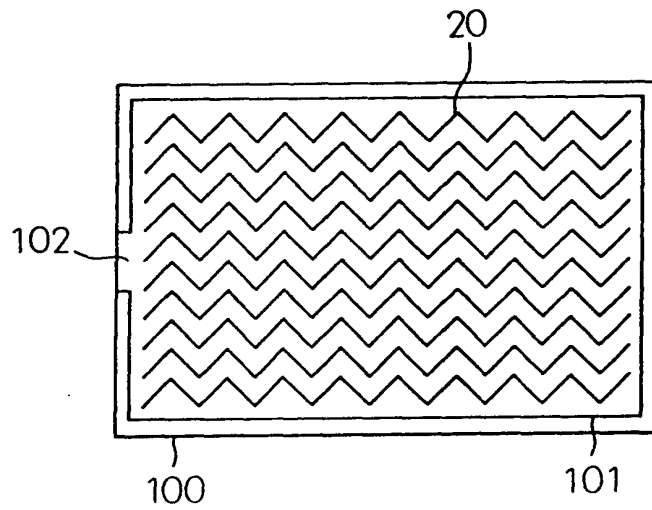


Fig. 203A

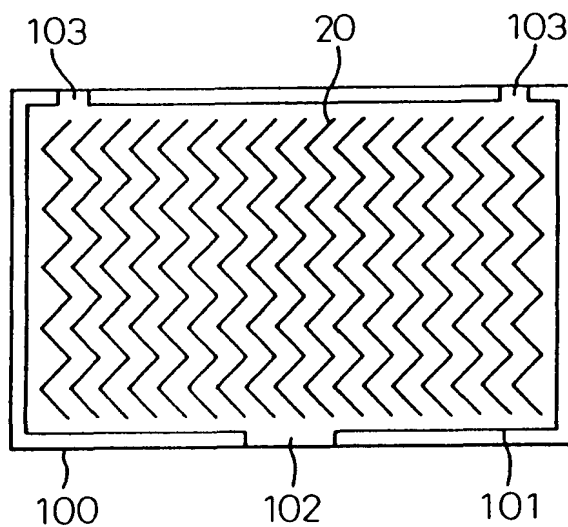
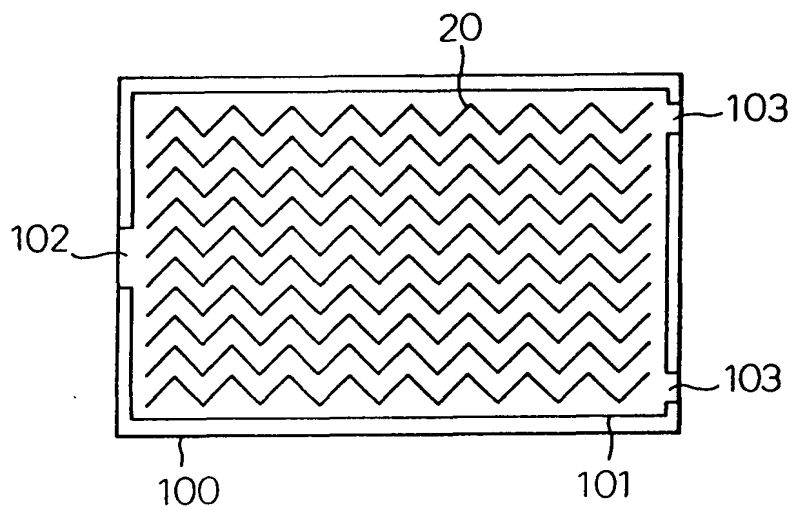


Fig. 203B



195/  
246

Fig. 204

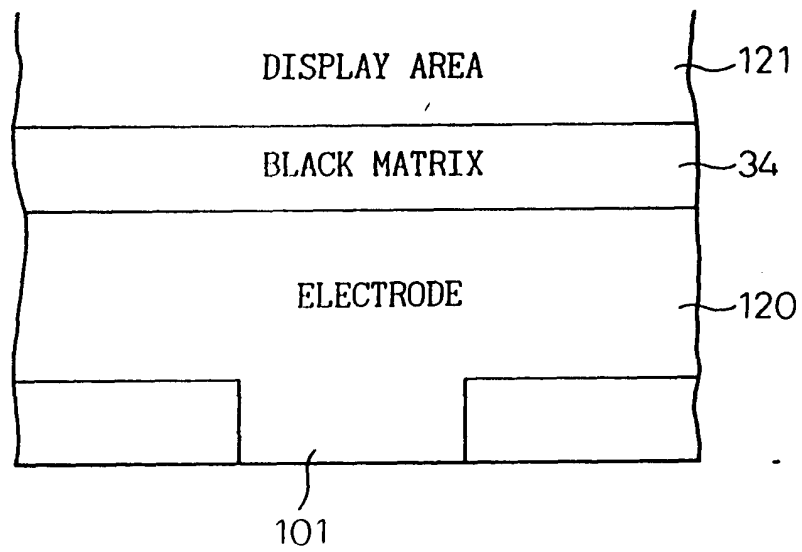


Fig. 205A

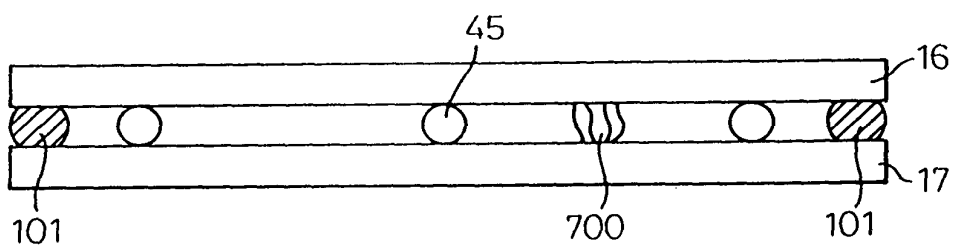


Fig. 205B

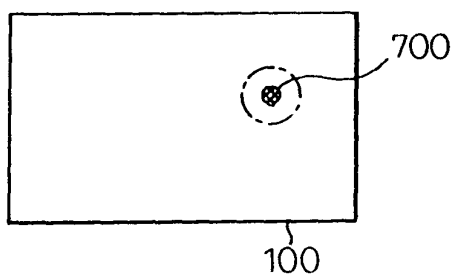
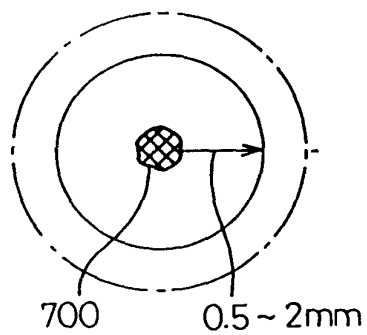


Fig. 205C



197/246

Fig. 206

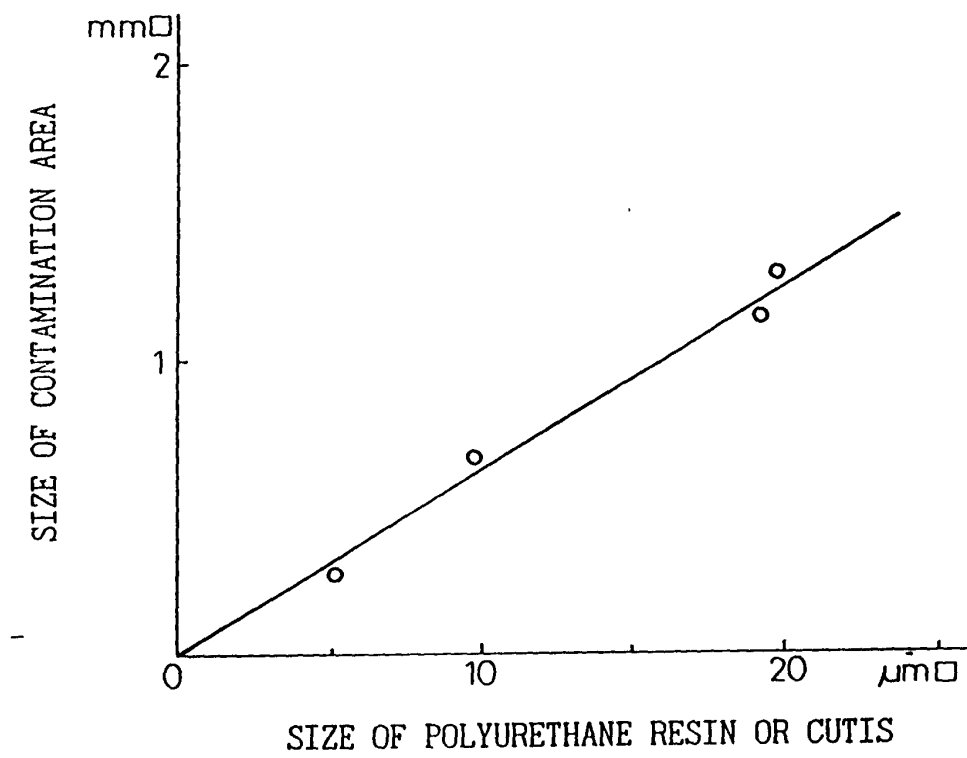
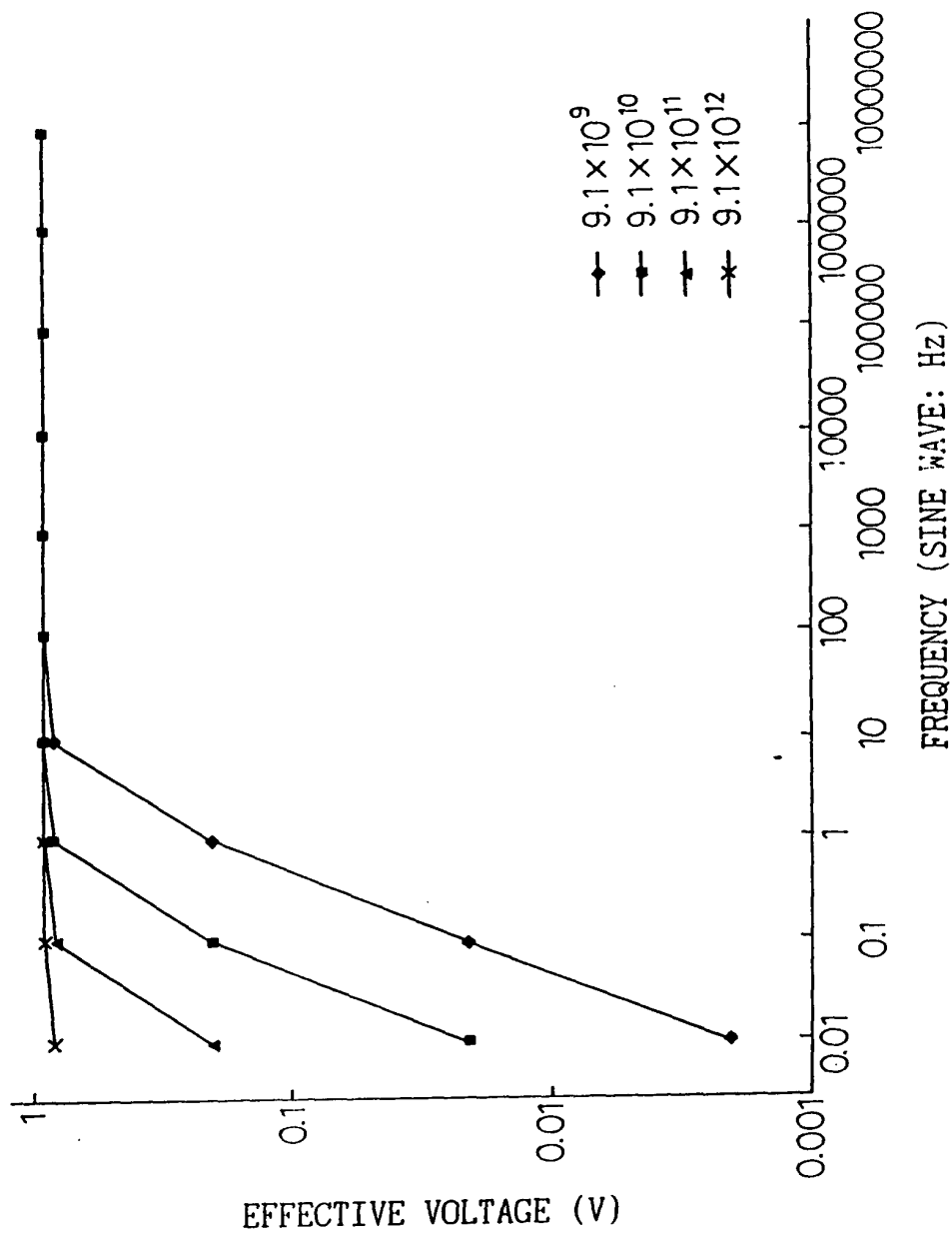
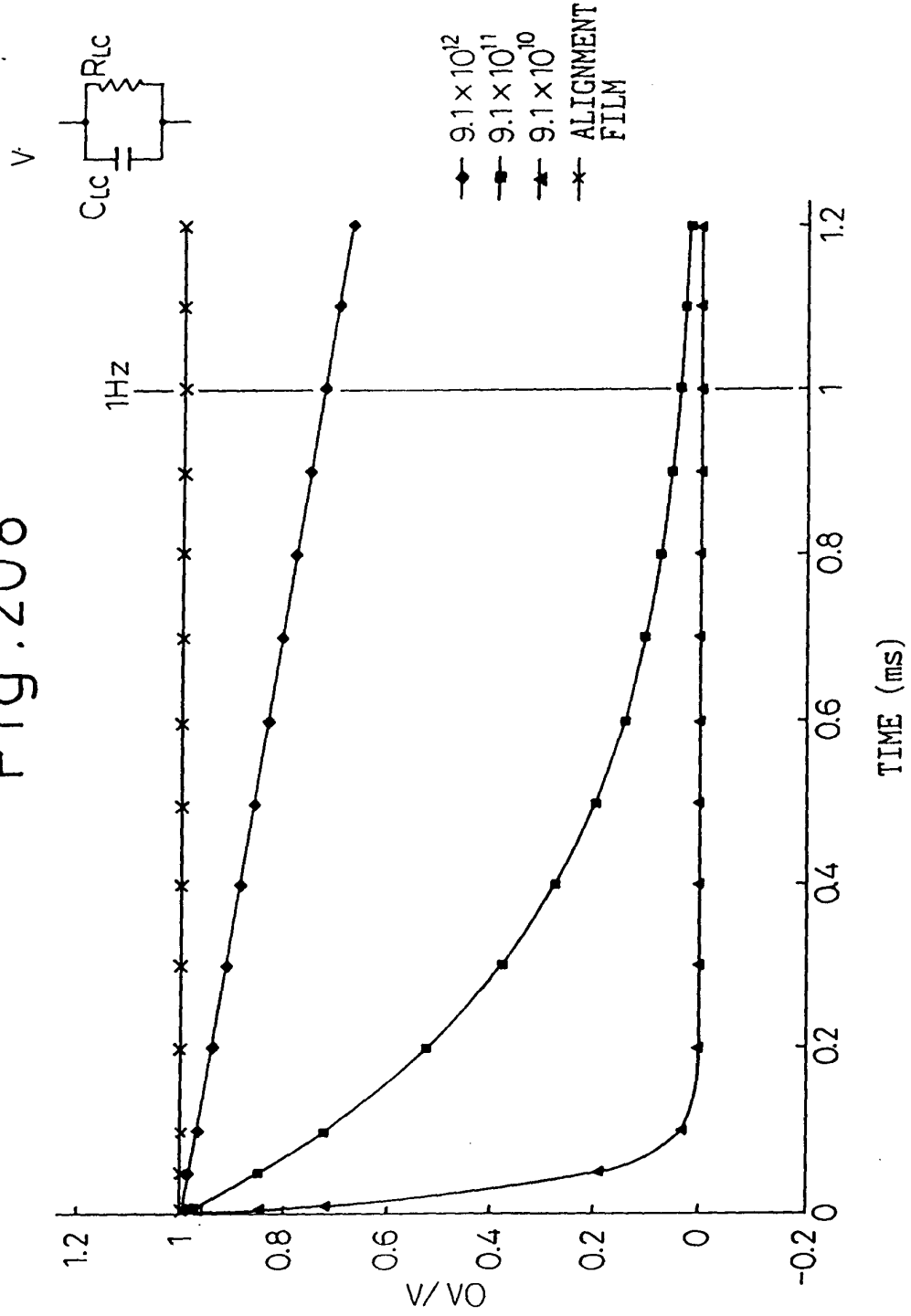


Fig. 207



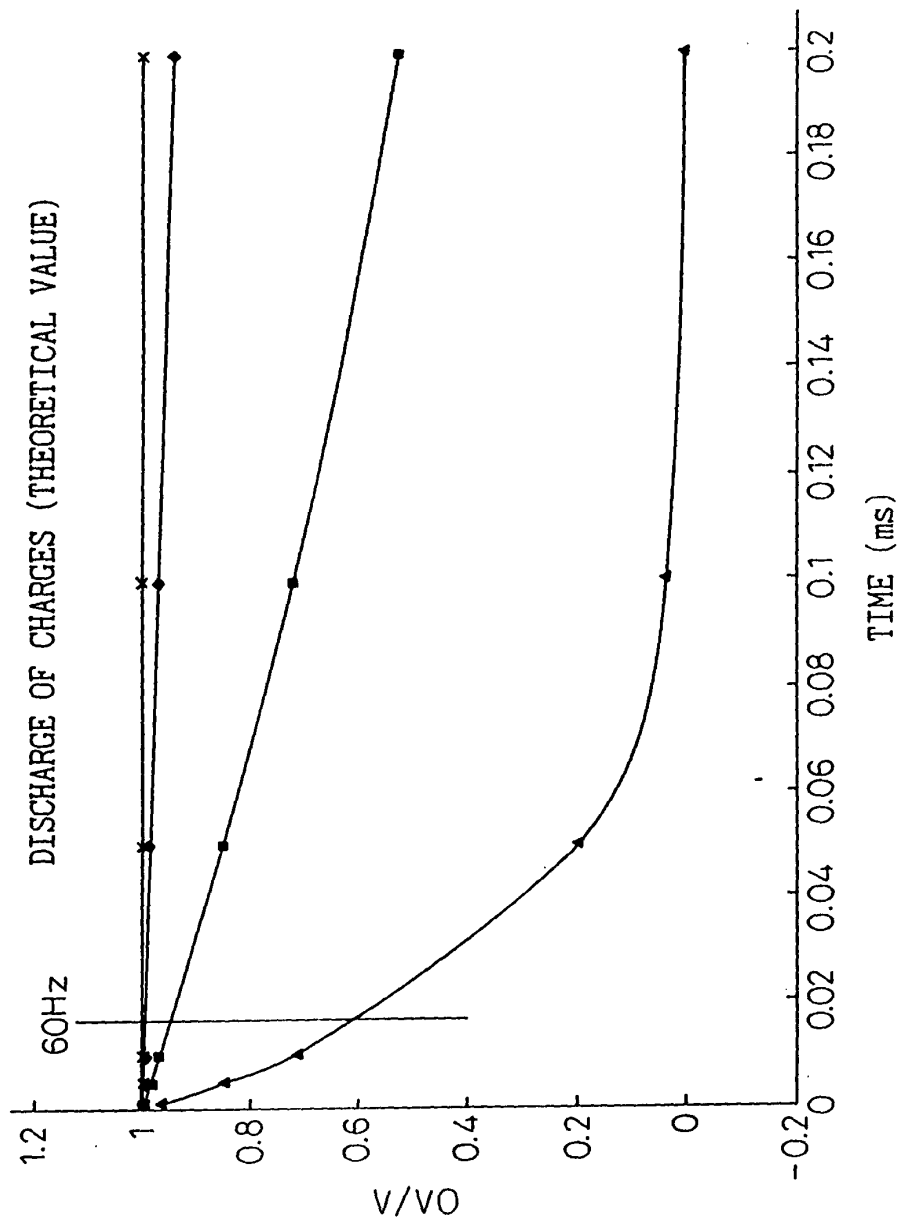
199/246

Fig. 208



200/246

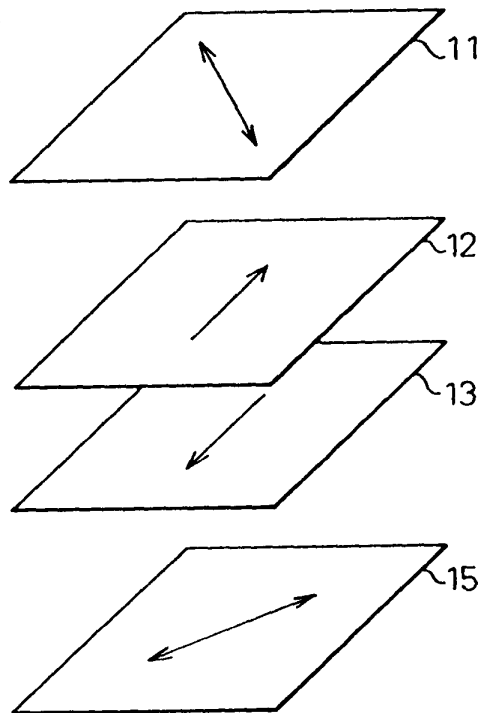
Fig. 209





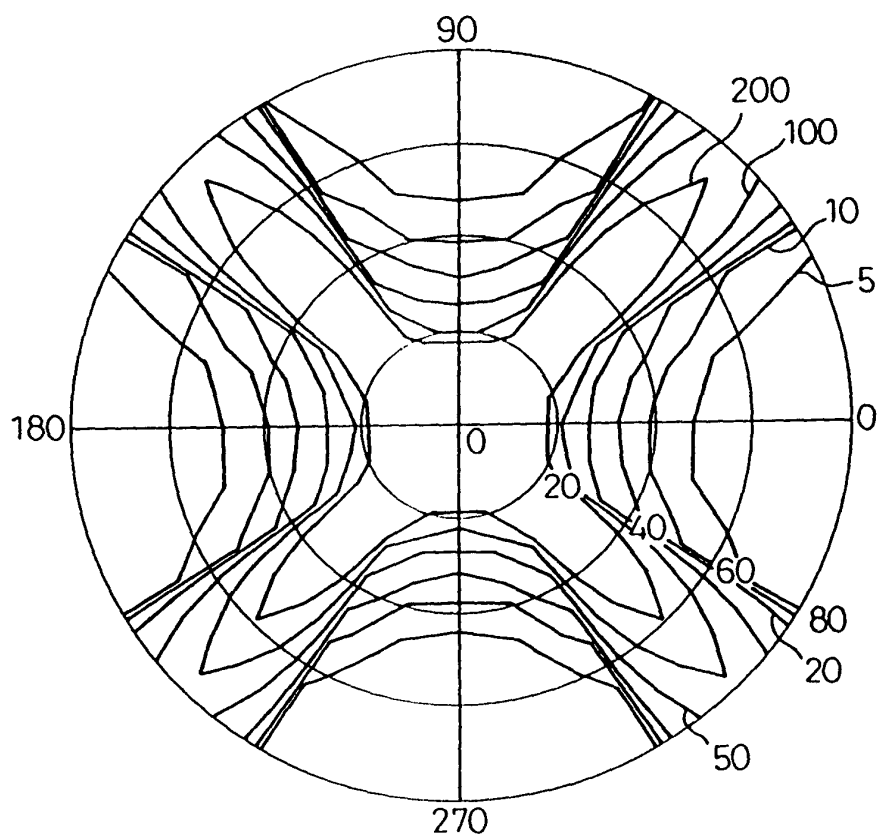
201/246

Fig. 210



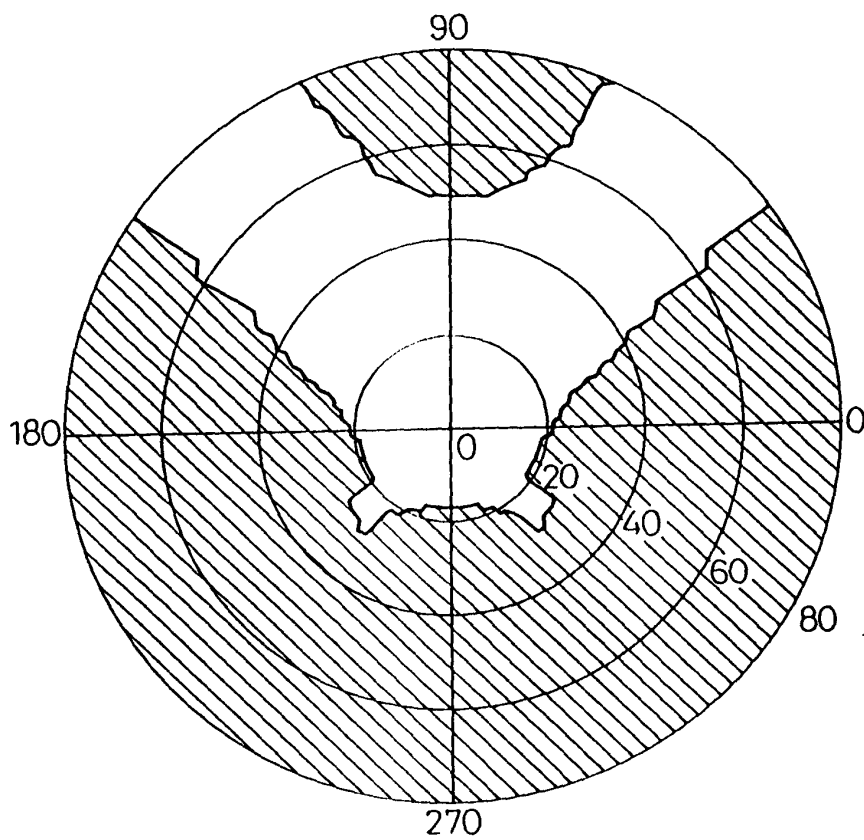
202/246

Fig. 211



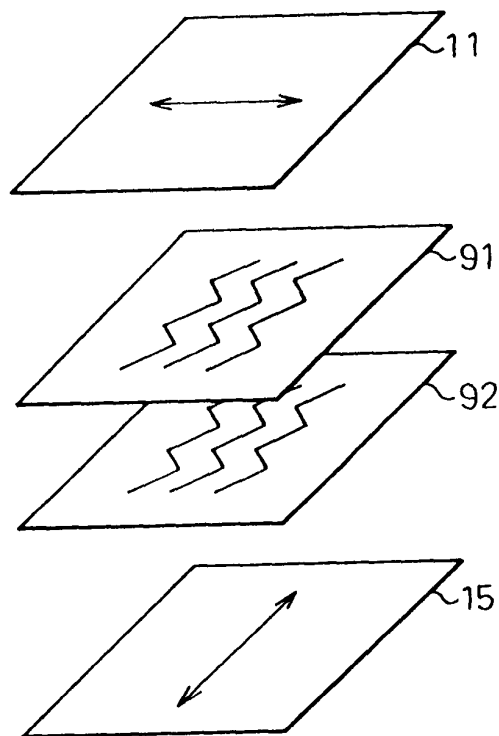
203/246

Fig .212



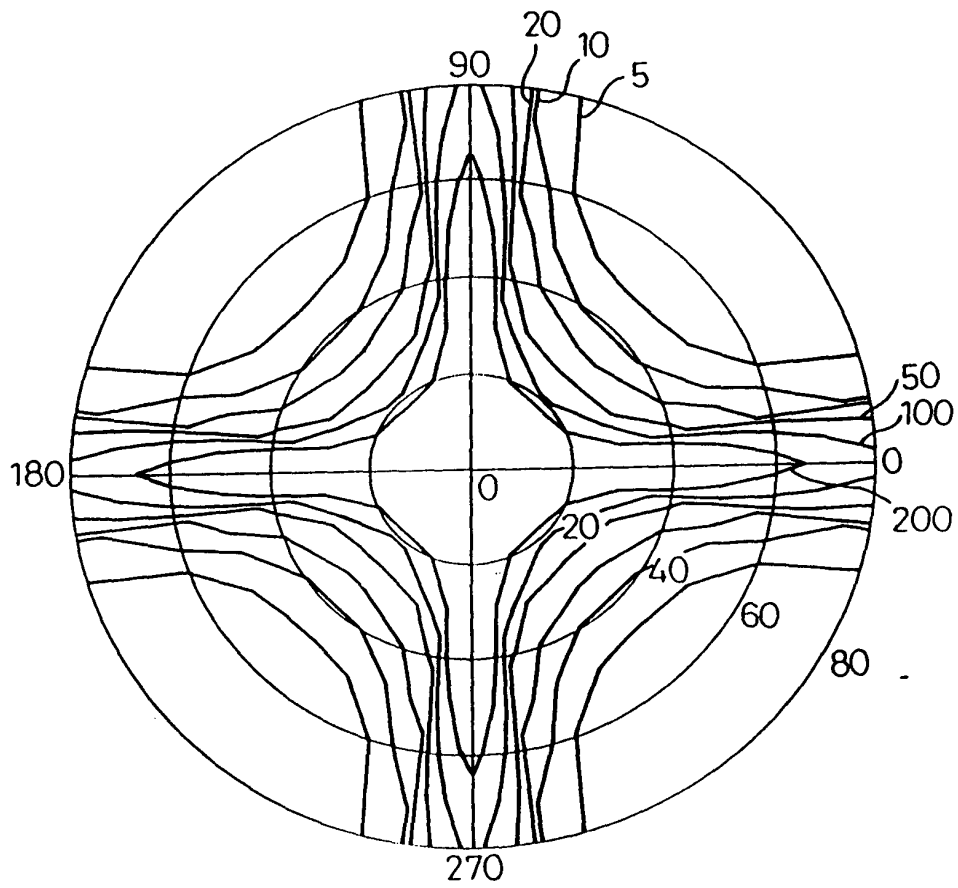
204/246

Fig.213



205/246

Fig. 214



206/246

Fig. 215

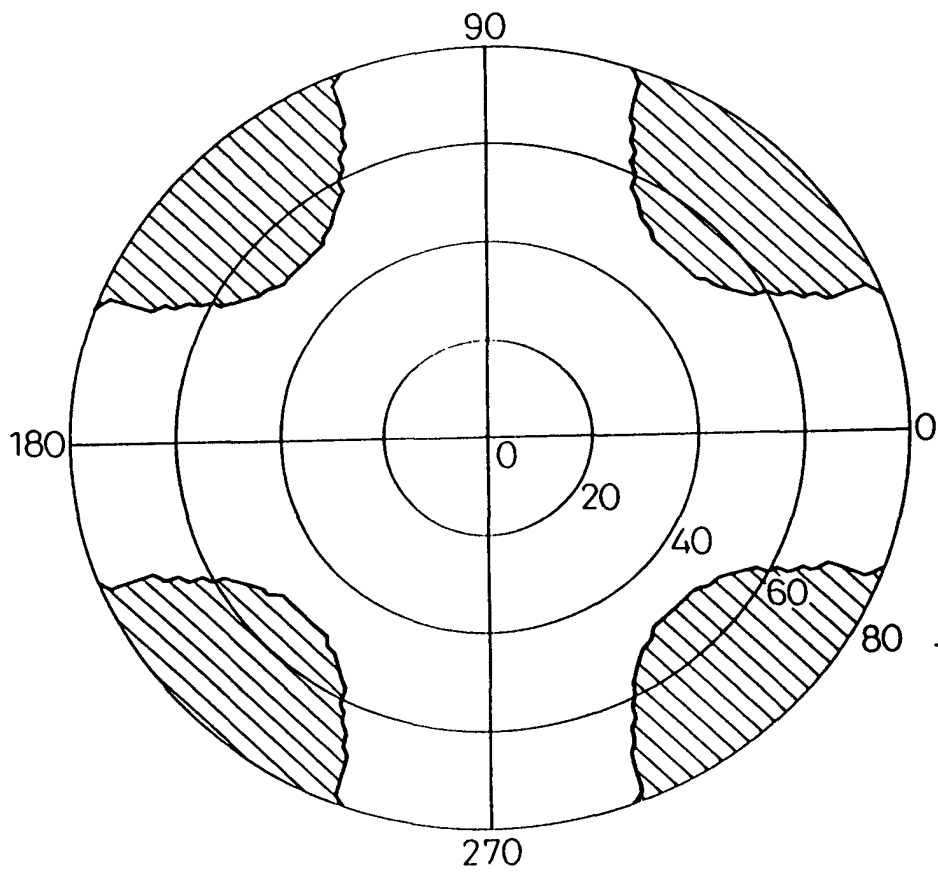
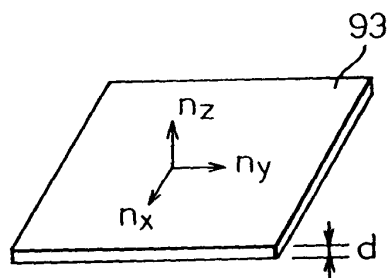


Fig.216



GENERAL CONDITION

$$n_x, n_y \geq n_z$$

POSITIVE UNIAXIAL FILM

$$n_x > n_y = n_z$$

NEGATIVE UNIAXIAL FILM

$$n_x = n_y > n_z$$

BIAXIAL FILM  
(A PHASE LAG AXIS IS X DIRECTION.)

$$n_x > n_y > n_z$$

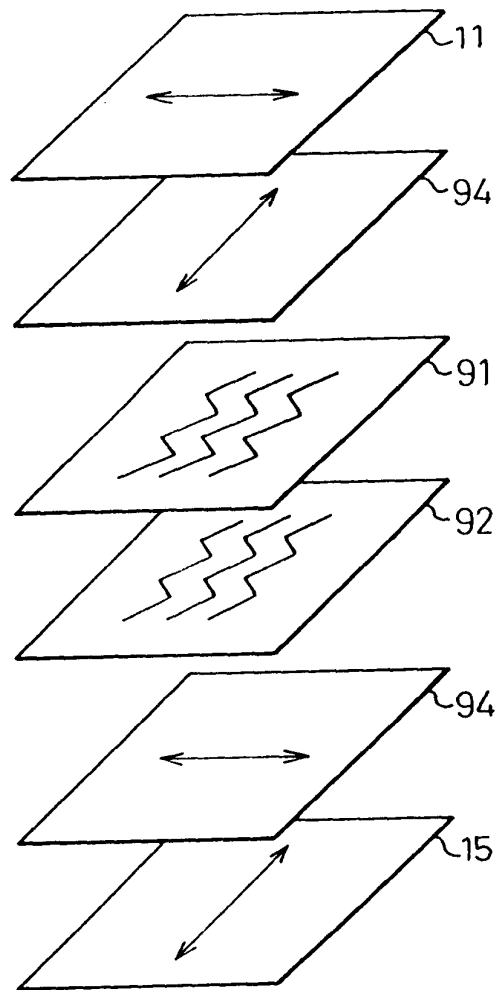
RETARDATION IN  
INPLANE DIRECTIONS

$$R = (n_x - n_y)d$$

RETARDATION OF  
THICKNESS DIRECTION

$$R = \left( \frac{n_x + n_y}{2} - n_z \right) d$$

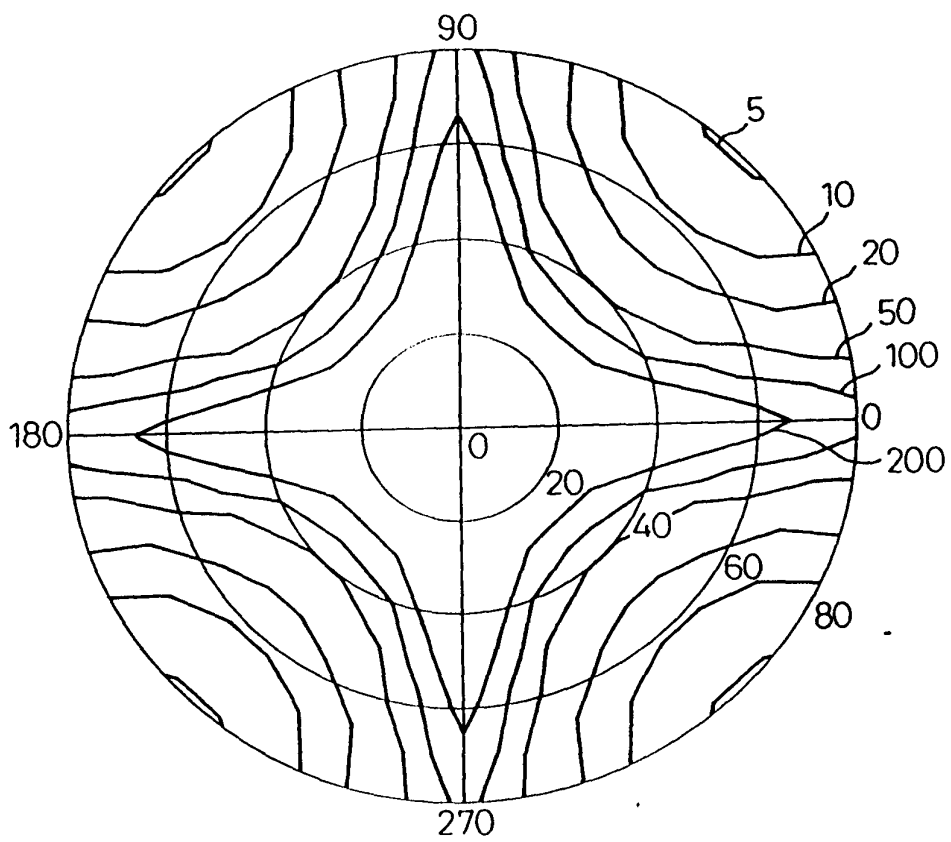
Fig. 217





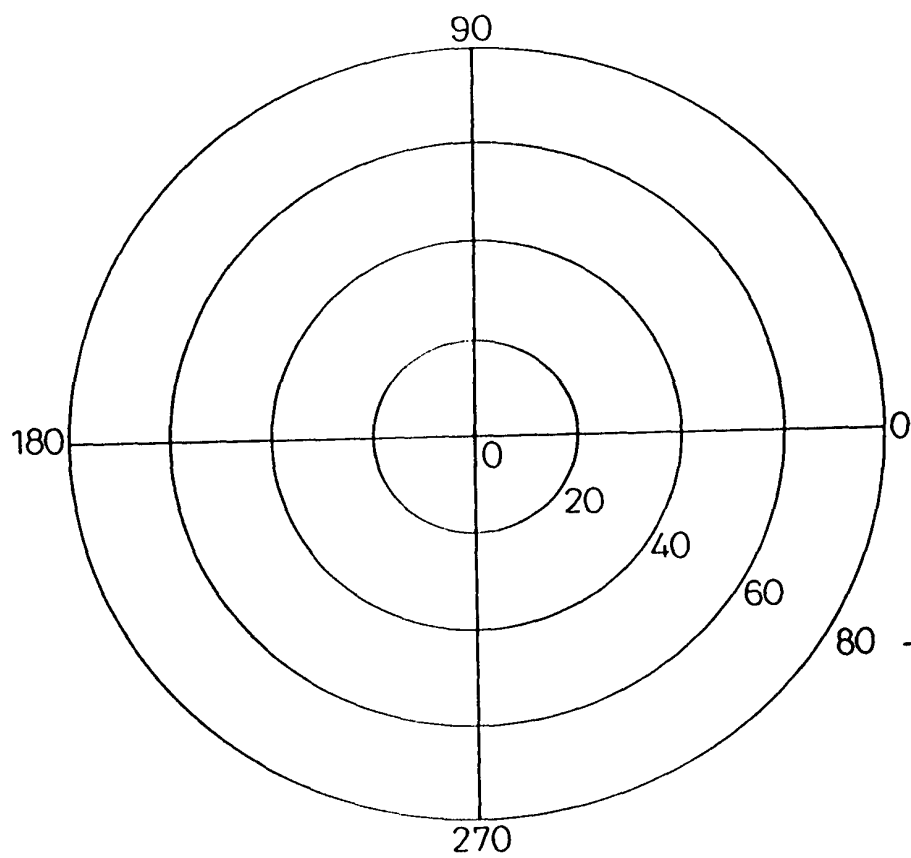
209/246

Fig.218



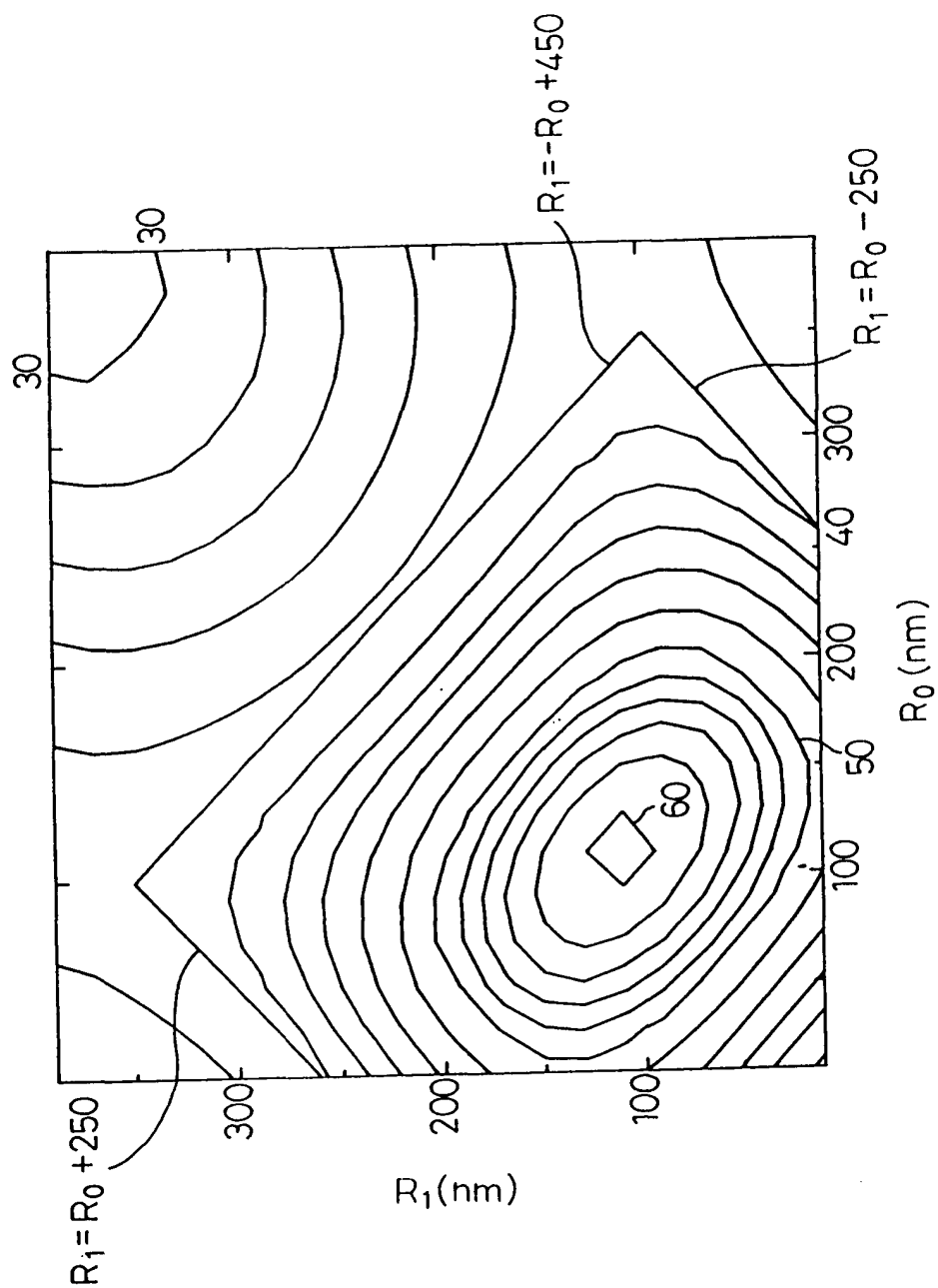
210/246

Fig. 219



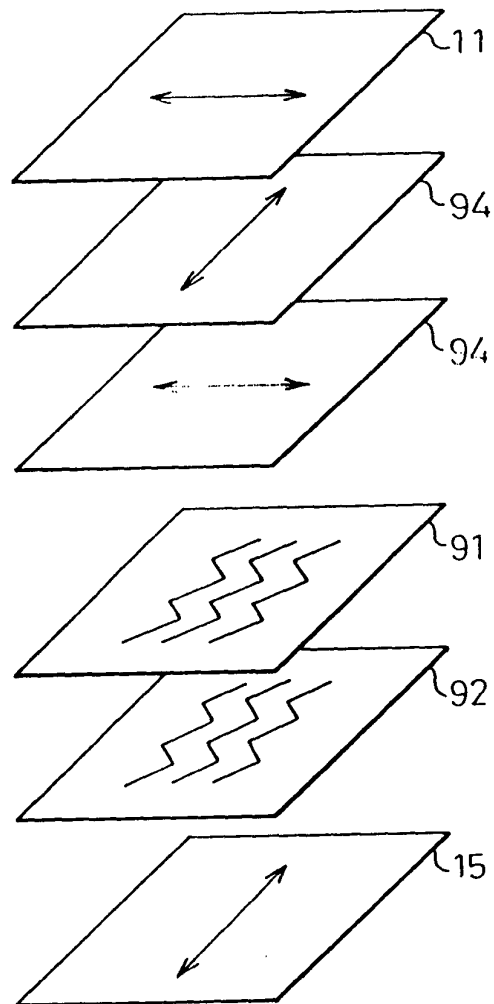
$\frac{211}{246}$

Fig. 220



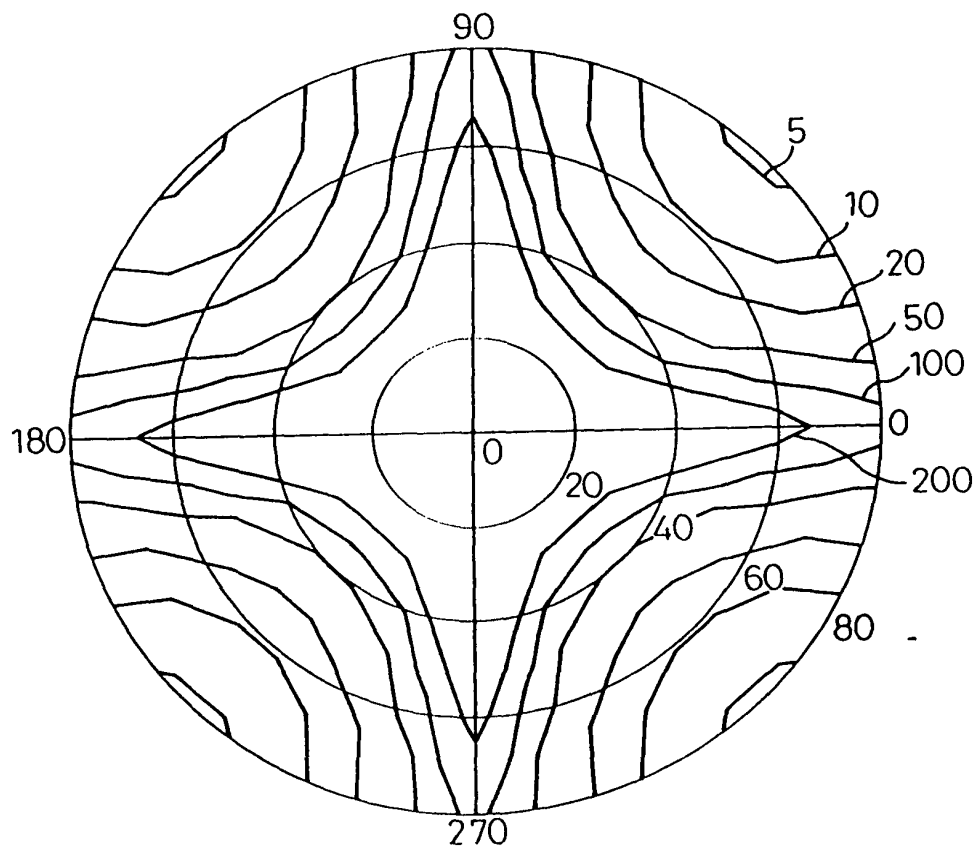
212/246

Fig. 221



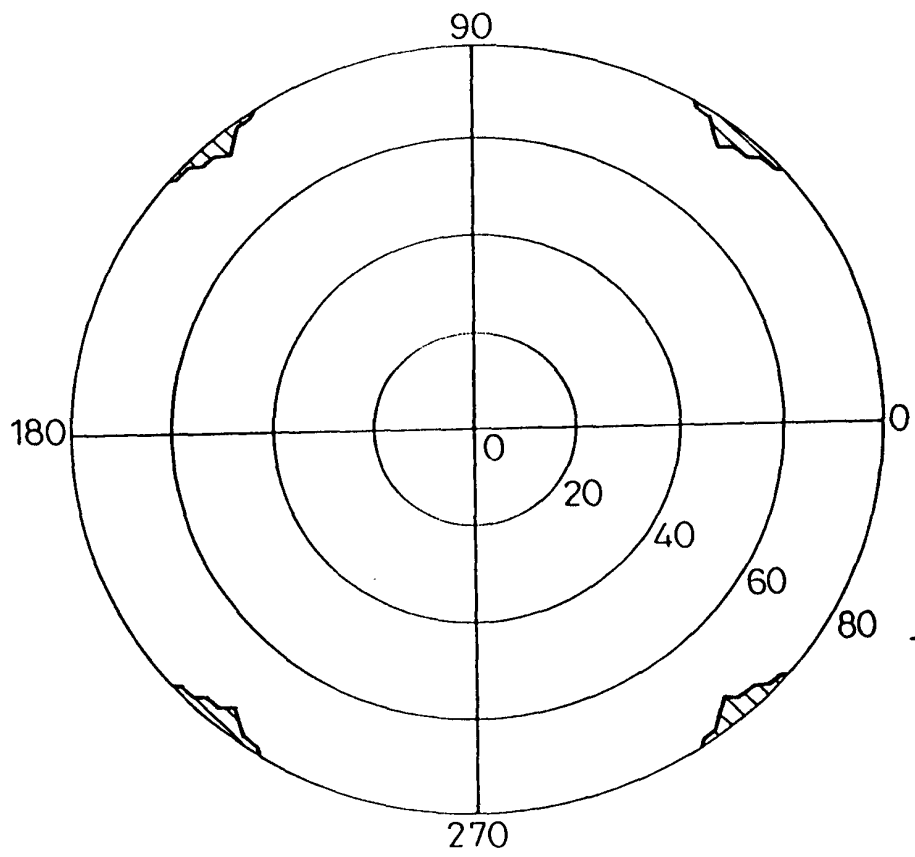
213/246

Fig. 222



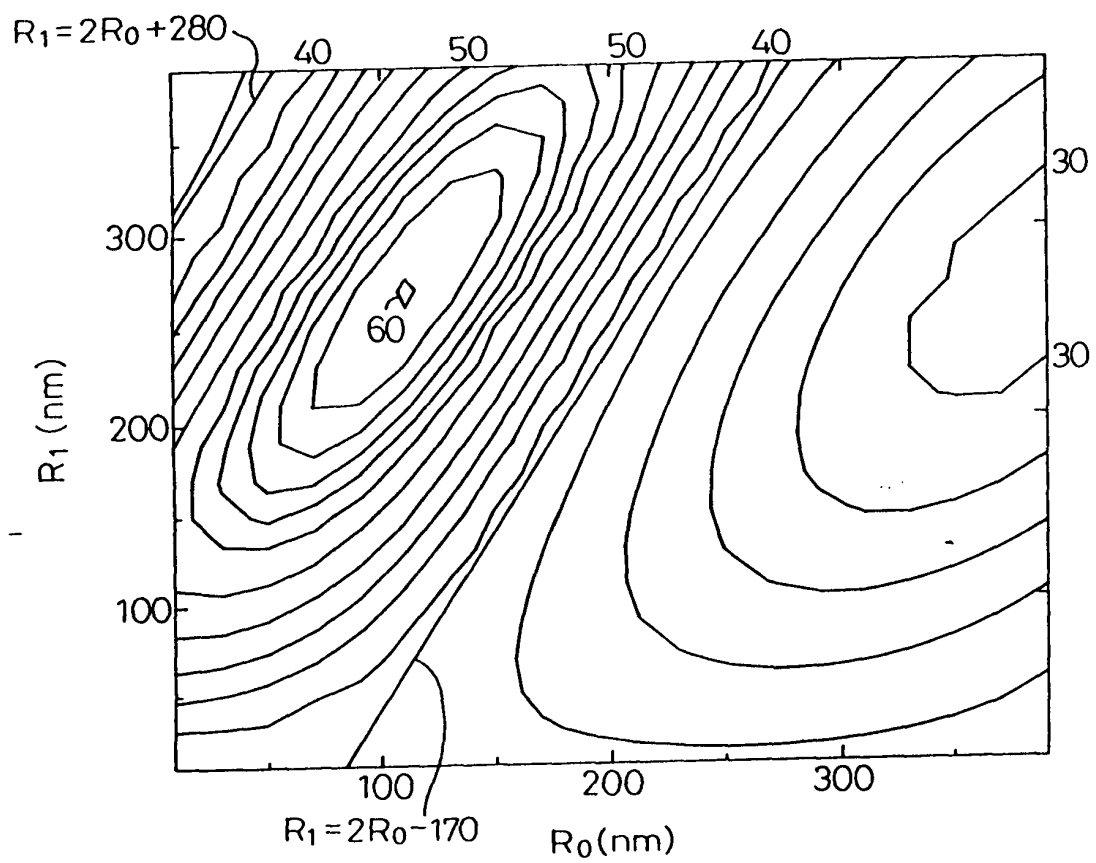
214/246

Fig. 223



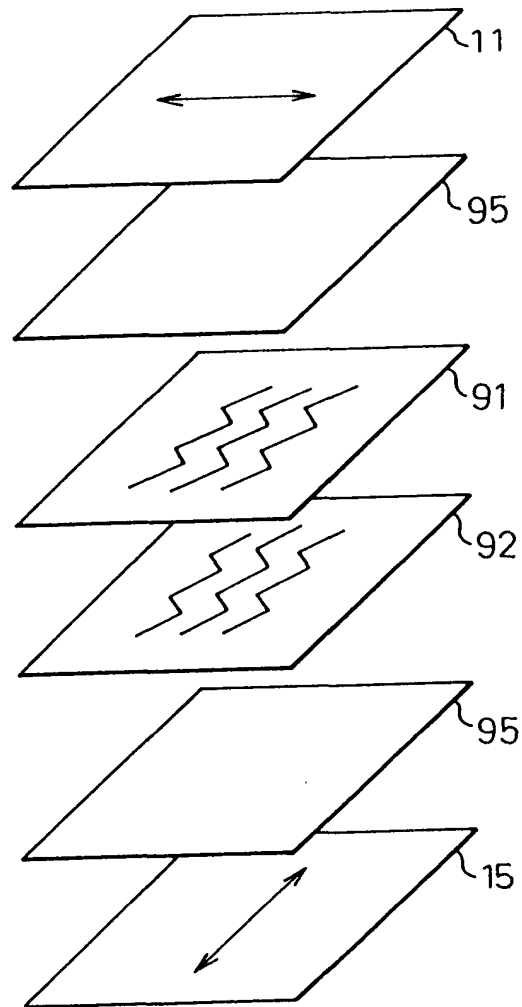
215/246

Fig. 224



216/246

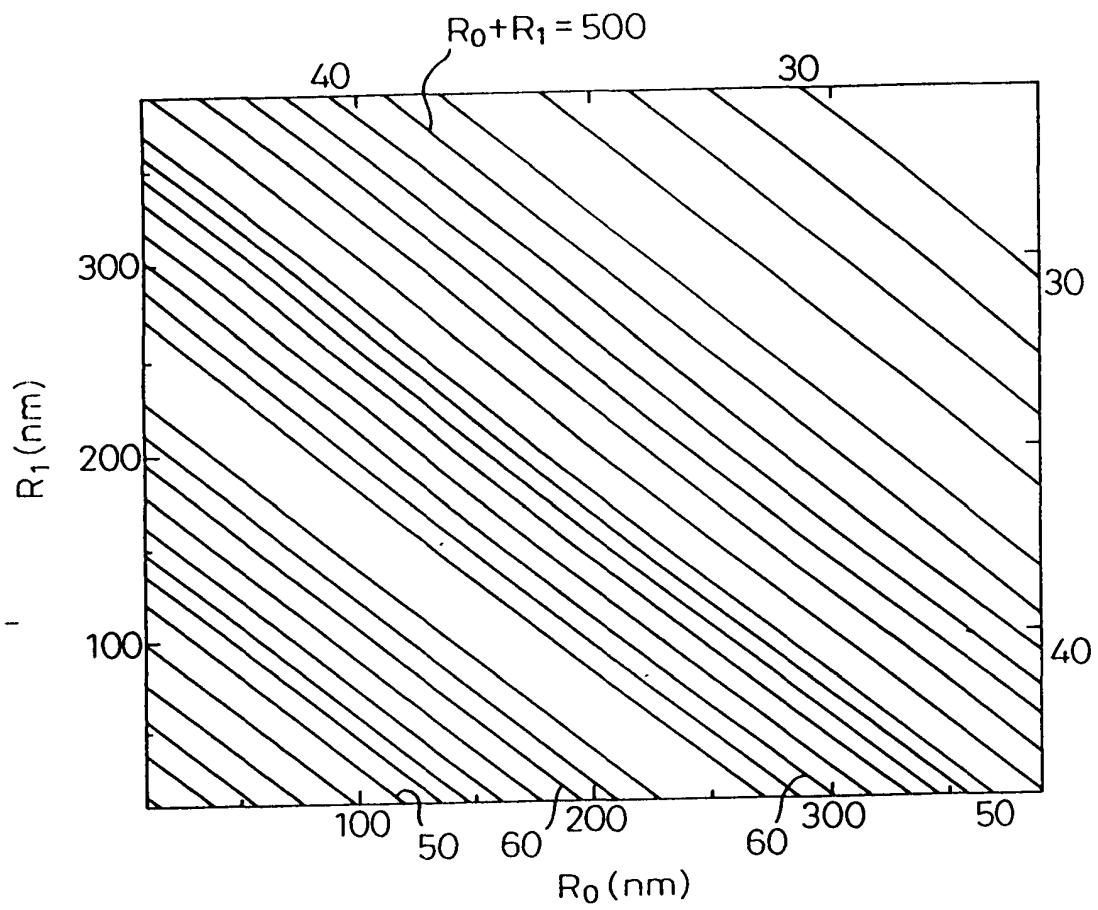
Fig. 225





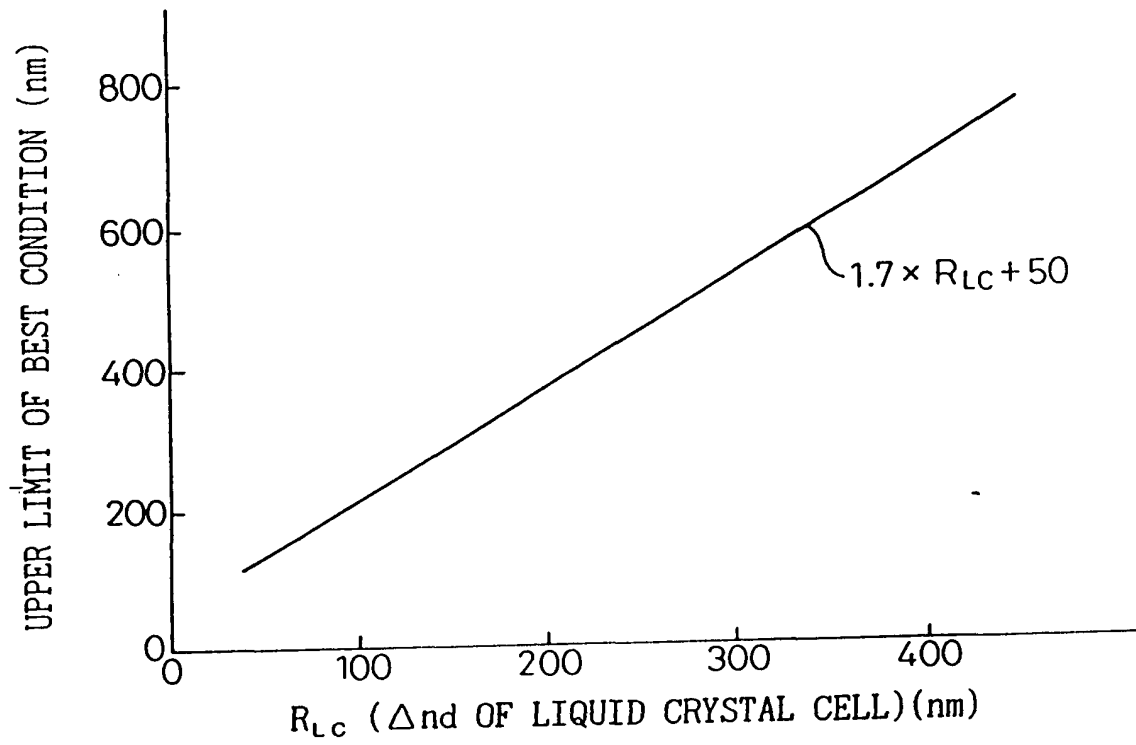
217/246

Fig. 226



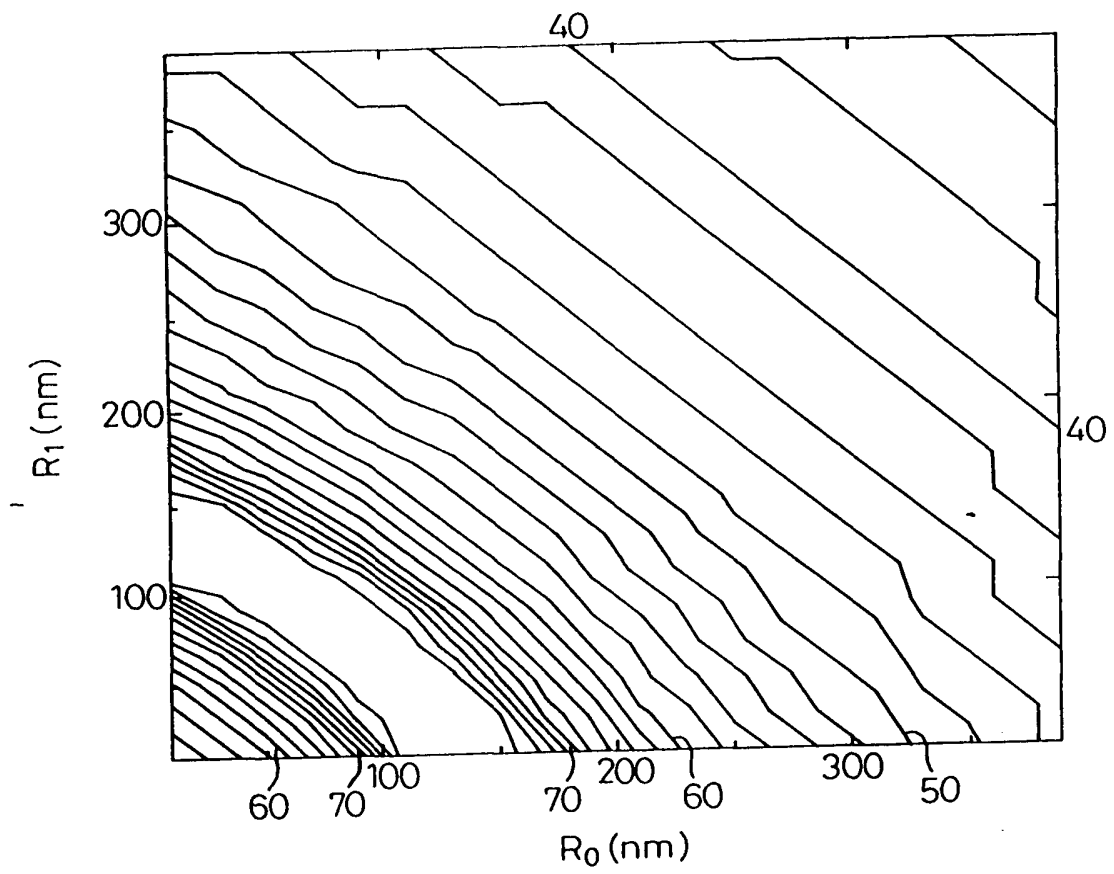
218/246

Fig.227



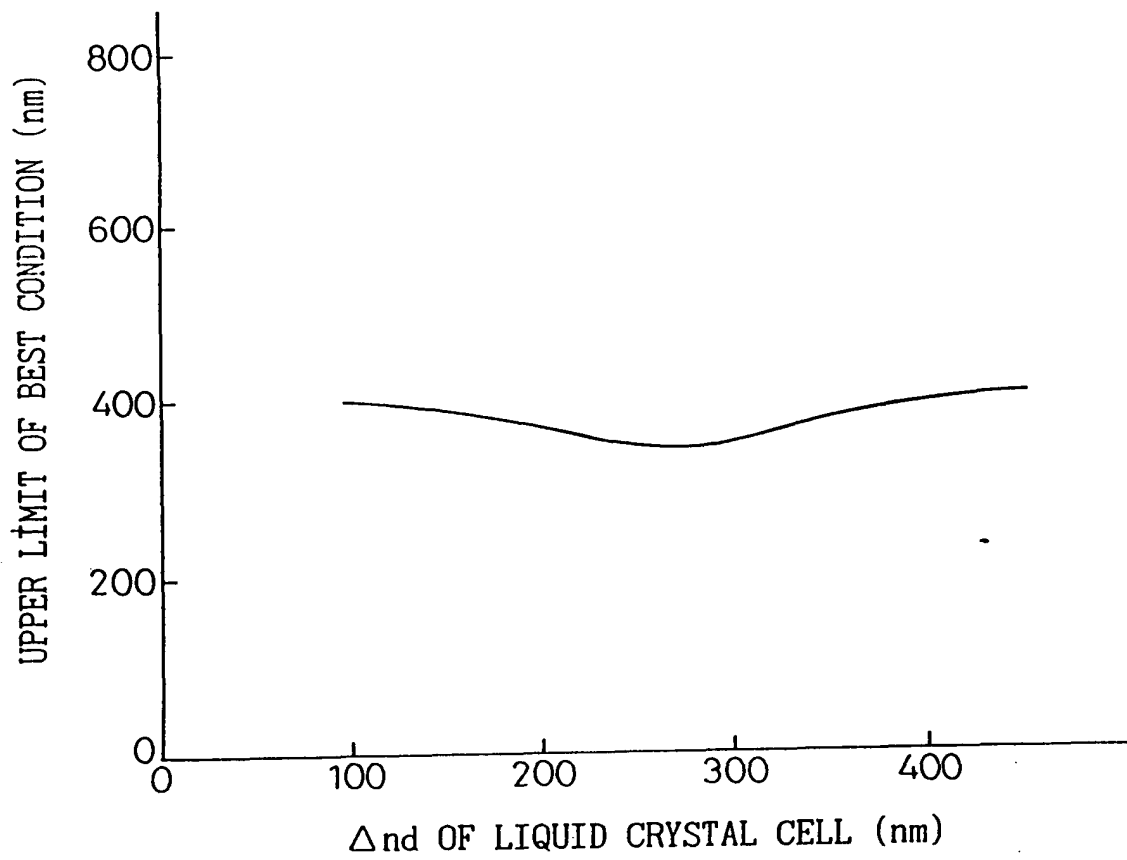
219/246

Fig.228



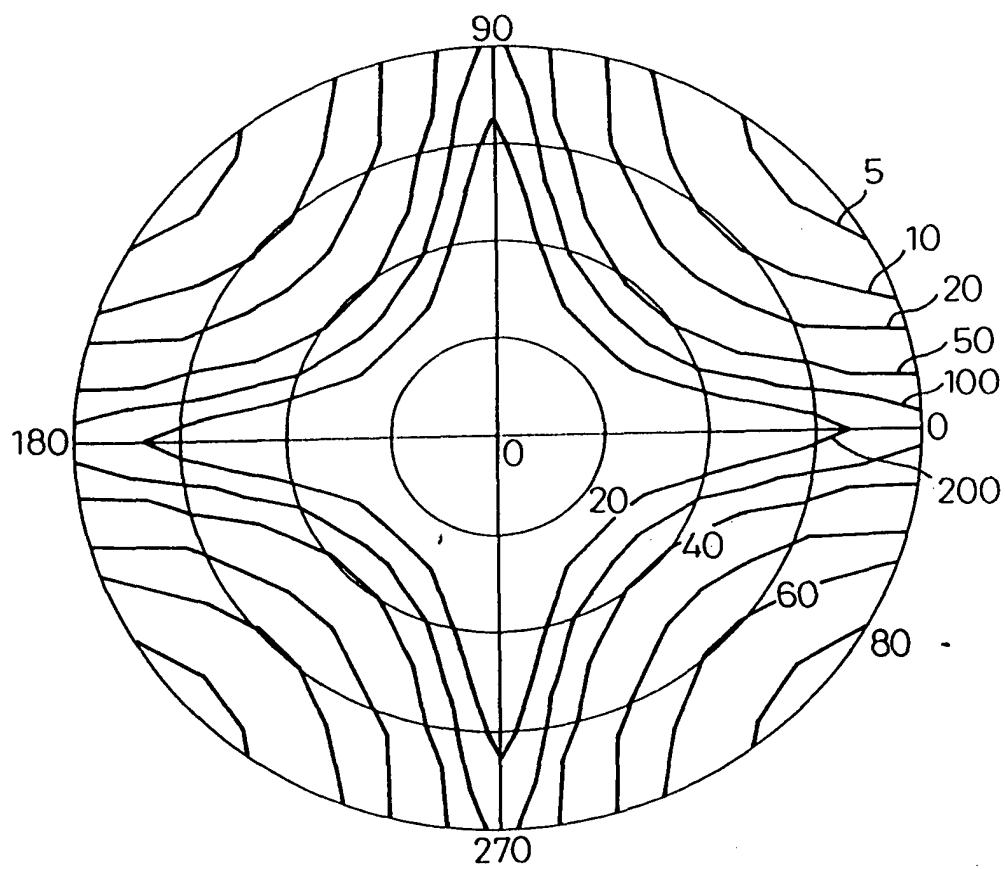
220/246

Fig. 229



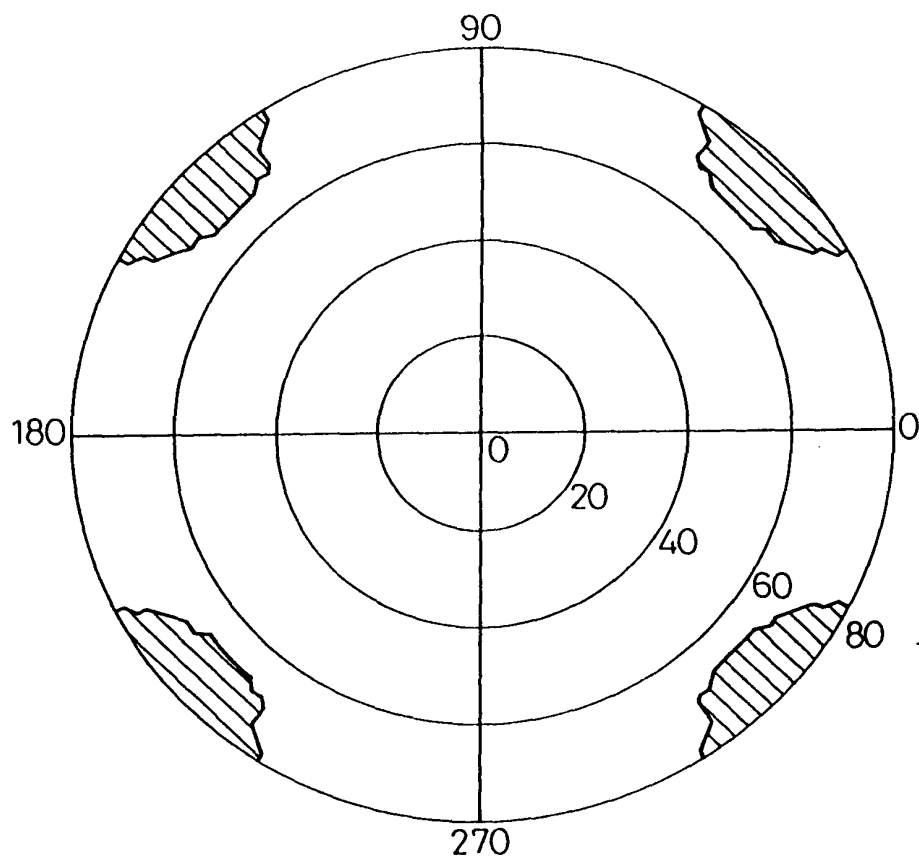
221/246

Fig. 230



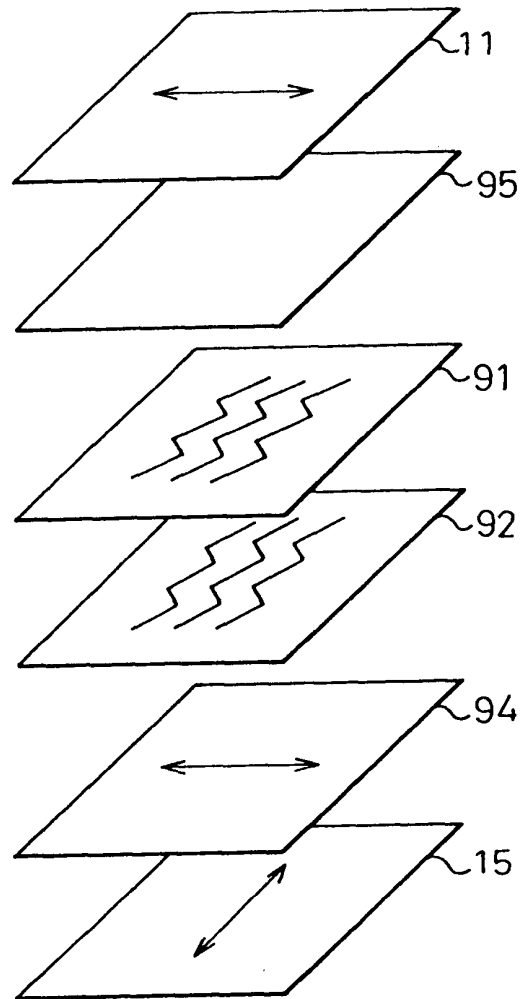
222/246

Fig. 231



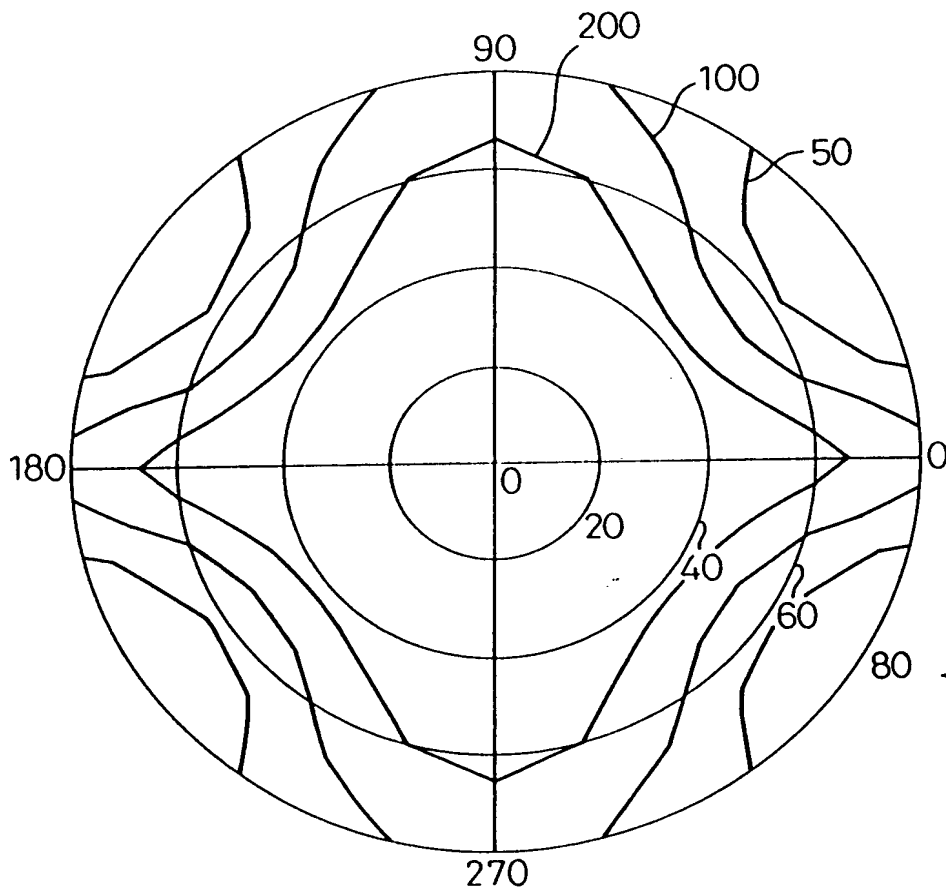
223/246

Fig. 232



224/246

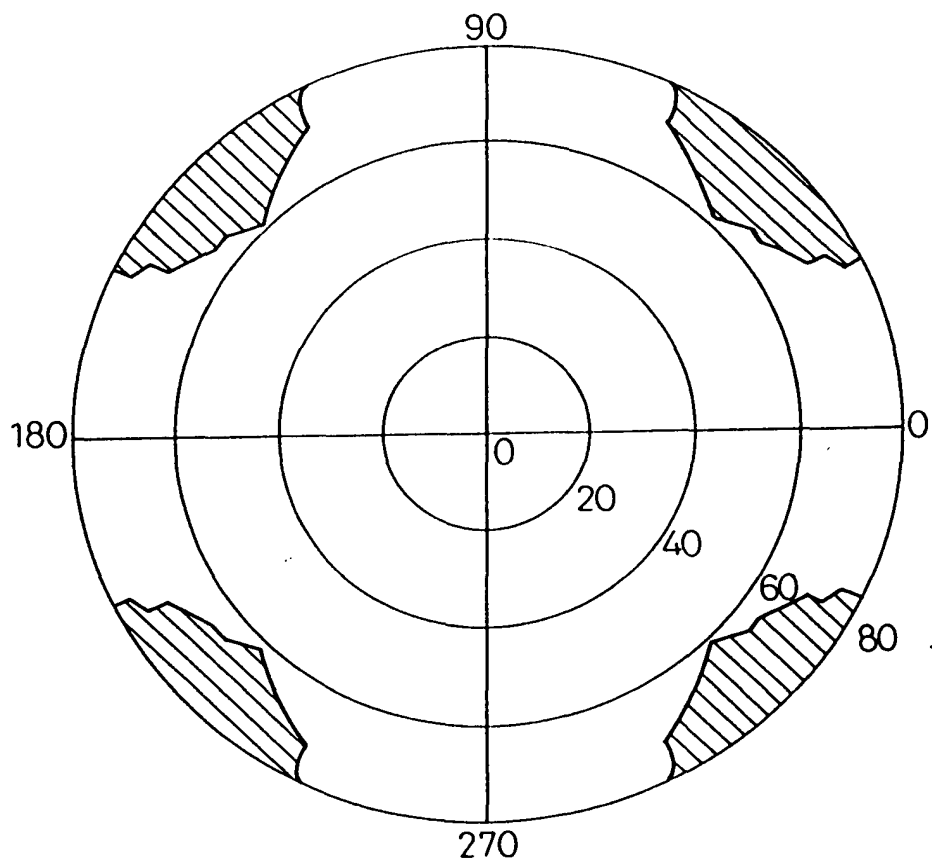
Fig. 233





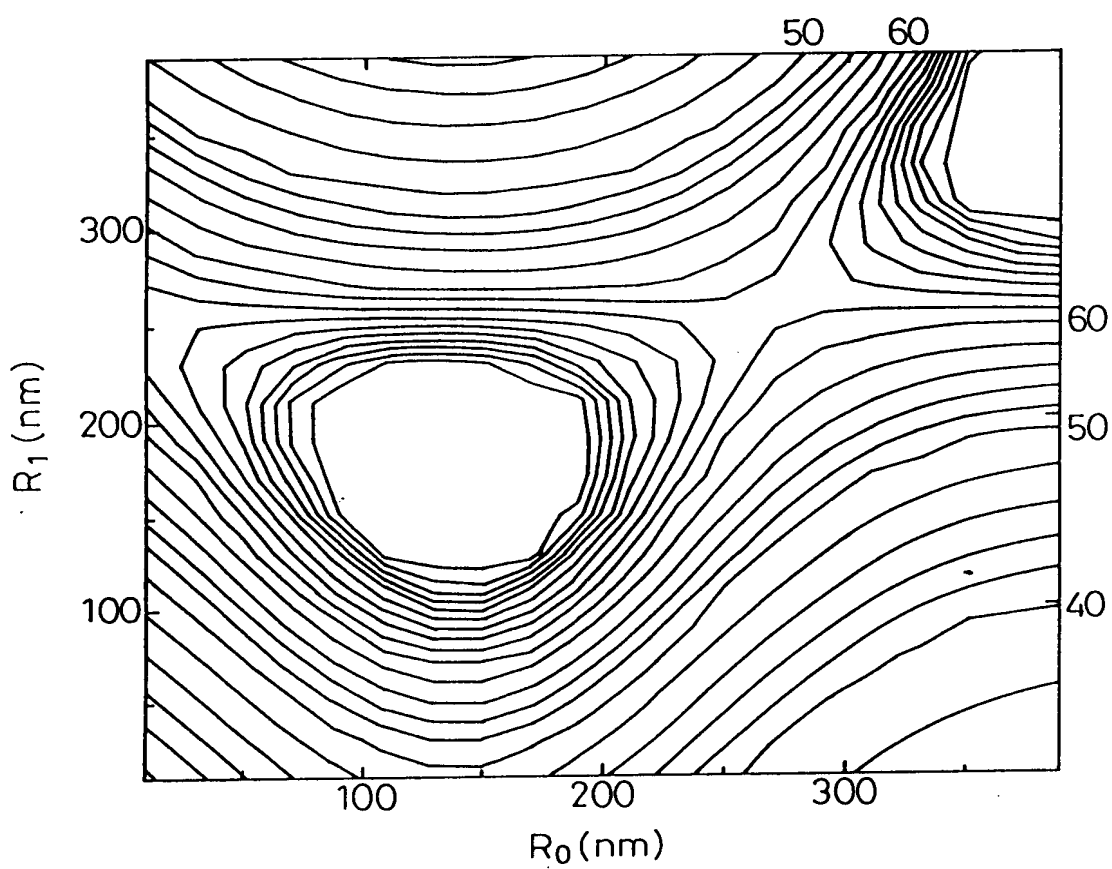
225/246

Fig. 234



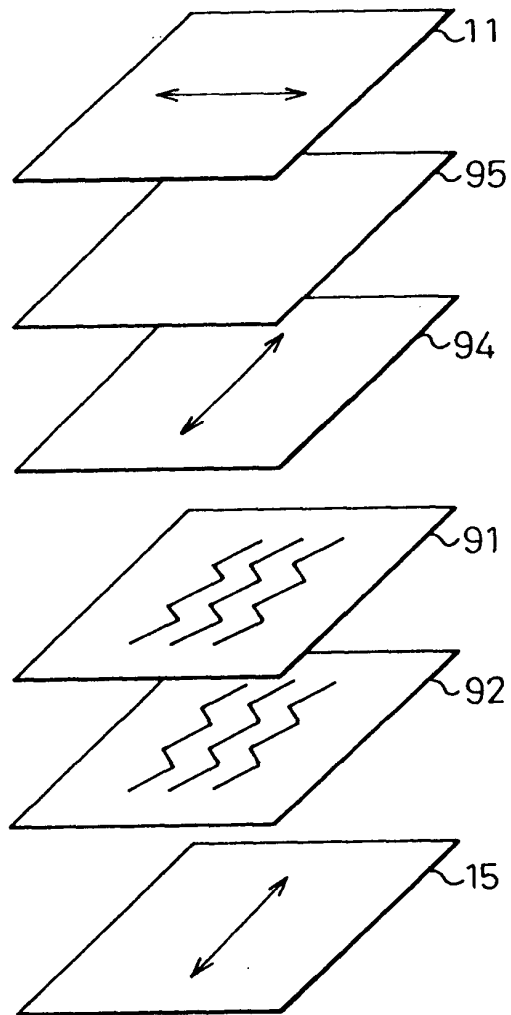
226/246

Fig. 235



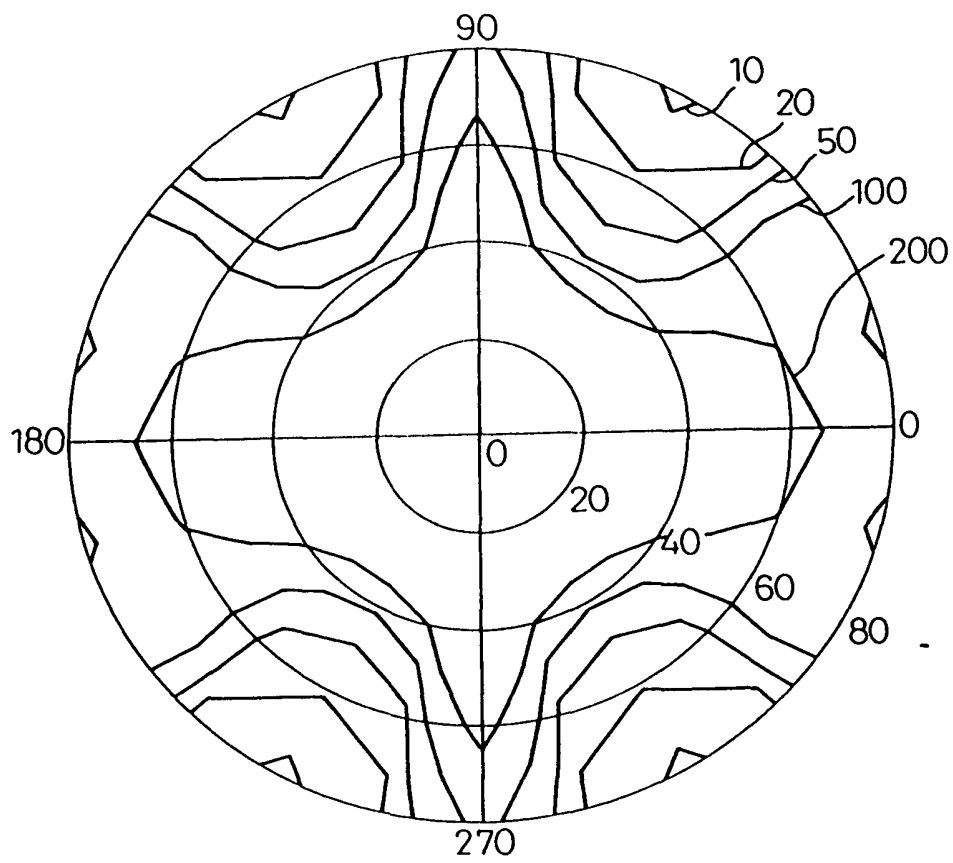
227/246

Fig. 236



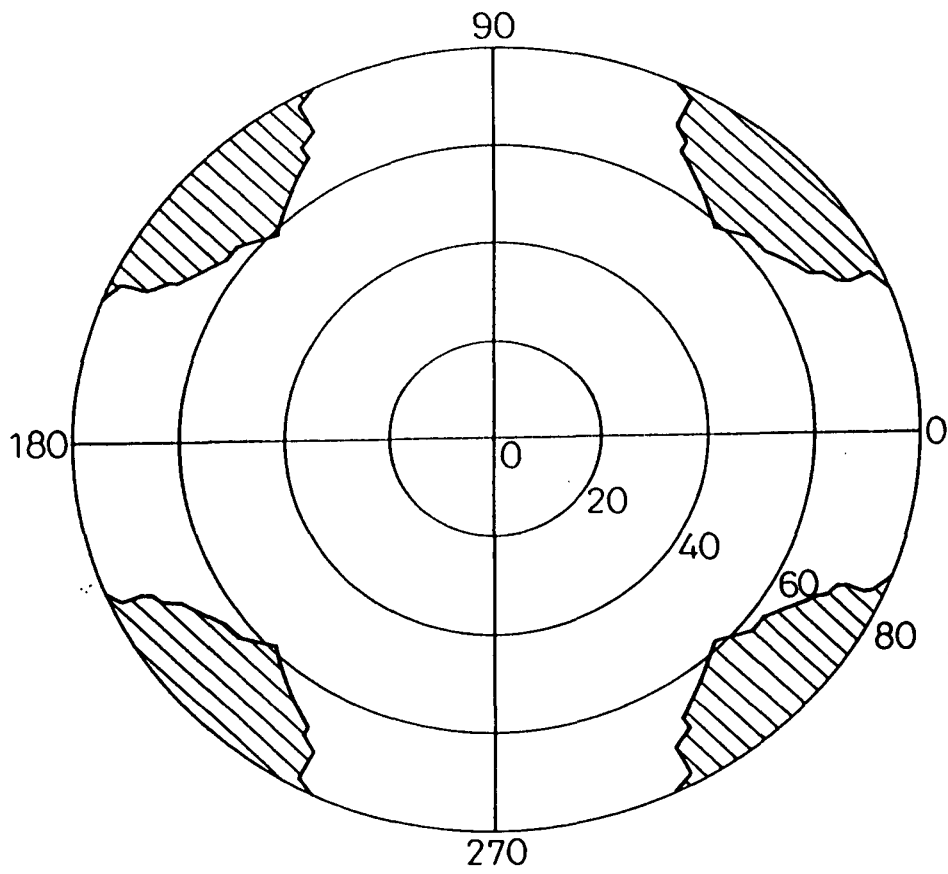
228/  
246

Fig. 237



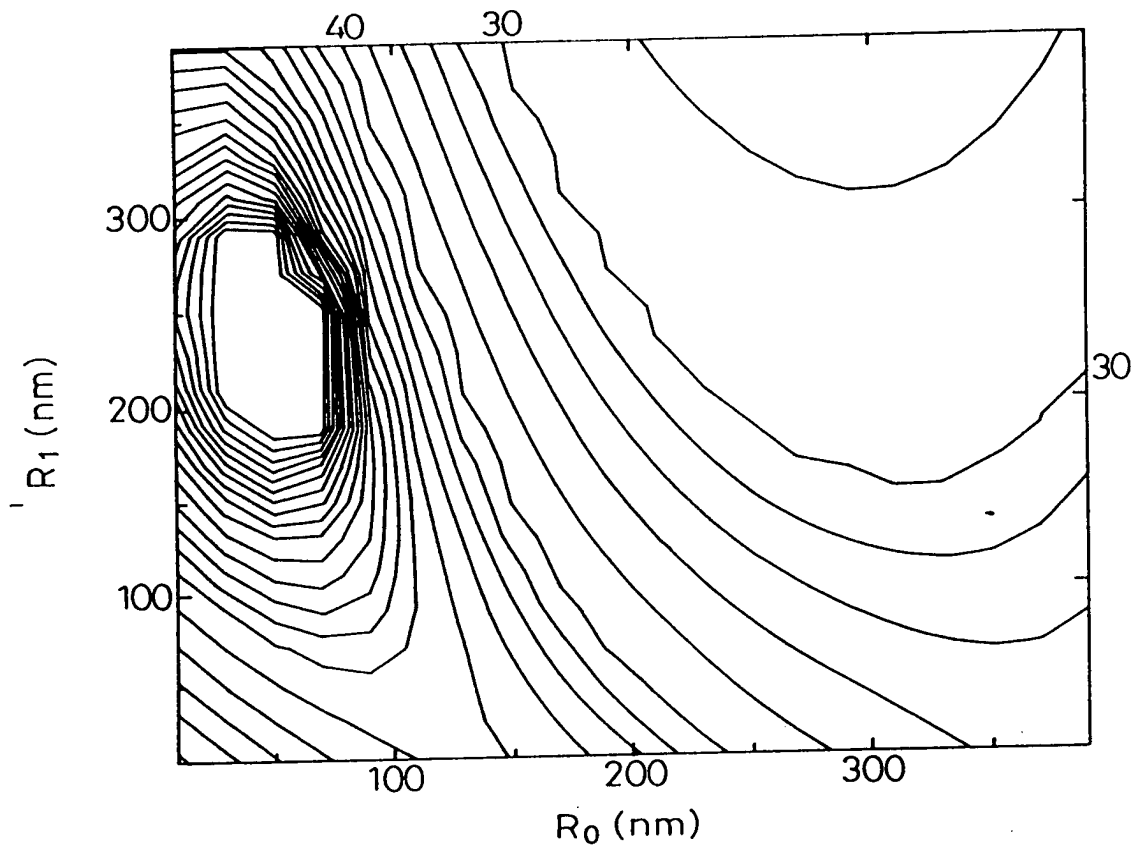
229/246

Fig. 238



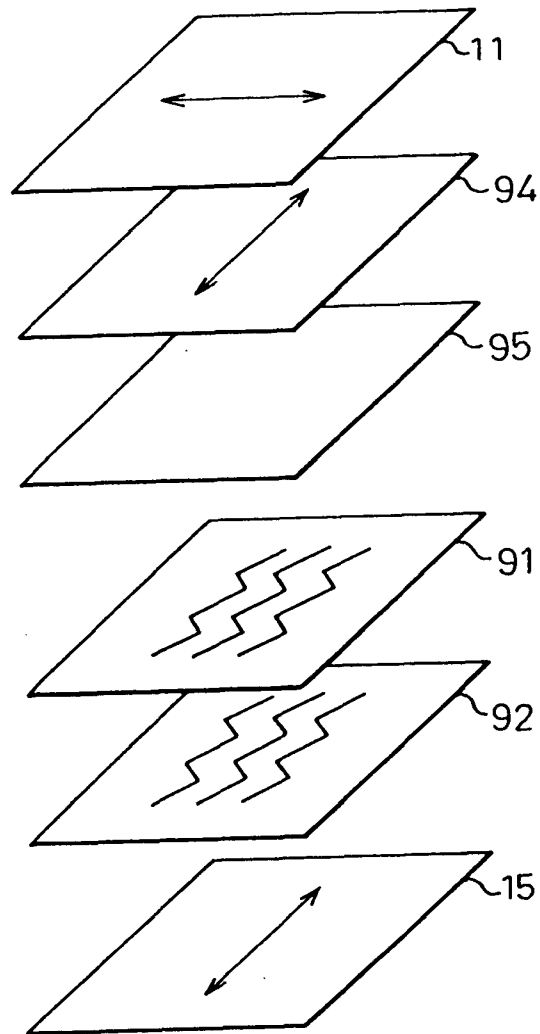
$\frac{230}{246}$

Fig. 239



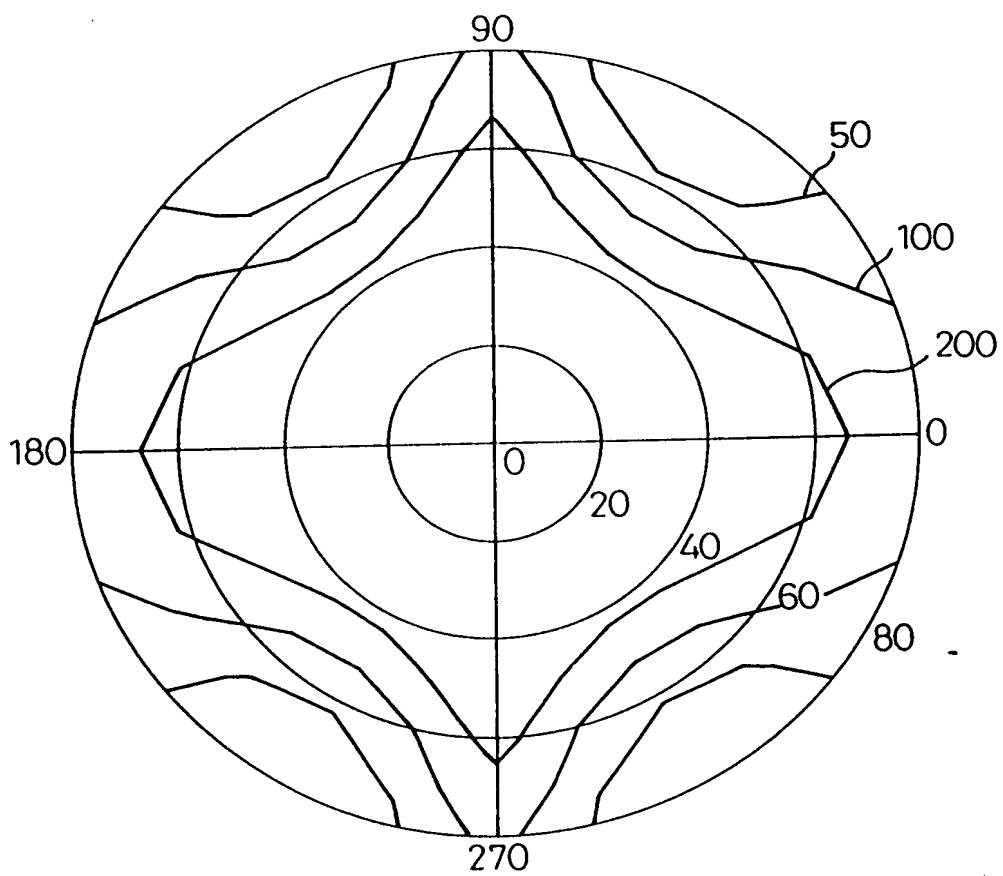
231/246

Fig. 240



232/246

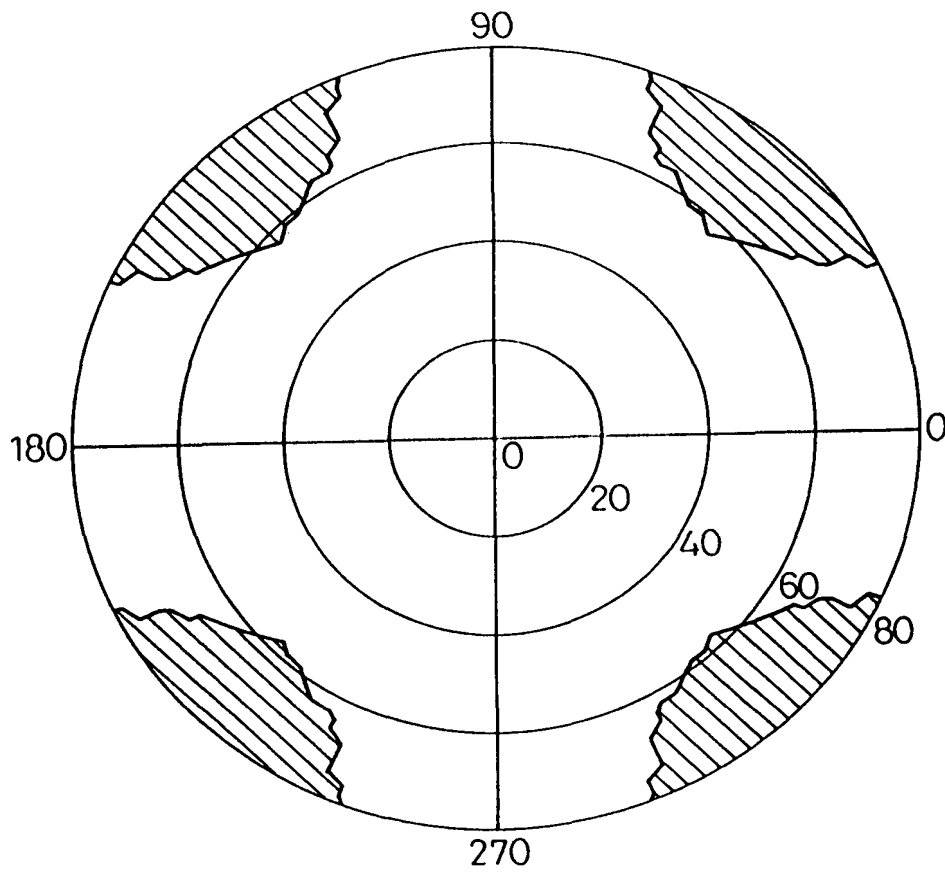
Fig. 241





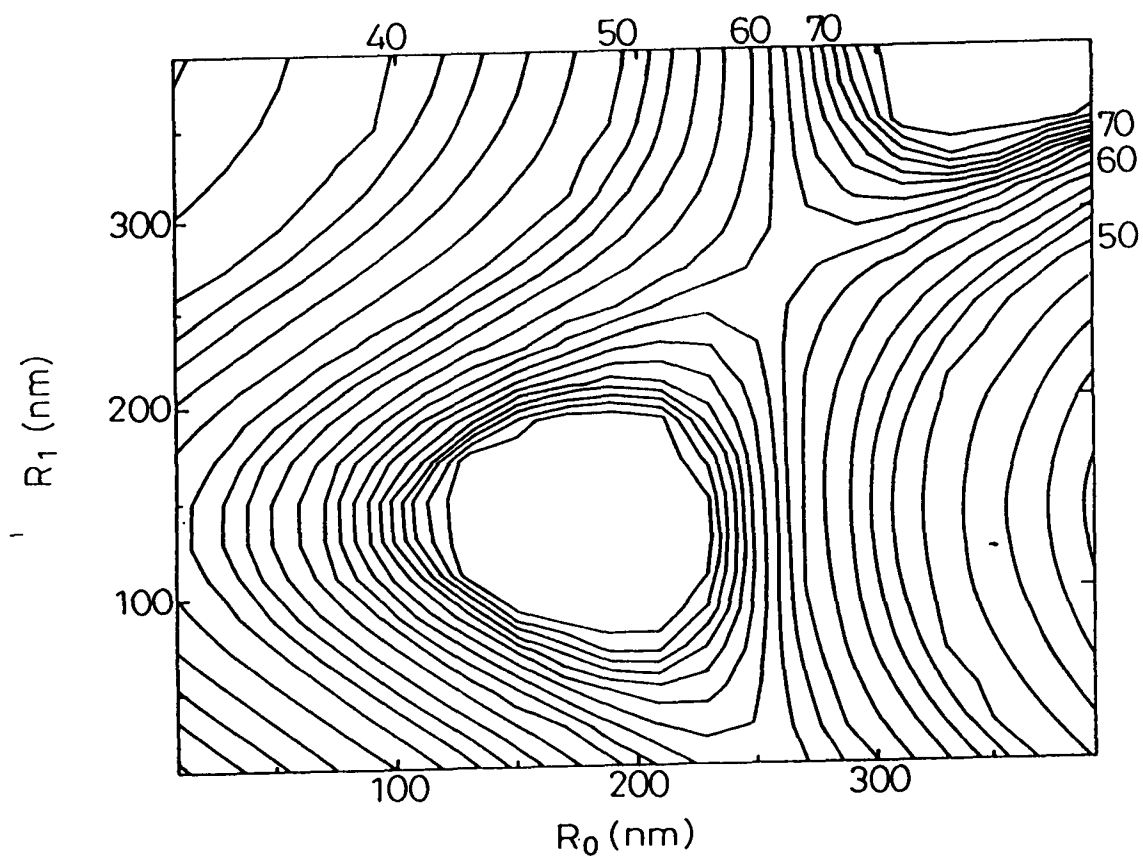
233/246

Fig. 242



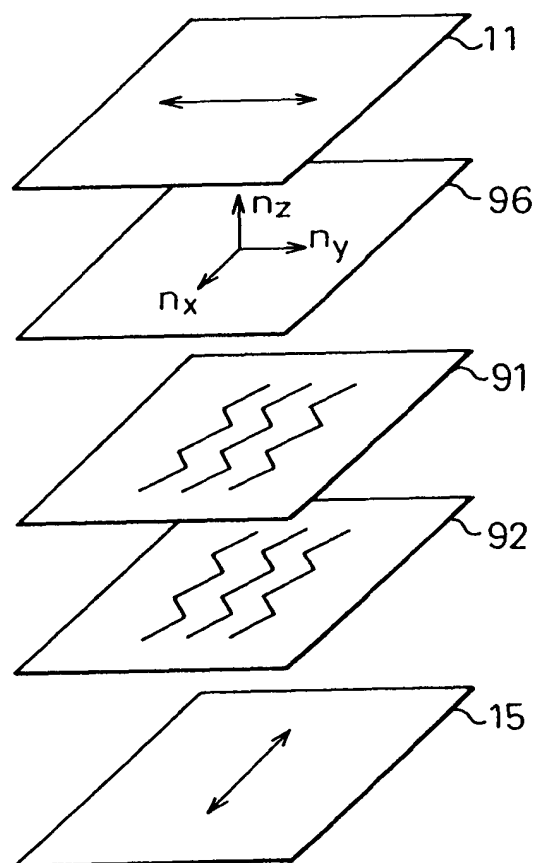
234/246

Fig .243



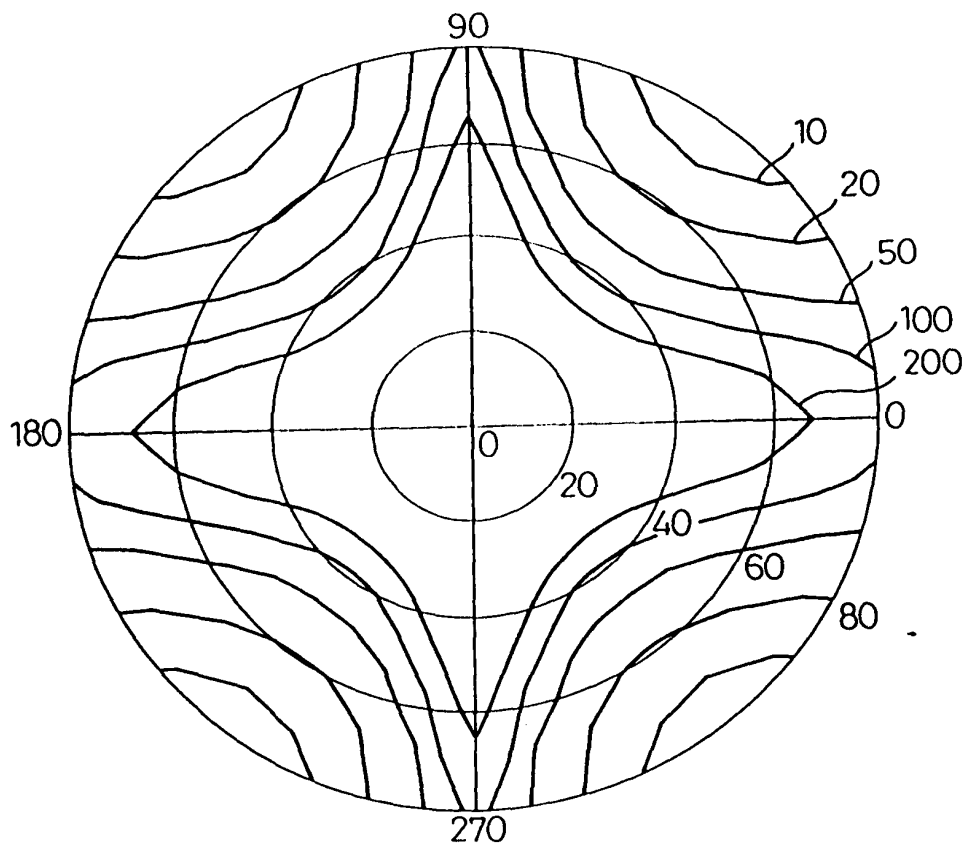
235/246

Fig. 244



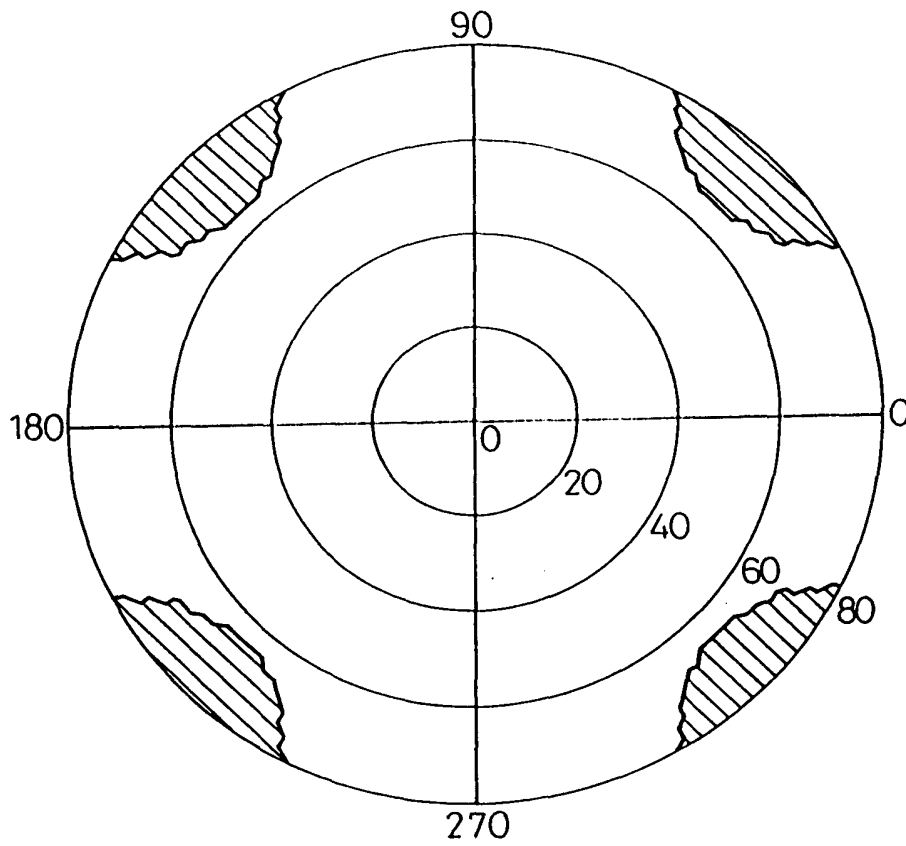
236/  
246

Fig. 245



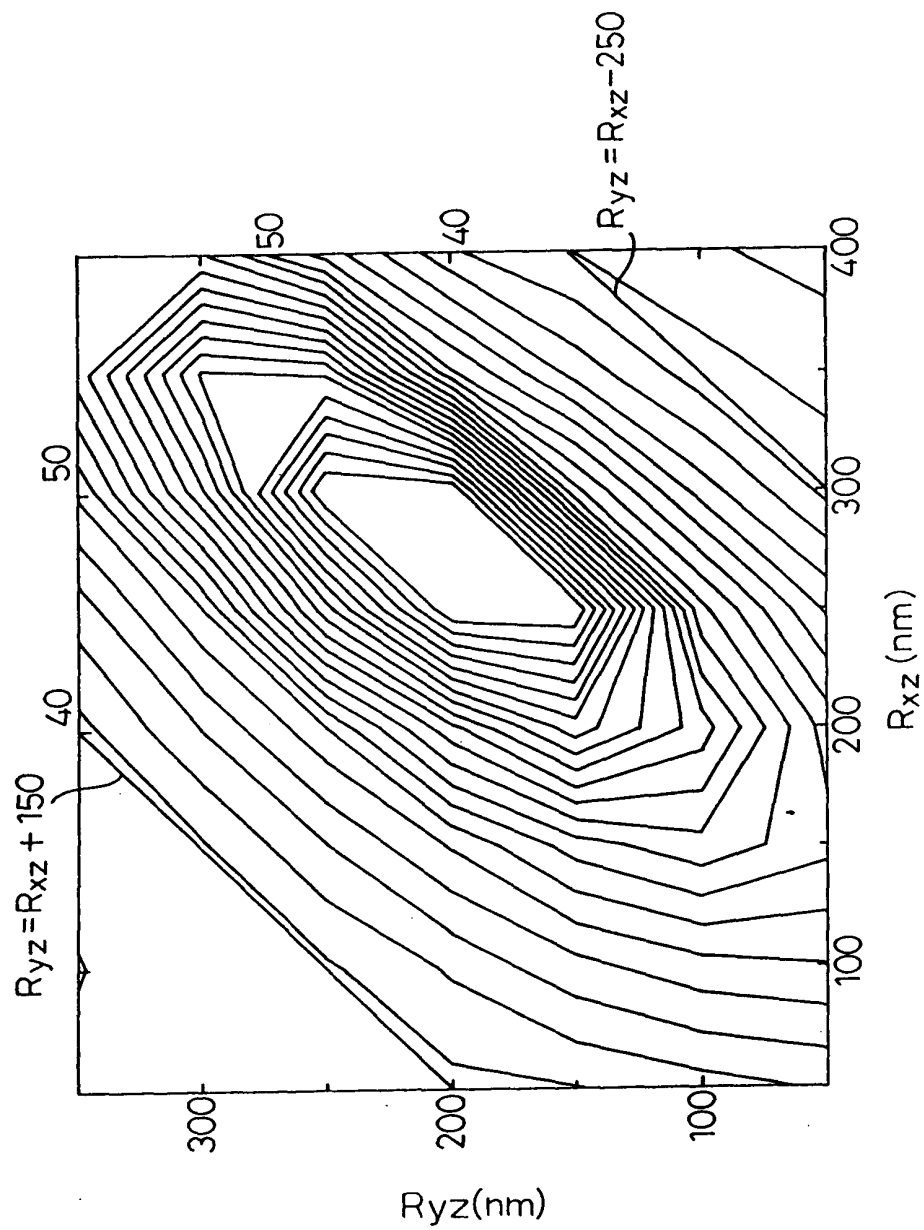
237/246

Fig. 246



238/246

Fig. 247



239/  
246

Fig. 248

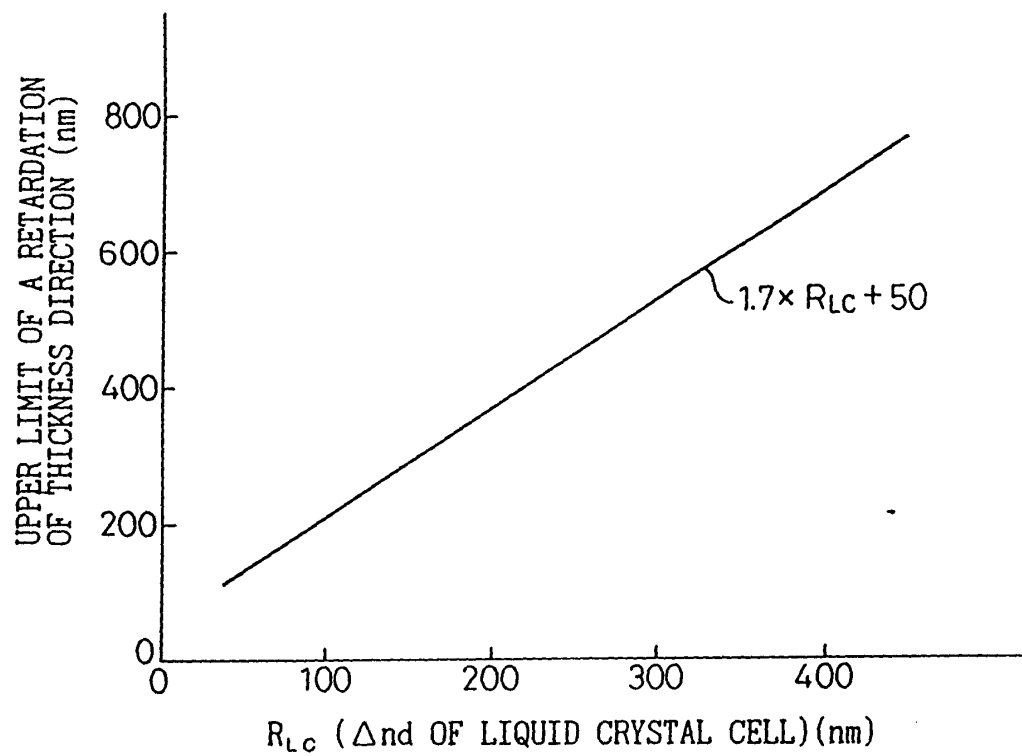


Fig. 249

SAMPLE	THICKNESS OF A PANEL ( $\mu\text{m}$ ) R G B	GAP BETWEEN PROJECTIONS ( $\mu\text{m}$ ) R G B	PHASE DIFFERENCE FILM Rd VALUE (nm)	TRANS- MITTANCE % (5v)	VIEW ANGLE : CR > 10 LEFT-RIGHT DIRECTION	COLOR DIFFERENCE (5v: LEFT -RIGHT)	
						$\Delta u(x)$	$\Delta v(y)$
EMBODIMENT A	5.7, 4.6, 3.6	20, 25, 30	320	5.60	$\pm 80^\circ$	0.03	0.03
EMBODIMENT B	5.7, 4.6, 3.6	20, 25, 30	320	5.60	$\pm 80^\circ$	0.03	0.05
PRIOR ART 1	R, G, B = 3.6	R, G, B = 30	240	4.50	$\pm 80^\circ$	0.06	0.05
PRIOR ART 2	R, G, B = 4.6	R, G, B = 30	320	5.80	$\pm 80^\circ$	0.14	0.12



241/246

Fig. 250

EXAMPLES	INITIAL VALUES	AFTER 200 HOURS
EMBODIMENT C	25	42
EMBODIMENT D	33	51
EMBODIMENT E	26	45
EMBODIMENT F	30	48
REFERENCE	32	70

242/  
246

Fig.251A

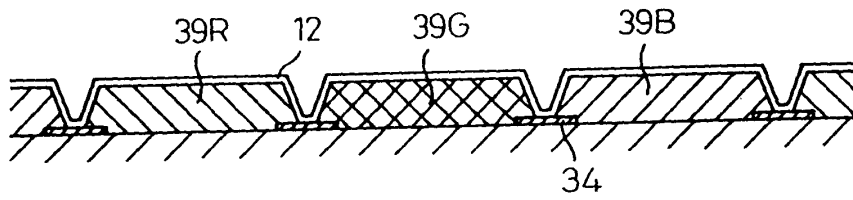


Fig.251B

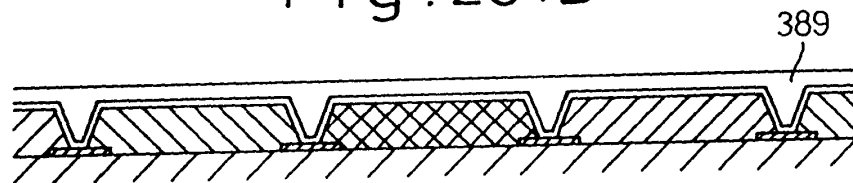


Fig.251C

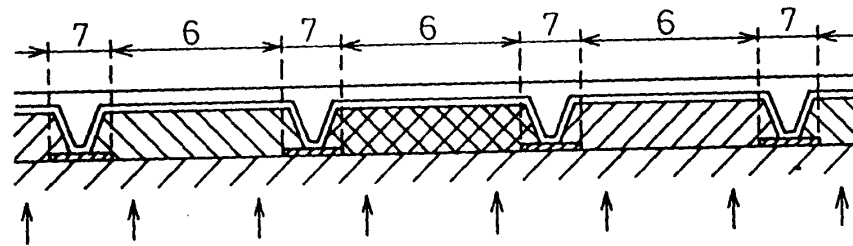
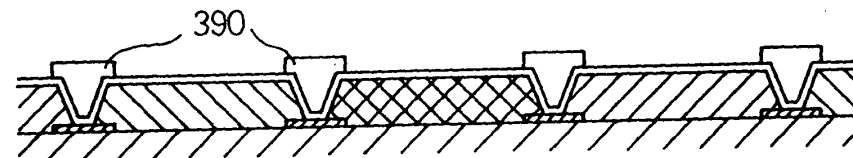


Fig.251D



243/246

Fig.252A

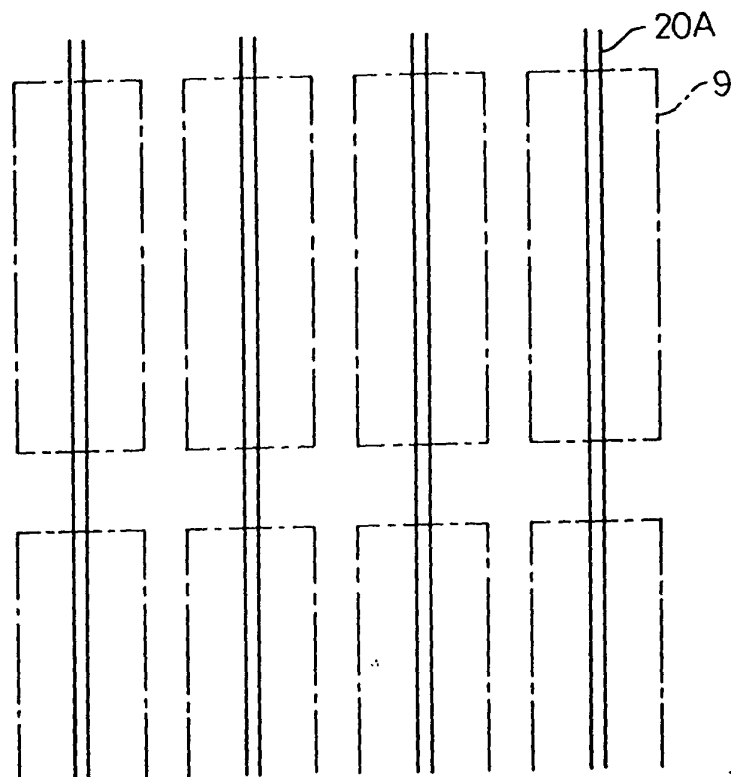
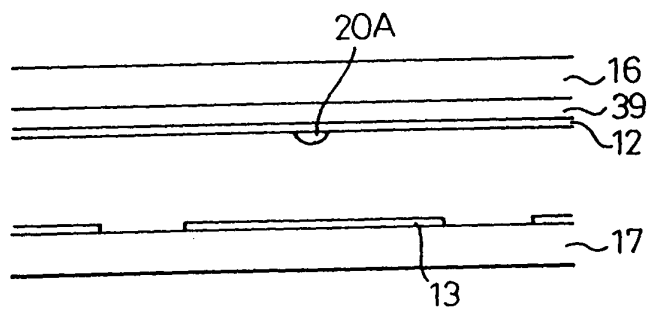
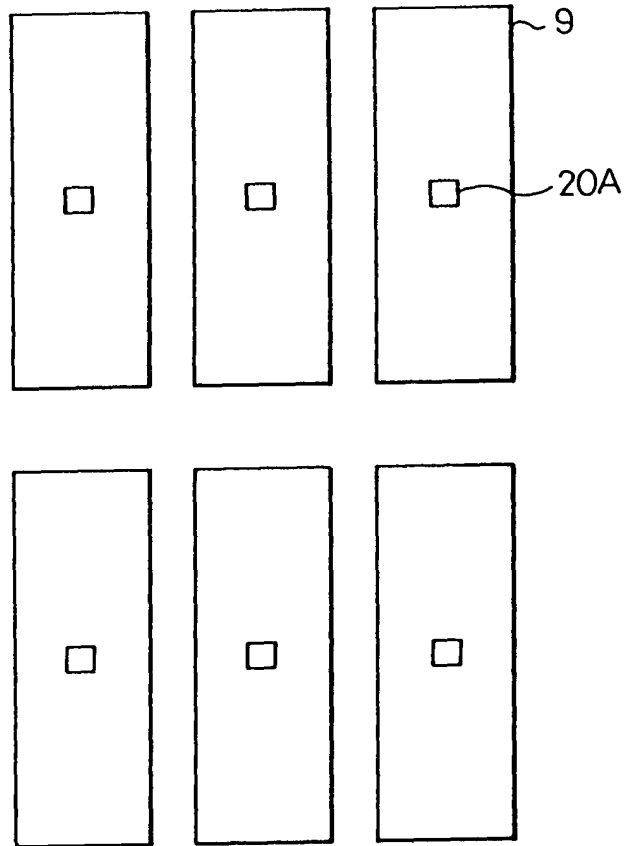


Fig.252B



244/  
246

Fig . 253



245/  
246

Fig. 254 A

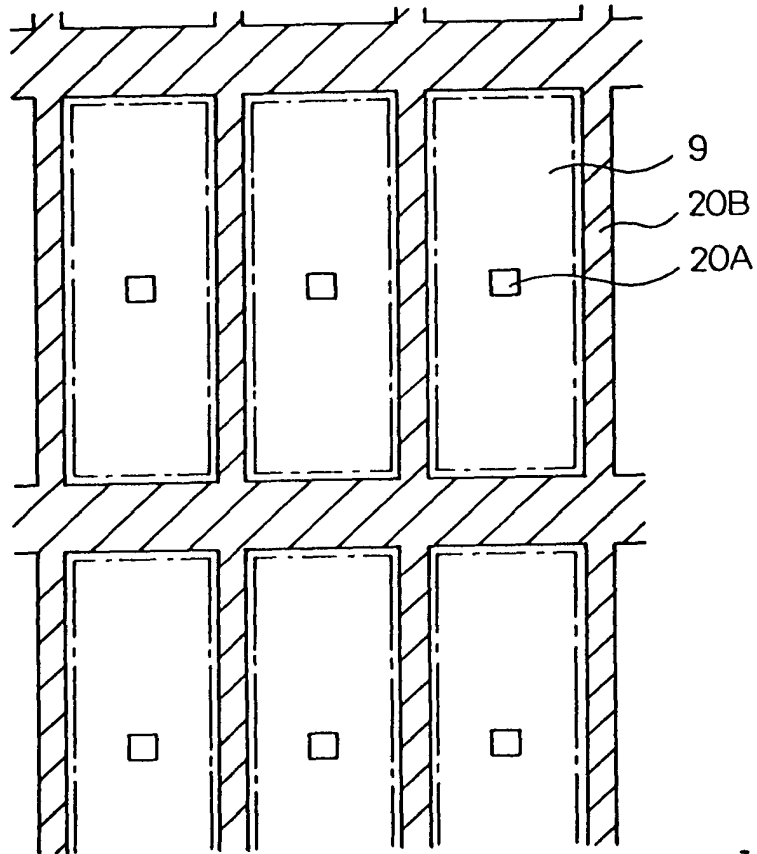
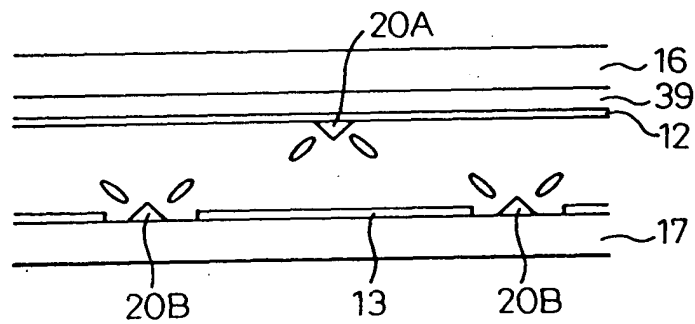


Fig. 254 B



246/  
246

Fig. 255

